US ERA ARCHIVE DOCUMENT

# **Coal Combustion Residue Impoundment Round 9 - Dam Assessment Report**

# Oklaunion Power Station Wastewater Evaporation Pond 6 – WMU 001 American Electric Power Vernon, Texas

### Prepared for:

United States Environmental Protection Agency Office of Resource Conservation and Recovery

### Prepared by:

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### INTRODUCTION, SUMMARY CONCLUSIONS AND RECOMMENDATIONS

The release of over five million cubic yards of coal combustion residue from the Tennessee Valley Authority's Kingston, Tennessee facility in December 2008, which flooded more than 300 acres of land and damaged homes and property, is a wake-up call for diligence on coal combustion residue disposal units. A first step toward this goal is to assess the stability and functionality of the ash impoundments and other units, then quickly take any needed corrective measures.

The Oklaunion Power Station features 17 total wastewater evaporation ponds; six (6) of the wastewater ponds contain some byproducts of the coal combustion process (CCP). Five of the six CCP ponds were incised (i.e., below grade) and therefore are not susceptible to dike failure. One Wastewater Evaporation Pond (Pond 6) has a sidehill configuration and was assessed for this report. This assessment of the stability and functionality of the one Oklaunion Power Station Wastewater Evaporation Pond (Pond 6) is based on a review of available documents and on the site assessment conducted by Dewberry personnel on Wednesday, February 23, 2011.

In summary, the Oklaunion Power Station Wastewater Evaporation Pond is rated **SATISFACTORY** for continued safe and reliable operation. This rating is based on the acceptable and satisfactory hydraulic and hydrological (H&H) and structural stability studies performed in June 2011.

### PURPOSE AND SCOPE

The U.S. Environmental Protection Agency (EPA) is investigating the potential for catastrophic failure of Coal Combustion Surface Impoundments (i.e., management unit) from occurring at electric utilities in an effort to protect lives and property from the consequences of a dam failure or the improper release of impounded slurry. The EPA initiative is intended to identify conditions that may adversely affect the structural stability and functionality of a management unit and its appurtenant structures (if present); to note the extent of deterioration (if present), status of maintenance and/or a need for immediate repair; to evaluate conformity with current design and construction practices; and to determine the hazard potential classification for units not currently classified by the management unit owner or by a state or federal agency. The initiative will address management units that are classified as having a Less-than-Low, Low, Significant, or High Hazard Potential ranking (for Classification, see pp. 3-8 of the 2004 Federal Guidelines for Dam Safety).

In early 2009, the EPA sent letters to coal-fired electric utilities seeking information on the safety of surface impoundments and similar facilities that receive liquid-borne material that store or dispose of coal combustion residue. This letter was issued under the authority of the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) Section 104(e), to assist the Agency in assessing the structural stability and functionality of such management units, including which facilities should be visited to perform a safety assessment of the berms, dikes, and dams used in the construction of these impoundments.

EPA requested that utility companies identify all management units including surface impoundments or similar diked or bermed management units or management units designated as landfills that receive liquid-borne material used for the storage or disposal of residuals or byproducts from the combustion of coal, including, but not limited to, fly ash, bottom ash, boiler slag, or flue gas emission control residuals. Utility companies provided information on the size, design, age and the amount of material placed in the units (See Appendix C).

The purpose of this report is **to evaluate the condition and potential of residue release from management units for hazard potential classification**. This evaluation included a site visit. Prior to conducting the site visit, a two-person team reviewed the information submitted to EPA, reviewed any relevant publicly available information from state or federal agencies regarding the unit hazard potential classification (if any) and accepted information provided via telephone communication with the management unit owner. Also after the February 23, 2011 field visit, additional information was received on March 22, 2011, by Dewberry & Davis LLC about the Oklaunion Power Station Wastewater Evaporation Ponds that was reviewed and used in preparation of this report.

This report presents the opinion of the assessment team as to the potential of catastrophic failure and reports on the condition of the management unit(s).

Note: The terms "embankment", "berm", "dike" and "dam" are used interchangeably within this report, as are the terms "pond", "basin", and "impoundment".

### LIMITATIONS

The assessment of dam safety reported herein is based on field observations and review of readily available information provided by the owner/operator of the subject coal combustion residue management unit(s). Qualified Dewberry engineering personnel performed the field observations and review and made the assessment in conformance with the required scope of work and in accordance with reasonable and acceptable engineering practices. No other warranty, either written or implied, is made with regard to our assessment of dam safety.



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### 1.0 CONCLUSIONS AND RECOMMENDATIONS

### 1.1 CONCLUSIONS

Conclusions are based on visual observations from a one-day site visit, February 23, 2011, and review of technical documentation provided by American Electric Power.

1.1.1 Conclusions Regarding the Structural Soundness of the Management Unit(s)

The dike embankments appeared to be structurally sound based on Dewberry engineers' observations during the site visit. A geotechnical analysis of Evaporator Pond 6 was provided to Dewberry in June 2011. The results of the analysis showed the pond has adequate Factors of Safety for both static and seismic conditions (See Appendix A, Doc 09).

1.1.2 Conclusions Regarding the Hydrologic/Hydraulic Safety of the Management Unit(s)

A hydrologic and hydraulic analysis was provided to Dewberry in June 2011. The analysis showed adequate freeboard to hold the 25% Probable Maximum Flood without overtopping (See Appendix A, Document 10). Therefore, Hydrologic/Hydraulic Safety factors are met for the CCR Management Unit.

1.1.3 Conclusions Regarding the Adequacy of Supporting Technical Documentation

The supporting technical documentation was adequate. Engineering documentation provided and subsequently reviewed is included in Appendix A.

1.1.4 Conclusions Regarding the Description of the Management Unit(s)

The description of the management unit provided by the Owner was a fairly accurate representation of what Dewberry observed in the field. Pond 6 is the only non-incised CCR pond that has been in service in the recent past. All other ponds on site either are incised or do not receive CCR. Also Pond 6 is in the process of being filled and eventually will be closed.

1.1.5 Conclusions Regarding the Field Observations

Dewberry staff was provided access to all areas in the vicinity of the management unit required to conduct a thorough field observation. The visible parts of the embankment dikes observed had no signs of overstress, significant settlement, shear failure, or other signs of instability. Embankments appeared structurally sound. There were no apparent indications of unsafe conditions or conditions needing remedial action. The only non incised pond (Pond 6) that received CCR appeared to be in the process of being filled and closed.

1.1.6 Conclusions Regarding the Adequacy of Maintenance and Methods of Operation

The current maintenance and methods of operation appear to be adequate for the non-incised pond, Pond 6. There was no evidence of significant embankment repairs or prior releases observed during the field inspection. However, there is no maintenance procedure documented.

1.1.7 Conclusions Regarding the Adequacy of the Surveillance and Monitoring Program

The surveillance program appears to be adequate. The management unit dikes are not instrumented. Based on a history of a current and regular inspection program and the fact that the only non-incised CCR pond (Pond 6) is in the process of being closed, installation of a dike monitoring system is not needed at this time. However, if Pond 6 is kept in operation a Surveillance and Monitoring Program should be documented.

1.1.8 Classification Regarding Suitability for Continued Safe and Reliable Operation

The Pond 6, Wastewater Evaporation Pond, is rated SATISFACTORY for continued safe and reliable operation.

### 1.2 RECOMMENDATIONS

1.2.1 Recommendations Regarding the Structural Stability

No recommendations warranted now that the seismic analysis has been received.

- 1.2.2 Recommendations Regarding the Hydrologic/Hydraulic Safety
  No recommendations warranted now that the H&H study has been received.
- 1.2.3 Recommendations Regarding the Supporting Technical Documentation The following recommendation is warranted: if Pond 6 is to be closed the operator should provide a closure plan and schedule.
- 1.2.4 Recommendations Regarding the Maintenance and Methods of Operation It is recommended that AEP develop and document a Maintenance and Methods of Operation Procedure, including checklists, or, as stated in Section 1.2.3, the plant should provide a closure plan and schedule for Pond 6.
- 1.2.5 Recommendations Regarding Continued Safe and Reliable Operation

  The recommendations cited above will ensure continued safe and reliable operation.

### 1.3 PARTICIPANTS AND ACKNOWLEDGEMENT

1.3.1 List of Participants

David Scott, Oklaunion Power Station
William R. Smith, American Electric Power Service Company
Steve Lewis, American Electric Power
Kyle Shepard, P.E., Dewberry
Andrew Cueto, P.E. PMP, Dewberry

1.3.2 Acknowledgement and Signature

We acknowledge that the management unit referenced herein has been assessed on February 23, 2011.

Andrew Cueto, P.E., PMP

# 2.0 DESCRIPTION OF THE COAL COMBUSTION RESIDUE MANAGEMENT UNIT(S)

### 2.1 LOCATION AND GENERAL DESCRIPTION

The Oklaunion Power Station is located at 12567 FM Rd 3430, Vernon, TX 76384, approximately three miles south-southeast of the intersection of Farm to Market Road 433 and Farm to Market Road 3430 in Wilbarger County, Texas

The plant is operated by American Electric Power Service Corporation and is a coal fired facility which features 17 total wastewater evaporation ponds with a total area of 335.9 acres: six (6) of the wastewater ponds contain some byproducts of the coal combustion process while the 11 other ponds contain cooling tower blowdown. The six ponds containing CCR are primarily located in the south central portion of the plant site.

Of the six CCR ponds five are incised; the sixth has a side hill embankment (Pond 6) with a height of 20 feet and a pool area of 68 acres. Earthen fill dikes retain the waste until it is sufficiently dry to be hauled away and landfilled. The Wastewater Evaporation Pond 6 is located at the south-central edge of the main evaporation pond complex of the generating station. An aerial photograph of the impoundment is provided in Appendix A – Doc. 01.

The Oklaunion Power Station Wastewater Evaporation Pond 6 was reported to be in the process of being filled with non-CCR material and is in the process of being closed. The impoundment was reported to not have received CCR for over three (3) years). The construction documents were issued on March 1, 1983 and construction was complete in 1987 as noted in Document 2 and 3 of Appendix A.

The table below provides the dimensions of the embankment:

Table 2.1: Summary of Dam Dimensions and Size							
Northeastern Station Bottom Ash Basin							
Dam Height (ft) 20 feet							
Crest Width (ft)	20 feet						
Length (ft)	3968 feet						
Side Slopes (upstream) H:V	N/A						
Side Slopes (downstream) H:V 3:1							

### 2.2 COAL COMBUSTION RESIDUE HANDLING

### 2.2.1 Fly Ash

The Fly Ash disposal process is a dry train procedure. AEP representatives preferred not to tour and inspect the Fly Ash disposal train directly. However, they did describe the process as follows:

- 1. Fly Ash is electrostatically precipitated and conveyed by gravity to a hopper,
- 2. The ash is then pneumatically conveyed into a holding silo,
- 3. The ash is then loaded via gravity feed into trucks (3<sup>rd</sup> party) for beneficial reuse.
- 4. Small quantities of fly ash that have not been sold (e.g., equipment cleaning during plant outages) are disposed of in Pond 6.

### 2.2.2 Bottom Ash

The Bottom Ash disposal process is a wet train procedure. Bottom ash is removed from the boiler and sluiced to the wastewater ponds.

### 2.2.3 Boiler Slag

The plant does not produce boiler slag.

### 2.2.4 Flue Gas Desulfurization Sludge

Flue Gas Desulfurization (FGD) sludge process was inspected on Wednesday, February 23, 2011. FGD sludge is disposed of in a pond located to the Northeast of Pond 6. This pond is incised and was not investigated further.

### 2.3 SIZE AND HAZARD CLASSIFICATION

The classification for size, based on the height of the dam is "Small" and based on the storage capacity criterion is "Small" in accordance with the USACE Recommended Guidelines for Safety Inspection of dams ER 1110-2-106 criteria summarized in Table 2.2a.

Table 2.2a: USACE ER 1110-2-106 Size Classification									
Impoundment									
Category	Category Storage (Ac-ft) Height (ft)								
Small	50 and < 1,000	25  and < 40							
Intermediate	1,000 and < 50,000	40 and < 100							
Large	> 50,000	> 100							

The State of Texas maintains a Dam Safety program through the Texas Commission on Environmental Quality (TCEQ). The only non incised pond (Pond 6) falls in the small category and is not a part of the Texas Dam inventory. Also, the American Electric Power Services Corporation Oklaunion Power Station Wastewater Evaporation Pond 6 dam is not in the National Inventory of Dams and therefore does not have an established hazard classification. Dewberry conducted a qualitative hazard classification based on the 2004 Federal Guidelines for Dam Safety classification system (shown in Table 2.2b).

Table 2.2b: FEMA Federal Guidelines for Dam Safety Hazard Classification									
	Loss of Human Life Economic, Environmental, Lifeline Losses								
-									
Low	None Expected	Low and generally limited to Owner							
Significant	None Expected	Yes							
High	Probable. One or more	Yes (but not necessary for							
	expected	classification)							

Loss of human life is not probable in the event of a catastrophic failure of the embankment and a failure of the embankment is expected to have a low economic and environmental impact. Therefore, Dewberry evaluated the Wastewater Evaporation Pond 6 as "low hazard potential".

# 2.4 AMOUNT AND TYPE OF RESIDUALS CURRENTLY CONTAINED IN THE UNIT(S) AND MAXIMUM CAPACITY

The data reviewed by Dewberry did not include the volume of residuals stored in Wastewater Evaporation Pond 6 at the time of inspection.

Table 2.3: Maximum Capacity of Unit							
Wastewater Evaporation Pond 6							
Surface Area (acre) <sup>1</sup>	68.6 at crest						
Current Storage Capacity (cubic yards) <sup>1</sup>	Unknown *						
<b>Current Storage Capacity (acre-feet)</b>	763 ac-ft						
Total Storage Capacity (cubic yards) <sup>1</sup>	Unknown *						
Total Storage Capacity (acre-feet)	Unknown *						
Crest Elevation (feet)	Unknown *						
Normal Pond Level (feet)	Unknown *						

<sup>\*</sup> Data was not provided by Utility

The maximum operating pool is El. 1205 ft. with a minimum crest elevation of 1208 ft, providing a minimum of 3 ft freeboard. Current water elevation is 1202 ft.

### 2.5 PRINCIPAL PROJECT STRUCTURES

### 2.5.1 Earth Embankment

The embankment is earthen filled with sandy clay with trace gravel. The approximate minimum designed crest width is 20 feet, however, since Pond 6 is in the process of being closed, the current crest widths exceed 150 feet with a minimum of 80 feet at its narrowest point. Approximate embankment height is 20 feet. The embankment is anchored into original ground at a minimum depth of five (5) feet. In-situ earthen material was used in the construction of the embankment according to the original specifications.

### 2.5.2 Outlet Structures

Water generated by Wastewater Evaporation Pond 6 is evaporated from the pond leaving the waste ash in place. The Pond does not have an outlet structure.

### 2.6 CRITICAL INFRASTRUCTURE WITHIN FIVE MILES DOWN GRADIENT

The American Electric Power Services Corporation Oklaunion Power Station is located southeast of Vernon Texas and south of Oklaunion Texas. Wastewater Evaporation Pond 6 is located on an unnamed tributary of Boggy Creek, Beaver Creek, Wichita River, and Red River. It cannot be determined if there is any critical infrastructure immediately downstream along the unnamed tributary, as this data was not provided by the Owner. Given the rural location of the plant, no critical infrastructure would be expected in the vicinity of the plant.

<sup>&</sup>lt;sup>1</sup> Appendix A, Document 10

### 3.0 SUMMARY OF RELEVANT REPORTS, PERMITS, AND INCIDENTS

### 3.1 SUMMARY OF REPORTS ON THE SAFETY OF THE MANAGEMENT UNIT

Four quarterly inspection reports were provided by AEP:

- 2009 Dam & Dike Inspection Report, Wastewater Pond Complex,
   Oklaunion Power Plant, June 2009, Prepared by URS Corporation.
- Dam & Dike Inspection Report, Wastewater Pond Complex, Oklaunion Power Plant, Inspection Date: August 4, 2010, Prepared by William R. Smith, P.E.
- Inspection Report, Oklahoma Pond Complex, Inspected By: Pat Mackenzie and Steve Lewis / Oklaunion Power Plant, November 22, 2010.
- Inspection Report, Oklahoma Pond Complex, Inspected By: Pat Mackenzie and Steve Lewis / Oklaunion Power Plant, March 7, 2011.

# 3.2 SUMMARY OF LOCAL, STATE, AND FEDERAL ENVIRONMENTAL PERMITS

The State of Texas has a Dam Safety Program that is the responsibility of the Texas Commission on Environmental Quality (TCEQ); however, due to its small size, this dam is not permitted by the TCEQ.

Discharge from the impoundment is regulated by the Texas Commission on Environmental Quality (TCEQ). The TCEQ has issued a National Pollutant Discharge Elimination System Permit for the plant. Permit No. WQ0002574000 was originally issued September 13, 2004 and was re-issued on November 16, 2007.

### 3.3 SUMMARY OF SPILL/RELEASE INCIDENTS

Data reviewed by Dewberry did not indicate any spills, unpermitted releases, or other performance related problems with the dam over the last 10 years.

### 4.0 SUMMARY OF HISTORY OF CONSTRUCTION AND OPERATION

### 4.1 SUMMARY OF CONSTRUCTION HISTORY

### 4.1.1 Original Construction

The Oklaunion Power Station Wastewater Evaporation Pond 6 was constructed in 1987. It is a side hill embankment.

### 4.1.2 Significant Changes/Modifications in Design since Original Construction

- The upstream slope has been filled and compacted with native soil dredged from adjacent process water evaporation ponds. It was reported that this material did not contain CCR.
- Dewberry personnel onsite were informed that Evaporation Pond No. 6 is in the process of being closed.

### 4.1.3 Significant Repairs/Rehabilitation since Original Construction

Notations have been made in the internal inspection reports over the past two years (2009 and 2010) of the following repairs / rehabilitation:

- Vegetation clearing
- Repair of eroded gullies on embankment slopes
- Removal of small trees from embankment slopes.

### 4.2 SUMMARY OF OPERATIONAL PROCEDURES

### 4.2.1 Original Operational Procedures

The Plant features 17 wastewater evaporation ponds. Eleven of these ponds receive cooling tower blowdown; no CCR is stored in these 11 ponds. Six of the ponds contain some byproducts of the coal combustion process. Five of these ponds are incised, and therefore have no embankments or dams. Only one evaporation pond is not incised - Pond 6. Earthen fill dikes retain the waste until it is sufficiently dry to be hauled away and landfilled or the waste is left in place and the ponds are closed as is the case with Evaporation Pond No. 6.

4.2.2 Significant Changes in Operational Procedures and Original Startup

No documents were provided to indicate any operational procedures have been changed.

4.2.3 Current Operational Procedures

Bottom ash is wet conveyed to the Evaporation Pond Complex. Ash is deposited via sedimentation into the six CCR storage ponds. Ash sediment is currently stored in Pond No. 6, which will eventually be closed, and the ash reclaimed for beneficial use.

4.2.4 Other Notable Events since Original Startup

No additional information was provided to Dewberry of other notable events that have impacted the impoundment's operation.

### 5.0 FIELD OBSERVATIONS

### 5.1 PROJECT OVERVIEW AND SIGNIFICANT FINDINGS

Dewberry personnel Andrew Cueto, P.E. and Kyle Shepard, P.E. performed a site visit on Wednesday, February 23, 2011 in company with the participants.

The site visit began at 10:30 AM. The weather was cloudy and cool. Photographs were taken of conditions observed. Please refer to the Dam Inspection Checklist in Appendix C for additional site information. Selected photographs are included here for ease of visual reference. All pictures were taken by Dewberry personnel during the site visit.

The overall assessment of the dam was that it was in satisfactory condition and no significant findings were noted.

### 5.2 SOUTH EMBANKMENT

### 5.2.1 Crest

The crest of the South Embankment showed no signs of depressions, tension cracks, or other indications of settlement or shear failure, and appeared to be in satisfactory condition. Figure 5.2.1-1 shows the conditions of the crest of the South Embankment.



Figure 5.2.1-1. Figure showing the South Embankment crest and outside slope conditions.

### 5.2.2 Upstream / Inside Slope

The South Embankment's inside slope has been filled up to the crest elevation with native soil, effectively eliminating this slope on the east end of the embankment. Figure 5.2.2-1 shows these areas.



Figure 5.2.2-1. Figure showing the South Embankment lack of inside slope.

### 5.2.3 Downstream / Outside Slope and Toe

There were no observed scarps, sloughs, bulging, cracks, or depressions indicating slope instability or signs of erosion. The outside slope of the South Embankment was covered with sparse overgrown vegetation. The outside slope appears to be in good condition. Figure 5.2.3-1 shows the general condition of the outside slope of the South Embankment.



Figure 5.2.3-1 general good condition of the outside slope of the South Embankment.

### 5.2.4 Abutments and Groin Areas

The outside slope of the abutments and groin were uniformly graded and covered with sparse grass. Erosion or uncontrolled seepage was not observed along either groin. Figure 5.2.4-1 shows the general condition of the Abutments and Groin.



Figure 5.2.4-1. Southern Groin.

### 5.3 EAST EMBANKMENT

### 5.3.1 Crest

The crest of the East Embankment showed no signs of depressions, tension cracks, or other indications of settlement or shear failure, and appeared to be in satisfactory condition. Figure 5.3.1-1 shows the conditions of the crest of the East Embankment.



Figure 5.3.1-1. Figure showing the East Embankment crest and outside slope conditions.

### 5.3.2 Upstream / Inside Slope

The East Embankment's inside slope is non-existent with the waste in the pond being allowed to remain in place up to near the crest elevation of the embankment. The Pond appears to being allowed to fill up with solid ash waste working its way east to west. This condition can be viewed in Figure 5.3.2-1.



Figure 5.3.2-1. East Embankment, lack of inside slope.

### 5.3.3 Downstream / Outside Slope and Toe

There were no observed scarps, sloughs, bulging, cracks, or depressions indicating slope instability or signs of erosion. The outside slope of the East Embankment is the upstream slope of the Emergency Spillway. It is uniformly graded and covered with sparsely overgrown grass. Figure 5.3.3-1 shows the general condition of the East Embankment's crest, outside slope and groin.



Figure 5.3.3-1. Crest, outside slope and groin of East Embankment.

### 5.3.4 Abutments and Groin Areas

There were no observed scarps, sloughs, bulging, cracks, or depressions indicating slope instability or signs of erosion on the groins of the East Embankment. The top right-side of Figure 5.3.3-1 shows the general condition of the East Embankment's groin.

### 5.4 OUTLET STRUCTURES

### 5.4.1 Overflow Structure

The Overflow Structure is detailed in the original design drawings (See Appendix A – Doc 3). The structure is not on Wastewater Evaporation Pond No. 6, but is on Pond No. 7, immediately to the east of the East Embankment of Pond No. 6. Pond 6 is an evaporation pond with no outlet structures or spillways.

### 5.4.2 Outlet Conduit

No Outlet Conduit is present.

### 5.4.3 Emergency Spillway

See Overflow Structure, Paragraph 5.4.1 above.

### 5.4.4 Low Level Outlet

No Low Level Outlet is present.

### 6.0 HYDROLOGIC/HYDRAULIC SAFETY

### 6.1 SUPPORTING TECHNICAL DOCUMENTATION

### 6.1.1 Flood of Record

No documentation has been provided about the flood of record.

### 6.1.2 Inflow Design Flood

Pond 6 only receives direct rainfall and there are no other flows into the pond area. The Hydrology and Hydraulic (H&H) Analysis assumed vertical sides so the pool area did not change during the flood condition and the study did not assume any discharge or overflow since there is no outlet structure (see Appendix A, Doc 10). Based on its small size category the design flood is the 25% Probable Maximum Flood (PMF).

### 6.1.3 Spillway Rating

No spillway hydraulic data was provided for review, since there is no pond outlet structure.

### 6.1.4 Downstream Flood Analysis

No downstream flood analysis data was provided for review.

### 6.2 ADEQUACY OF SUPPORTING TECHNICAL DOCUMENTATION

The supporting documentation reviewed by Dewberry is adequate.

### 6.3 ASSESSMENT OF HYDROLOGIC/HYDRAULIC SAFETY

The H&H analysis looked at multiple rainfall events ranging from the 10-year, 24-hour to the 25%, 72-hour PMP. The analysis showed the total Pond 6 rainfall event that does not result in any overtopping is equivalent to the 25%, 12-hour PMP of 8.6 inches. This PMP event is greater than either the original design basis or the larger current design basis. (See Appendix A, document 10). The analysis is therefore adequate to demonstrate the pond is safe from overtopping.

### 7.0 STRUCTURAL STABILITY

### 7.1 SUPPORTING TECHNICAL DOCUMENTATION

### 7.1.1 Stability Analyses and Load Cases Analyzed

A stability analysis for Evaporation Pond No. 6 was conducted by BBCM (see Appendix A, Document 09). The analysis addressed rapid drawdown, steady state seepage at maximum water level, steady state seepage with surcharge water level, and seismic conditions assuming 2%, 50-year occurrence. The study was completed in June 2011.

The stability analyses were performed using the program SLIDE (V.6) and used Spencer's Method to perform 2-D limit equilibrium for slope stability analyses. The analyses were performed for the cross section location along the dike that represented the highest point and steepest slope.

### 7.1.2 Design Parameters and Dam Materials

Documentation provided to Dewberry for review was the specifications for Phase I Construction (Site Preparation) Oklaunion Power Station (Unit No. 1) (See Appendix A – Doc. 4). For the stability analyses soil shear strength and unit weight values were developed based on recent construction of Evaporation Ponds 12 and 13 that are part of the whole evaporation pond complex. Soil borings at Pond 6 were analyzed to verify the soils strength data for Ponds 12 and 13 were representative of Pond 6. An effective cohesion value of 50 psf was used to focus the program on deep failure surfaces rather than shallow slope sloughing.

Seismic analyses were performed using a pseudo-static analytical approach with a horizontal coefficient of 0.06g derived from the 2008 USGS National Seismic Hazard Maps for peak acceleration with 2%, 50-year exceedance (see Appendix A, Document 09, Plate 9)

### 7.1.3 Uplift and/or Phreatic Surface Assumptions

Data from the groundwater monitoring system at the plant was used to develop the phreatic surface levels within the embankments for the analyses. Three groundwater wells are located along the crest of the south embankment of Pond 6. The well at the southwest corner was used to locate groundwater elevations at 1179.3 ft msl.

Based on the Geotechnical Borings included in the Specifications for Phase I Construction (Site Preparation) Oklaunion Power Station (Unit No. 1), (See Appendix A – Doc. 2), the initial phreatic surface was assumed to be at the elevation measured in the borings.

### 7.1.4 Factors of Safety and Base Stresses

Table 7.1-1 presents the computed Factors of Safety for loading conditions of concern. Note that the rapid drawdown condition is not appropriate for this pond configuration.

<b>Loading Condition</b>	Minimum Allowable Factor of Safety	Slope	Computed Factor of Safety
Rapid Drawdown	1.3	Inboard	1.38
Steady-State Seepage (Max Water Level)	1.5	Inboard	2.24
		Outboard	1.69
Steady-State Seepage with Surcharge Water Level	1.4	Outboard	1.69
Seismic (Max Water Level)	1.0	Inboard	1.61
		Outboard	1.45

### 7.1.5 Liquefaction Potential

The documentation reviewed by Dewberry did not include an evaluation of liquefaction potential. Foundation soil conditions do not appear to be susceptible to liquefaction.

### 7.1.6 Critical Geological Conditions

There was no documentation provided to Dewberry that included an evaluation of Critical Geological Conditions.

### 7.2 ADEQUACY OF SUPPORTING TECHNICAL DOCUMENTATION

Structural stability documentation is adequate.

### 7.3 ASSESSMENT OF STRUCTURAL STABILITY

The structural stability of the dam is Satisfactory based on the static and seismic analyses provided

The following observations were made during the onsite inspection:

- The crest appeared free of depressions and no significant vertical or horizontal alignment variations were observed,
- There were no major scarps, sloughs, or bulging along the embankments,
- Boils, sinks, or uncontrolled seepage were not observed along the slopes, groins, or toes of the embankments.

### 8.0 ADEQUACY OF MAINTENANCE AND METHODS OF OPERATION

### 8.1 OPERATING PROCEDURES

The facility is operated as a settling basin and storage of coal combustion ash residual deposits and bottom ash transport water.

### 8.2 MAINTENANCE OF THE DAM AND PROJECT FACILITIES

While no maintenance plan was supplied to Dewberry for review, based upon observations made during the February 23, 2010 site visit and discussions with Plant representatives, dam maintenance appears to be adequate.

### 8.3 ASSESSMENT OF MAINTENANCE AND METHODS OF OPERATIONS

### 8.3.1 Adequacy of Operating Procedures

No documented operational procedures were supplied to Dewberry for review. However, a verbal description of maintenance procedures and methods was presented at time of inspection.

### 8.3.2 Adequacy of Maintenance

No record of Maintenance was supplied to Dewberry for review. It was observed that the existing operating procedures adequately maintain the Management Unit. It was recommended that these procedures be documented and put into checklists.

### 9.0 ADEQUACY OF SURVEILLANCE AND MONITORING PROGRAM

### 9.1 SURVEILLANCE PROCEDURES

### **Quarterly Inspections**

The plant surveillance procedures state, "Quarterly inspections shall be completed by Plant personnel and within 24 hours of unusual events, such as seismic activities or a "significant storm event". A significant storm event is defined as three inches or more of rainfall in 24 hours. Inspections should be documented in accordance to AEP Circular Letter CI-M-CL-010C."

### 9.2 INSTRUMENTATION MONITORING

No documentation was provided to Dewberry, nor was monitoring instrumentation seen during the site visit, to suggest that instrumentation monitoring was in place at Oklaunion Power Station.

### 9.3 ASSESSMENT OF SURVEILLANCE AND MONITORING PROGRAM

### 9.3.1 Adequacy of Inspection Program

Based on the data provided in the quarterly inspection reports reviewed by Dewberry, plus observations during the site visit, the inspection program is adequate.

### 9.3.2 Adequacy of Instrumentation Monitoring Program

An instrumentation monitoring program is not needed for the one non-incised pond, given its small size and the intention to close Pond 6 in the near future

# APPENDIX A

**Document 1** 

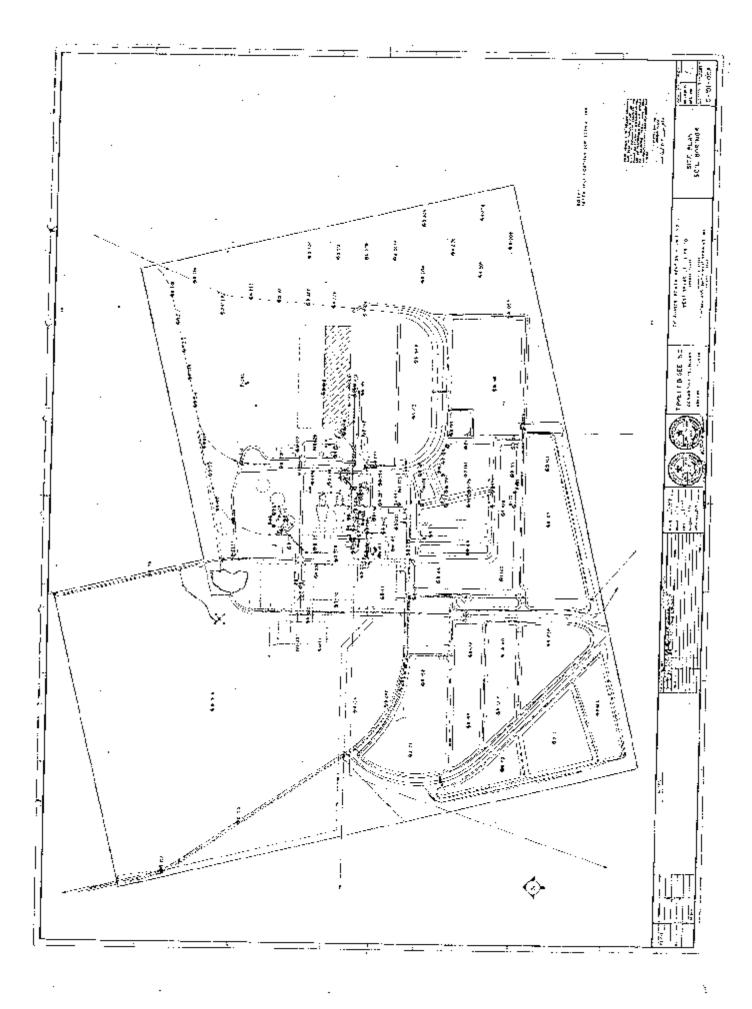
Aerial Photo



# APPENDIX A

# Document 2

Plans Original Site & Boring Locations



	LOG OF BORING NO. 8-108 OKLAUNION POWER STATION UNIT NO. 1 WILBARGER COUNTY, TEXAS									
7	ÞΕ	BOS	RING: Undisturbed Sample and Core (	.OÇA	TIO	N: Se	e Pi	an o	f 8or	rings, Plate 3
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: 1201.2	ROD %	8	% PASSING NO. 200 SIFVE	Light	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH X 10 10 10 10 10 10 15 10 15
5			Very stiff reddish-brown silty clay, w/occasional coarse gravel and organic material -w/numerous weathered calcareous nodules at 3.0' (CL) Soft reddish-brown sandstone, fine grained, thin bedding							
-10-			-w/numerous soft bluish-gray sandstone laminations and inclusions at 6,0' Soft reddish-brown sillstane, thin flat bedding, w/numerous soft bluish-gray sillstone inclusions -soft bluish-gray sillstone seams,		100 100	99	35	16	10	=3.06x1\01"cm/sec 131
-15 -20			gently dipped bedding at 11.0' -clayey at 13.0' -high angle fractures -soft reddish-brown claystone seam, thick bedding from 18.0- 20.7'		100 160	92	31	16	10 %	(**): 30x10
			-soft bluish-gray sandy claystone seam from 20.7-21.0°, coarse grave!	- 1	100 100	86	29	14	8 14	di
= {	77		seam, w/fine grave! from 27.5- 28.5	ľ	00				H	
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35	33	. 1	thick bedding, w/occasional off bluish-gray silty claystone netusions			-	-		- <del>  -</del>  - - - - - - - - - - - - - - - - -	
	(Continued)									
WE MATIONAL SOR SERVICES PLATE 24										

	LOG OF BORING NO. 8-108 (Cantd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS									
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	R00 %	CORE: RECOVERY*%	% PASSING NO. 200 SIEVE	CIOUID	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH AND SHEAR STRENGTH AND SHEAR STRENGTH AND SHEAR SHE
40		V 717 13 13 15 17 17	-w/numerous high angle fractures at 35.0'	79	80					
45			-w/numerous high angle fractures -soft clayey shale seam from 43.0-44.0f -soft bluish-gray claystone seam	<u>.</u>	300			:		
-50			from 44.8-45.1° -w/numerous high angle fractures -extremely slickensided				į		- - - - - - - - - - - - - - - - - - -	
			-soft bluish-gray claystone seam,	93	100					
68	w/fine gravel from 57.0-57.6"  -w/numerous slickensides, indurated									
3	TATA TATA		-w/numerous high angle fractures	97	100					
70	(Continued)									
PLATE 25										

SOIL DESCRIPTION  SOIL DESCRIP		LOG OF BOOKLAUNION PO WILBAR	OWE	R ST/	ATIC	N -	- UN	IIT N	
stone inclusions —moderately herd bluish-gray clayey silistone seam at 73.3- 74.6¹ —moderately hard reddish-brown, indurated, w/accasional moderately hard bluish-gray silistone inclusions and numerous fractures  -slightly slickensided, w/high angle fractures -very soft clayey shale seam at 85.1-85.8¹  Very soft reddish-brown clayey shale, w/soft reddish-brown claystane interbeds to 97.0¹  84 100	DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	1	PECOVERY %	% PASSING NO. 200 SIEVE	Clouid Likit	PLASTIC	MOISTURE CONTENT, %	IN TONS/SOFT X:00/SE
40101 57101 570711 1/3 81		moderately hard bluish-gray clayer sillstone seam at 73.3-74.6' -moderately hard reddish-brown, indurated, w/occasional moderately hard bluish-gray sillstone inclusions and numerous fractures  -slightly slickensided, w/high angle fractures -very soft clayer shale seam at 85.1-85.8'  Very soft reddish-brown clayer shale, w/soft reddish-brown clayer alloystone interbeds to 97.0'	91	100					
COMPLETION DEPTH: 101.0'   DEPTH TO WATER: 3.0'   DATE: 4/25/81   DATE: 5/2/81   PLATE 26			DEPT	H 1					

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Γ	LOG OF BORING NO. 8-168 OKLAUNION POWER STATION - UNIT NO. I													
	WILBARGER COUNTY, TEXAS													
TY	PE	ео	RING: Undisturbed Sample 1,004	T!OI	ų; 5e	e Pl	en o	f Sar	ing	s, P	late	e 3		
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-10-			w/numerous fine roots (ML)  Hard brown silty clay  -w/numerous calcareous nodules at 3.0'  -light brown, w/calcareous and magnesium nodules at 5.0'  -reddish-brown, w/numerous pockets of weathered calcareous material and fine sand at 7.0'  -w/occasional magnesium nodules and bluish-gray silty clay inclusions at 9.0'  -w/calcareous filled fissures and		87	43	14	17					\$ 4 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5 4 5	
	N	V	inclusions at 11.0° (Cl)	100					#	<del>†</del>	<b>!</b> ††	<del>         </del>		1 -
-20-		AMERICA MACAMETANA	Soft reddish-brown silty claystone, thin flat bedding, w/occasional bluish-gray silty alaystone inclusions -crossbedded, w/occasional pyrite -thin flat bedding, w/occasional	100										
	43	22	codrse sand pockets	60			ŀ		2	<u>i        </u>				]
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MEST HATTOMAL SOIL SERVICES
CONSELTING EMPLOYERS

PLATE C6

LOG OF BORING NO. 8-170 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS													
*YPE_BORING:Undisturbed_Sample_and_Core!			-			F Para	rings, Plate 3						
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ELEVATION: 1213.0	, "	<u> </u>	%.5			38	0.5 LO (5 📴						
Hard brown silty clay, w/fine roots -reddish-brown, w/occasional coarse sand and fine gravel, w/weathered calcareous nadules (CL)		100											
Soft reddish-brown silty dlay- stone, w/numerous large bluish- 100													
gray silty claystone inclusions,													
w/some fine sand   10-2-15   Hard reddish-brown silty clay,   somewhat friable (CL)   Soft reddish-brown silty clay-		100											
stone, crossbedded, w/occasional bluish-gray silty claystone inclusions -rossbedded, w/occasional	<u> </u> 	100				-							
bluish-gray silty claystone laminations and very soft clay- stone and increasing silt at 14.0'		100	į										
-w/numerous yellow inclusions, thick bedded, decreasing silt		100				 							
-w/bluish-gray silty claystone		100				-  -  -  -  -							
seam at 30.1–30.4'  w/coarse sand and fine gravel to 33.0'													
Soft recidish-brown silty shale,  w/occasional bluish-gray silty shale inclusions	85	100		-	1	-							
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	LOG OF BORING NO. B-170 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
DEPTH. FT. SYMBOL SAMPLES	so	il. DESÇI	RIPTION	Rob %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	LIGUID	PLASTIC	MOISTURE CONTENT, %	IN	TONS	/5 <b>Q</b>	LBS./CU. FT.
	Soft reddist stone, w/b stone seam, 38.1-38.4'-w/occasio packets and	luish-gray w/coarse nat bluish	silty clay- e sand at	39	97								
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	X	1	w/weathered calcareous nodules								┆┼┼╄	<del>╏</del> ┋┋	1 1
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	-reddish-brown, w/occasional bluish-gray silty clay seams,												
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	$\mathcal{H}$		stone, w/soft to moderately hard		ĺ		İ		H		┇┍╏╽┇ <del>┇┆</del> ┾╅╄	<del>┥</del> ┋┥╃┡┋╁╴	
			clayey sandstone interbeds from 7.0-12.0'	ļ		ŀ		Ì	-		╆╫	<del>┞</del> ┼╁╏┆╎┋╸	3
	N.	3	-w/bluish-gray silty claystone	1		ı					<b>[</b> ]	<del>                                     </del>	1
15 %	挩	7	seams, w/coarse sand at 8.9-9.1"	ľ	100		Į					사	3
		7	-cræsbedded at 11.0'	ĺ					H	╁╁╂╂┷	<b>!!</b>		- [
			-w/some coarse sand and bluish- gray silty claystone inclusions			- 1	ļ	-	1		┦╫┾	┋╇╃┾╏╀┼	- 1
			of 15.0'		- 1	j	ŀ	-	H	╁┼┼╂┼┾	╌┼┼	┇┩┪┇╃╏	4
-20-5	14		-decreasing silt	ו	col	Ì			Ţ			φ	4
	拯	1	-thin flat badding	į	-			İ	ļļ	<u>                                     </u>	<u> </u>		
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	Ŋ.	ĺ			ŀ			-	H	<del>╎╎╏╏</del>	┥┿╅┼	╁╂┼┼┼	3
25.3	17	l	-w/bluish-grey silty claystone		10Q		1				<del>┆┋</del> ┞╬┩	<del></del> <del></del> <del> </del>	4
( <del>)</del>	挺	Ì	inclusions, crossbedded			1			Ţ.				3
	挺			ŀ		ļ			[]		<del>┞╏╏</del> ┋	<del>┊┋</del>	4
<del>- 2</del>	贫	ĺ		]			İ		} <del>[</del>		╀╂┼┞╃	<del>┦</del> ┦╃ <del>┦</del> ╅┩	-1
30 3	揪		-w/bluish-gray silty claystone	1	00		-	Ī	j	<b> </b>	<del>           </del>	<del>                                      </del>	#
<del></del>	随	;	eam at 30.0-31.01		ᅱ.			1					1
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OCHE	CHAL LL THE	50K	Kringes Heirs							P	ATE	91	_

	LOG OF BORING NO. 8-171 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
DEPTH, FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	ROD %	CORE RECOVERY %	% PASSING NO 200 SIEVE	LIOUO	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH IN TONS/SOFT. LA DOS/SOFT. LA			
	77.	ill.	······································				·						
40 -			Very soft reddish-brown clayey shale, w/occasional bluish-gray shale inclusions	58	58								
45-			Soft reddish-brown silty clay- stone -w/accasional bluish-gray seams, w/coarse sand at 43.0' -w/bluish-gray silty claystone seam; w/coarse sand at 45.8- 46.1'	93	95								
-55-													
	OME	l'E	TION DEPTH: 50.0° DATE: 5/12/81	7930	TH T				7.7. 5/12	/31			

MATIOGRAL EDIL SERVICES, MO., COMMUNICAL ENGINEEMS.

	LOG OF BORING NO. 3-172 OKLAUNION POWER STATION - UNIT NO. 1														
						LEARGER						•	,		
	ŢΥ	?E	BOS	NG: Undistud	ood Sample o	and CareL	OCA	TION	; 5	ee P	lan	of B	orings, Plate 3		
	рЕРТН. FT.	SYMBOL	SAMPLES	SOIL	DESCRIPTION	ON	RQ0 %	RECOVERY %	A PASSING C. 200 SIEVE	LIGUID	PLASTIC	MOISTURE CONTENT %	IN TONS/SQFT	S./CU. FT.	
Į		NIN.	<u> </u>	ELEVATION:			<u> </u>	72	°`≥			20	[ C.S R.J 1,5 45		
	5 1		****	Very stiff re- cley, w/acc and organics nincreasing s at 3.0' -hard, incre- and fine grav- gravel seam	asianal fine ilt and grav- asing coarse rel, very fri	gravel el sand able		100							
	10-			Soft reddish- stone, thick sional bluish- stone inclusion	bedded, w/i -gray silty o	clay <del>-</del> occa÷		100		ļ					
	15			-increasing s -medium gen w/moderately at 14.0-14.2 -w/occasiona claystone sea	tly dipped b hard sillsto tl bluish-gro	edding, ine soom ly silty		100				: : : - -			
				at 15,0° -thick beddir	g		į	100							
	1 1 1 1 1	为的在我的		-w/numerous silty clayston		-gray		100						-	
3	77777777	THE PROPERTY OF	] .	decreasing si severe water heavily fracti	loss at 30.0			100						بعقية فيتبانينينا	
	٦						<u> </u>	<u> </u>		1			TITETTI (TITETTI)	1	
₩	(Continued)														
	COM	A.T.N	4 6+	COMMITTING ENGINEERS PLATE 93.											

	LOG OF BO OKLAUNION PO WILBAR	<b>DWE</b>	r st	ATIO	· MC	- UN	VI T	
SYMBOL SAMPLES	DESCRIPTION	Rob %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	Liguid	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH SLL IN TONS/SOFT COLUMN LNC/C
-extremely slines -extremely slines -sosososocompletion depth:	ckensided high angle	92 PEPT		0 W	ATE	न: C		d at 20.5
DATE:	5/11/81				DAT			

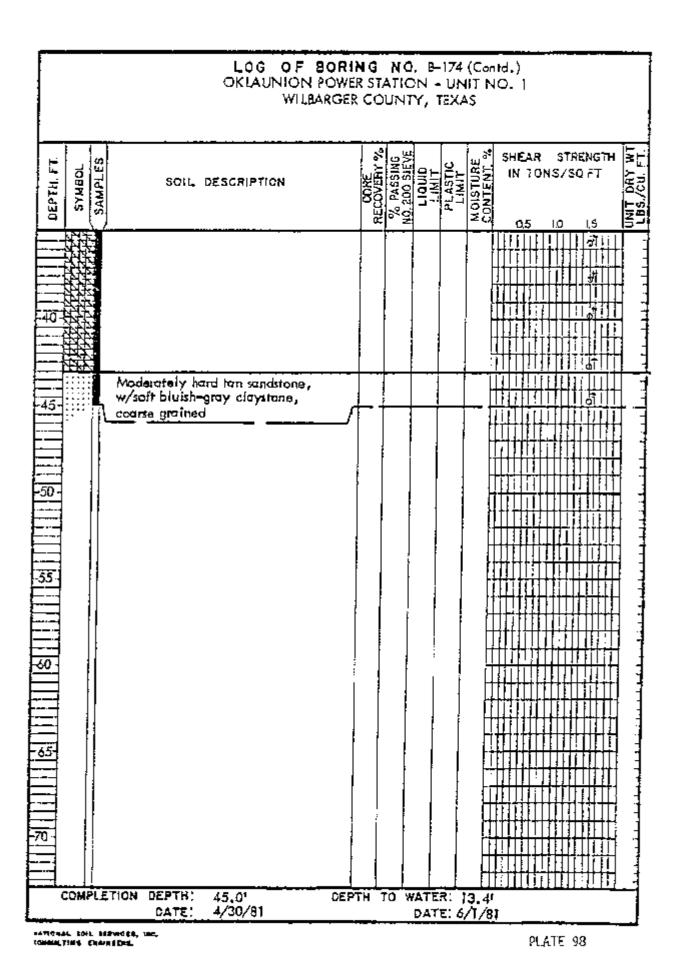
	LOG OF BORING NO. 8-173 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
TY	ÞΕ	80	RING: Undisturbed Sample and Core L	OCA	TION	<u>11,</u> 5e	e P!	an a	f 8ar	lnes,	Plat	e 3	
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: 1203.9	RQD %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	LIQUID	PLASTIC LIMIT	MOISTURE CONTENT, %	SHE	AR Tons	STRENGTH S/SQ FT	MIT DRY WT
		Ĭ	Hard deik brown silfy clay,							Πij		0 <b>i.5</b>	
			w/calcareous and magnesium nodules and numerous fine roots (CL) Hard reddish-brown silty clay,		100				<del></del>				
			increasing weathered calcareous (CL)  Soft reddish-brown clayey silt- stone, w/small bluish-gray clayey		98					       			1 1
			siltstone inclusions -slightly slickensided at 8.0' -w/increasing claystone lamina- tions, crassbedded at 11.0'		100								1
15		1	Soft reddish-brown silty clay- stone, w/bluish-gray silty clay- stone seam at 14.2-14.6'		95		<del> </del>						1111
			-w/accasional bluish-gray silty claystone inclusions and seams		96								***********
25				1	100							principal de la companya de la compa	
30 77 77 77	HOW HAND	1	crossbedded, w/numerous large luish-gray silty clayatone nclusions w/bluish-gray silty claystone eam at 33.0-33.51		co	:						1	
35	127				,								
(Continued)													
Mes/Mat Com	PERMITTORIAL SON SERVICES PLATE 95												

MATTORAL BOOL I (RYCCE), INC.

	LOG OF BORING NO. 3-173 (Contd.) OKLAUNION POWER STATION - UNIT NO. I WILBARGER COUNTY, TEXAS											
DEPTH, FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	RaD %	RECOVERY %.	% PASSING NO. 200 SIEVE	CIOUID LIMIT	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH IN TONS/SQ FT LONS/SQ FT LONS/CO LO LO LO LO LO LO LO LO LO LO LO LO LO		
40 45 55 55 70		The state of the s	-w/bluish-gray silty claystone seam, w/coarse send at 39.0-39.8  -w/cocasional bluish-gray silty claystone inclusions	73	80		JATE TO THE PROPERTY OF THE PR					
. (	COME	7.5	TION DEPTH: 50.0° DATE: 5/14/81	CEP.	TH 1	ro v	JATE DAT			/81		

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LOG OF BORING NO. 8-174 OKLAUNION POWER STATION - UNIT NO. 1														
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ļ														
ł	TY	PĘ	808 	NNG: Undisturk	ed Sample	<u>. LO</u>		( T			an o	T .	rings, Plate 3	
١	Ę	占	Sil.				% ≾.	RFT	PAE TEVE	•	ပ္ပ	]#E	SHEAR STRENGTH SHE	
Į	OEPTIR FT	SYMBOL	룈	SOIL DES	SCRIPTION	9	į	8	% PASSII	3	& ₹	ST	100	
	9	20	8	ELEVATION: 1198	. 6		RECOVER	BLOWS PER	%-S	[ <b>-</b> ] -	<u>a</u>	NO.	(1-0) 	
ŀ			¥	Hord reddish-bro		-		(2)		-			05 10 15 3-	
F		N	1	w/numerous fine	roots and					!				
Ė		$\sim$	¥,	-w/increasing we	•	4		_						
			) I	calcateous noduli	es at 3.0' (Cl	1/ر		i					<del>                                      </del>	
E	_5_		1	Hard reddish-bro		_ [			ı					
ŀ			<b>1</b>	-w/large weather	red calcaranus (Cl	سماس ک								
E			∦`	Soft reddish-brow	n silty	۳	o			ļ	ŀ	ļ	k: =5:0x10   gm/sec	
Ė	10-		3	claystone, w/bla gravel seam at 8.		8	٥		89	34	14	17	111111111111111111111111111111111111111	
þ		玆	3	w/numerous color		.	ļ	- ;	İ					
E		從		gravel pockets an	d occasional	<b>^</b>		ļ	]	ſ		}		
ŀ	=	採	3	iron stained inclu- -decreasing silt	sions	:	}	5)/5	ſ			ŗ	<del>;*;;\;;;</del> }++;;\;;\;	
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E	$\Rightarrow$		1	-w/occusional sol	1 bluish-gray			- 1	- 1	ł		1		
H	<del>10</del> ₹		1	claystone inclusio	ns	10	٥Į				ĺ			
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*	PLATE 97													



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	LOG OF BORING NO. 8-176 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS											
TYPE	80	RING: Undisturbed Sample and Care Li	OCA	TION	: Se	e 21	on o	f 3or	ings, Plate 3			
DEPTH, FT.	SAMPLES	SOIL DESCRIPTION ELEVATION: 1210.9	800 %	CORE RECOVERY %	% PASSING	dinoi.	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH M. TONS / SO FT. W. M. TONS / SO FT. W. M. M. M. M. M. M. M. M. M. M. M. M. M.			
	N	Very stiff reddish-brown silty			<del>  -</del>							
	V	alay, w/some fine sand and										
	N	calcareous nodules				ļ	l		·			
	$\mathcal{M}$	-hard, w/line gravel and calcareous nodules and			96	46	17	[13]				
- 5 - 14	76.1	magnesium nodules at 3.0' (CL)										
	, je	Soft reddish-brown silty clay-							<del>                                      </del>			
10000000000000000000000000000000000000	7	stone, thick bedded					ĺ		<u> </u>			
	45 45	1		1		ĺi						
1013	77	-w/numerous seams of bluish-		100								
	M.	groy silty claystone inclusions							╫			
					97	32	16	10	+++++++++++++++++++++++++++++++++++++++			
	R	-decreasing silt					' ]	-	<del>                                     </del>			
- 13	7	221,24311,3		100			-	;	<b>┼</b>			
15	N.							ſ	7			
		-crossbedded, slightly fractured				İ	}					
	FA FA	and w/some fine sand		į		]	į	ļ.	<b>┩╃╅┞┩╅┼┼╀┼┼╀┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼</b>			
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-25-		-w/clay laminations, lissured	[	100		1	ĺ					
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30-23	2	-w/bluish-gray silty claystone	Ì	icd			ĺ					
		seam at 29.5'							<u> </u>			
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<u>,</u>	LOG OF BE OKLAUNION P WILLAR	C)WE	てろけん	411C	<i>7</i> •7 ₹	. 014	(1)	
DEPTH, FT. SYMBOL SAMPLES	SOIL DESCRIPTION	RQD %		% PASSING NO. 200 SIEVE	FIMIT LIQUID	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH IN TONS/SQFT AND CONSTRUCTIONS CONTROL OF THE CONTR
	-w/numerous large bluish-gray silty claystone inclusions	76	92					
45 25 25 25 25 25 25 25 25 25 25 25 25 25		94	96					
50						2		
-60-								
\$								
CCMP	LETION DEPTH: 50.0' DATE: 5/8/81	DI	EPTH	T C	WA D	TER	: Dry	7 - Caved at 14-11 28/81 PLATE 102

NATIONAL BOIL SERVICES, INC. CONSULTING ENGINEERS.

	LOG OF BORING NO. 8-177? OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
TYPE BORING:	Undisturbed Sample (	OCA	TION	i : Se	e PJ	an o	f Bor	ings, Plate 3			
SYMBOL SAMPLES	SOIL SESCRIPTION	CORE FECOVERY %	BLOWS PER FT.	% PASSING NO. 200 SIEVE	Clubin	PLASTIC LIMIT	MOISTURE CONTENT, %	NIT DRY NIT DRY NEW TANK			
ELEVA	TION: 1207.3	╁			<u> </u>	╀╼		05i0(552_)			
Hard dacre	stiff dark brown silty clay, merous organic material (CL) reddish-brown silty clay, asing silt, w/occasional gravel and roots umerous weathered cal- (CL)	52									
	eddish-brown silty clay-		<u> </u>					<u> </u>			
stone, calear ca	w/numerous weathered reaus nodules bedded, w/occasional soft -gray silty claystone stions and inclusions at agovel seam at 10.0° addish-brown claystone, bedding, w/occasional uish-gray claystone	100 100 100 100 100 60		99	34	15	10				
<u> </u>	(Continu	red)	····		<u></u>						
COMBATING ONLINE SERVICES PLATE 103											

			LOG OF BORI OKLAUNION POWE WILBARGER	R ST	ATIC	- N	UΝ	IJΝ	
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	RECOVERY %	% PASSING NO. 200 SIEVE	LEGIO LEGIO	PLASTIC	MOISTURE	SHEAR STRENGTH LAND IN TONS/50 FT LAND LIN IN ION LIN
45.			-w/numerous soft bluish-gray clay- stone inclusions	100					
,	COM	PLE	TION DEPTH: 49.5' DEP DATE: 4/30/81	-TH	точ			3.8 /11/	

PATIONAL SME TORNICES, INC.

silly claystone inclusions		LOG OF BORING NO. B-178 OKLAUNION POWER STATION - UNIT NO. 1										
SOIL DESCRIPTION  BLEVATION: 1203.6  Very stiff brown silty clay, w/numerous fine roots and creanics  Were stiff brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Were stiff brown silty clay (CL)  Hard dark brown silty clay (CL)  Soft reddish-brown silty clay-  wy/occasional gravel and bluish-  gray silty clay inclusions  -w/some fine sand, fissured  ct 7.0'  Soft reddish-brown silty clay-  stene, thick bedding  -increasing silt, crossbedded,  w/some fine sand at 12.0'  -thick bedding  -increasing silt, crossbedded,  w/some fine sand at 12.0'  -thick bedding  -increasing silt  -decreasing silt  -decreasing silt  -w/small bluish-gray silty  claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions						·				ļ		
SOIL DESCRIPTION  SOIL DESCRIPTION  BLEVATION: 1203.6  Very stiff brown silty clay, w/numerous fine roots and caranics (CL)  Hard dark brown silty clay, w/weathered calcareous nodules readiles and accasional fine gravel at 4.0'	TYP	<u>ع</u>	SORING: Undisturbed Sample and Core L	OCA.	TION	: S	ee P	ал с	of Bo	rings, Place 3		
Very stiff brown silty clay, w/numerous fine roots and creanics  Hord dark brown silty clay, w/weathered calcareous nodules reddish-brown, w/soft pockets and accasional fine grave!  at 4.0'	DEPTH FT.	SYMBOL.			CORE RECOVERY %	% PASSING NO. 200 SIEVE		PLASTIC LIMIT	MOISTURE CONTENT, %	IN TONS/SQ FT AND/SQ LINE		
w/numerous fine roots and cranics (CL) Hord dark brown silty clay, w/weathered calcareous nodules -reddish-brown, w/soft pockets and accasional fine grave! at 4.0' -w/accasional gravel and bluish- gray silty clay inclusions -w/some fine sand, fissured at 7.0' Soft reddish-brown silty clay- stone, thick bedding -increasing silt, crossbedded, w/some fine sand at 12.0' -thick bedded, w/magnesium flakes at 15.0' -w/bluish-gray silty claystone seam at 16.5-16.8' -decreasing silt -increasing silt -increasing silt -w/small bluish-gray silty claystone inclusions  100 -w/accasional large bluish-gray silty claystone inclusions		Z					_					
-w/small bluish-gray silty claystone inclusions  -w/accasional large bluish-gray silty claystone inclusions  -w/numerous bluish-gray silty	10		w/numerous fine roots and arganics (CL) Hard dark brown silty clay, w/weathered calcareous nodules -reddish-brown, w/soft pockets and occasional fine gravel at 4.0' -w/accasional gravel and bluish- gray silty clay inclusions -w/some fine sand, fissured at 7.0' (CL) Soft reddish-brown silty clay- stone, thick bedding -increasing silt, crossbedded, w/some fine sand at 12.0' -thick bedded, w/magnesium flakes at 15.0' -w/bluish-gray silty claystone seam at 16.5-16.8'									
(Continued)	25 GA A A A A A A A A A A A A A A A A A A											

METANATIONAL, SON, SERVICES CONSULTING ENGINEERS

	LOG OF E OKJAUNION WILE	POWE	R 57	ATI	νс.	- UN	4FT 1	ntd.) NO. 1
OEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	ROD %	CORE RECOVERY?	% PASSING NO. 200 SIEVE	LIQUID	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH ALL IN TONS/SQ FT AUG/S LINE DE LES
	-w/clayey shale seem at 38.1-38.51 -extremely slickensided at 39.01 -w/occasional bluish-gray silty claystone seams	93	93					
COMPLE	TION DEPTH: 50.0° DATE: 5/11/81	DEPT	FH T	ю w	ATER DATE	₹: 6, :: 5,	[[ /5 <sup>;</sup> /11/	81

MATTOWAY SONE SERVICES, MIC.

P1 0TT 106

CONSULTING ENGINEERS

		LOG OF BORING NO. 8-179 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
SOIL DESCRIPTION  SOIL DESCRIP	TYPE BO	RING: Undisturbed Sample and Care L	OÇA	TION	l:Se	e Pic	an o	f Sor	ings, i	Plate 3		
Very stiff dark brown silty clay, w/numerous fine roots (CL) Hard reddish-brown silty clay, w/catcareous and magnesium nodules  -w/occasional large catcareous and magnesium nodules  -w/numerous bluish-groy silty ator inclusions (CL)  Saft reddish-brown silty clay- stone, crossbedded, w/occasional bluish-gray silty claystane inclusions  100  -thick bedded  -thick bedded  -thick bedded  -thick bedding -w/numerous large bluish-gray silty claystone inclusions	1 . I i	SOIL DESCRIPTION	35	RECOVERY %	% PASSINS NO. 200 SIEVE	L.IQUID LIMIT	PLASTIC LIMIT	OISTURE ONTENT %	SHEA IN 1	R STR	ENGTH 2 FT;	LAS /CU. FT.
Hard reddish-brown silty alay, w/calcareous and magnesium nodules  100  -w/cacasianal large calcareous and magnesium nodules  100  -w/numerous bluish-gray silty atay inclusions  Saft reddish-brown silty clay- stone, crossbedded, w/accasional bluish-gray silty claystane inclusions  100  100  100  101  101  101  101  1		Very stiff dark brown silty clay,								<del>niini</del>	1111	
-increasing silt  -thick bedded  -thin flat bedding -w/numerous large bluish-gray silty claystone inclusions		w/numerous fine roots (CL)  Hard reddish-brown silty clay, w/calcareous and magnesium nodules  -w/occasional large calcareous and magnesium nodules  -w/numerous bluish-groy silty clay inclusions (CL)  Soft reddish-brown silty clay- stone, crossbedded, w/occasional bluish-groy silty claystone		1 00 85							3 3 4 5 5	
	30	-thick bedded -thin flat bedding -w/numerous large bluish-gray									\$	المؤال المالم والمالم المنافيا المتطوع المهيز معالط ألمعتم
(Continued)		(Continu	ued)		<u> </u>	1	1		11111		<u> </u>	7

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	LOG OF OKLAUNION WILE		R ST.	ATIC	NC -	UN	iit N	
DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	RQD %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	LIGUID	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH ALL THE SHEAR STRENGTH ALL THE
	-w/bluish-gray stity claystone eam, w/coarse sand at 35.5- 16.3' -slightly slickensided -w/accasional high angle tractures	100	100					
45	w/accasional healed high ngle fractures	100	100				- +	
-55								
8								
-70	10N DEPTH: 50.0"	DEP	тн	10 W	STAN	R: (	5.7	
MATHEMAL BOIL CERT	OATE: 5/14/81						5/14	/81 PLATE 108

WE FRATIONAL SOR SERVICES

	LOG OF BORING NO. 8-180 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS													
77	PE :	i d F	RING: Undisturbed Sample L		_		_		Bori	nas,	Pla	te 3	J	
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: 1198.4	CORE RECOVERY %	PER (	% PASSING NO. 200 SIEVE	LIMIT	PLASTIC	MOISTURE CONTENT %	SHE IN	TON	STRI IS/SC	ENGTH OFT 15	UNIT DRY WT
	$\mathbf{H}$	1	Hard brown clayey silt,		<u> </u>				<u></u>		ĬII		φii	
		1	-w/numerous calcareous nodules and fine roots	<del></del> ,									<u> </u>	
5 -			-w/large calcareous nodules at 3.0'  Hard reddish-brown silty clay, w/numerous weathered calcaroous nodules -w/large calcareous nodules,	08		90	38	16	13				40 - 64	
-10-		X .	coarse sand, and medium to coarse gravel at 6.0'  -w/coarse gravel at 8.0'  Soft reddish-brown silty clay- stone, w/bluish-gray silty clay- stone inclusions		<b>20/3</b>								新 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
-20-				100			-						5	
	***************************************		-w/occasional high angle fractures -w/bluish-gray clay seam at	00					  -  -	<del>┇</del> <del>┇</del>				
30			24.5-25.5 <sup>1</sup> Hard reddish-brown silty clay		0/4"									
			-w/occasional bluish-gray silty clay inclusions (CL) Soft reddish-brown silty clay-	00				_	1		<del>                                     </del>			
35-1			stone, thin flat bedding	7	<del>-  </del>	_  -	Ť	- -						
			(Continue	d)										

	LOG OF BORIN OKIAUNION POWER WILBARGER	E STA	<b>LTIC</b>	)M -	UΝ	!T N	10.1
DEPTH. FT. SYMBOL.	SOIL DESCRIPTION	CORE RECOVERY %	% PASSING NO. 200 SIEVE	Uldul Ulmi:3	PLASTIC LIMIT	MOISTURE CONTENT, %	CO CO CO CO CO CO CO CO CO CO CO CO CO C
	-bluish-gray claystone, w/gravel at 36.0"	100					
40	Hard reddish-brown silty clay (C1)	100				-	
	Soft reddish-brown claystone, thick bedded	100					
	Very soft reddish-brown clayey shale, w/occasional small bluish- gray clayey shale inclusions	100					
-60-10-10-10-10-10-10-10-10-10-10-10-10-10	ETION DEPTH: 45.0' DEP	714		WATE	io. 1		

MATICULA, LOIL METHERS, AME

91ATE 110

$\lceil$	LOG OF BORING NO. 8-181 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
TY	۶E.	ВОЯ	ung: Undisturbed Sample L	OCA	TION	l∷_Se	e 21.	a <b>u</b> a	f Bor	ings, Plate 3	╝
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	CORE RECOVERY %	BLOWS PER FT.	% PASSING NO. 200 SIEVE	LIQUID	PLASTIC LIMIT	IDISTURE ONTENT, %	SHEAR STRENGTH A	BS./cu. FT.
<u> </u>		<u>(")</u>	ELEVATION: 7206.0	i de	<u> </u>	아			≆೮	0.5 LD 1.5 3	긔
- 5			Hard dark brown silty clay, w/calcareous nodules and numerous fine roots (CL) Hard reddish-brown silty clay, w/numerous weathered calcareous pockets and black		•						يبليينينيني
- 2-			gravel (CL)  Soft reddish-brown siltstone, w/thin gently dipped very soft claystone laminations -w/some coarse gravel at 8.0' -crossbedding at 8.3-8.7', w/occasional bluish-gray silt- stane inclusions	60	50/4°						
-15 -20-			Soft reddish-brown silty clay- stone, thick bedding, w/occa- sional bluish-gray silty clay- stone inclusions  -thin flat bedding	100	ar∕a.						
				100							<del>, , , , , , , , , , , , , , , , , , , </del>
	(Continued)										

Warnational Son, Structs Communication

	LOG OF BOR OKLAUNION POV WILBARGE	ver sta	ATIC	N -	UN	IT N	0.1
DEPTH. FT. SYMBOL	SOIL DESCRIPTION	CORE RECOVERY %	% PASSING NO. 200 SIEVE	LIGUD	PLASTIC	ALOISTURE	SHEAR STRENGTH ALL IN TONS/SQ FT AND LINE 0.5 IO 1.5
40-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	→lightly slickensided	100				Tanga Panasa Angara Angara Angara Angara Angara Angara Angara Angara Angara Angara Angara Angara Angara Angara	
55-							
	LETION DEPTH: 40.0' DEPTH: 5/6/81	EPTH 1	10 V			1.3.	BI ATE 112

	LOG OF BORING NO. 8-182 OKLAUNION POWER STATION - UNIT NO. 1										
			ARGER C						-, ,	1	
TY	먇	зония: Undisturbed Sample	L	DCA	TION	: Se	e 21a	en of	<u> 8∞r</u>	ings, Plate 3	
DEPTH. FT.	SYMBOL	SOIL DESCRIPTION	N	CONERY %	ROWS PER FT.	6 PASSING 3. 200 SIEVE	나보는	PLASTIC	OISTURE	SHEAR STRENGTH ALL	
	***	ELEVATION: 1203.7	-	REC	골	~5			ತನ	05 ID 15 34	
- 5 :		Hard brown silty clay, w/ roots, accasional coarse w and weathered calcareous nodules Hard reddish-brown silty o w/numerous weathered cal	and <u>(CL)</u> / :lay,							(b)	
		eous nodules  -extremely friable, w/fine gravel at 5.01  -w/some fine gravel and i nodules at 7.01  -w/occasional bluish-gray silty clay inclusions at 10, -w/bluish-gray silty clay	e Iron	100		99	40	20	12	(a)   50xil(0   cm//sec	
-15-5	沉	pockets	(CL)		seat						
		Soft reddish-brown silty all stane, thin to medium bedd w/numerous line roots	ding,	100		24	20	, ,			
20		-continuing bluish-gray po			37/5 seat	34	30	15	7   1   1   1   1   1   1   1   1   1		
-30-8		Very soft reddish-brown classical shale  -w/bluish-gray silty clay inclusions	· · · · · · · · · · · · · · · · · · ·	00							
35	<b>施雅</b>	Soft reddish-brown silty che stone, thick bedded -slightly slickensided		00							
									-  -  -		
,	(Continued)										

	LOG OF BORING NO. 3-182 (Cantd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS													
рерти, ят.	SYMBOL	SAMPLES	SOIL D	ESCRIPTION		CORE RECOVERY %	% PASSING NO. 200 SIEVE	Libur	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH XI IN TONS/SQ FT X80			
45 45 45 45 45 45 45 45 45 45 45 45 45 4			-very soft clays 38.5-40.0'	sy shale seam at		100								
	COM	PLE	TION DEPTH: DATE:	40.0' 5/5/81	DEI	тн	TO	PATE DAT	ER:C	σνακ 6/11	d at 7.51 1/81			

TYPE BORING: Undisturbed Sample  LOCATION: See Plan of Borings, Plate 3  SOIL DESCRIPTION  SOIL DESCRIPTION  BOOM SON SHEAR STRENGTH SIN TONS/SQ FT.  Hard brown silty clay,  W/weathered calcareous  and iron nodules  -reddish-brown at 3.0'  -w/occasional coarse sand and  fine gravel, w/some fine roots  at 4.0'  -w/fine gravel and iron stains  at 4.0'  -w/fine gravel and iron stains  at 4.0'  -w/coassional sluish-gray  silty claystane inclusions at 8.0'  -w/nomerous fissures  (C1)  Soft reddish-brown silty clay-  stone  -w/same sand at 13.7'  100  100				OKLAL	OG 0 PION P WILBA	OWER	STA	TTO:	<b>N</b> -	UNI	TN	0, 1	
SOIL DESCRIPTION  SOIL DESCRIP	->05 801	DING'	Undis	sturbed S	ample	Ĺ	OCAT	าดผ	: \$e	e Pla	ın of	Bor	ings, Plate 3
Hard brown silty clay,  w/weathered colcarecus  and iron nodules  -reddish-brown at 3.0'  -w/occasional coarse sand and fine gravel, w/some fine roots  at 4.0'  -w/fine gravel and iron stains  at 6.0'  -w/occasional cluish-gray  silty claystone inclusions at 8.0'  -w/numerous fissures  (C1)  Soft reddish-brown silty clay-  stane  -w/same sand at 13.7'  100  100			şoı	L DESC	RIPTION		RE ERY %					STURE TENT, %	SHEAR STRENGTH X 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
w/weathered calcareous and iron nodules -reddish-brown at 3.0' -w/occasional coarse sand and fine gravel, w/some fine roots at 4.0' -w/fine gravel and iron stains at 6.0' -w/occasional cluish-gray sitly claystone inclusions at 8.0' -w/numerous fissures (C1) Soft reddish-brown sitly clay- stone -w/same sand at 13.7' 100  100		ELEV			•		£.	盘				-	
-w/numerous fissures (CL) Soft reddish-brown silty clay- stone -w/same sand at 13.71  100  100		w/w and -red -w/ fine at 4 -w/ at 6	reather iron no dish-b occasion grave .0' fine grave .0' occasion	ed coloco odules rown at conal coa l, w/son royal and	areous  3.0' irse sand ne fine ro i fron sta	thoo ani	80						
stone -w/same sand at 13.7*  100  100		⊢ -w/	human	ous fissu	res (	(CL)/-	┼╾	-	ļ <u> </u>	<u>                                     </u>	-	<del> </del>	
-w/decreasing silt -w/occasional bluish-gray silty claystone inclusions  -crossbedded, w/some fine sand  100  100		Soft stan -w/ -w/ clay	decrea focasi vitone	sing silt and at I	isilty cla 3.7°	sî lty	100	Section 1					
(Continued)						(Cont	isue.	d١					

	LOG OF BORING NO. 8-183 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILLDARGER COUNTY, TEXAS														
DEPTH. FT.	SYMBOL	SAMPLES	SOIL	DESCRIPTION		CORE RECOVERY %	% PASSING NO, 200 SIEVE	LIQUID	PLASTIC	MOISTURE CONTENT %				/50	UNIT DRY WY
	<u> </u>	9	Very soft red	dish-brown clay	vey shale							₩	#	1	1
40			-w/occasiono	ri gravel		30	_			-					
	, <u>, , , , , , , , , , , , , , , , , , </u>														· ;;
45											╈┼┢ ╋┼┇ ╇┼┇				•
-50-											<del> - - -</del>  - - -  - - -				
-55										į					
-60															
65										-  -  -  -					
70-								'   							
				10.01		<u> </u>	-						<u> </u>		
•	COW	<i>-</i> 15	THON DEPTH: DATE:	40.0° 5/5/81	DEP	TH	10 '		FR:			ıt 3	.8		

NATIONAL BOIL REPORTS, INC. COMMUNICATION STREETS

9LATE 106

HES/HATIONAL NOW SERVICES COMMUNICATIONS

	LOG OF BORING NO. 8-185  OKLAUNION POWER STATION - UNIT NO. 1  WILBARGER COUNTY, TEXAS  TYPE BORING: Undisturbed Sample LOCATION: See Plan of Barings, Plate 3												
ŤΥ	ÞΕ	801	RING: Undisturbed Sample (	OCA	T:ON	<u> </u>	e Pla	n of	3or	ings, Plate 3			
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: 1198.3	CORE RECOVERY %	- I	% PASSING NO. 200 SIEVE	diupi i	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH IN TONS/SQFT. LA DE/SONG IN TONS/SQFT. LA DE/SONG IS 15 CO 15			
	$\mathcal{M}$	Ì	Hard tannish-brown clayey silt,	<del>!                                    </del>	1 44				-	05			
10-			Hard tannish-brown clayey silt, w/numerous calcareous nadules and fine roots (ML) Hard brown silty clay, w/numerous packets of calcareous nodules and gravel -w/numerous fine gravel at 4.0° -w/numerous medium to coarse gravel and weathered calcareous nodules at 5.0° (CL) Soft reddish-brown silty clay- stone, w/occasional calcareous filled fractures  -w/accasional soft bluish-gray silty claystone inclusions  -medium bedding		£1.5"	72	39	15		### 20 k3 U T c-m/sec   30   130 km / sec   30 km / sec   30   130 km / sec   30			
30 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3			increasing silt, crossbedded (Contin	+	75								
	_		CONT	.063	_								

	LOG OF OKLAUNION WILE	BORING POWER STA ARGER CO	AOIT/	1 - UN	III NO. I
DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	CORE PECCOVERY %	% PASSING NO. 200 SIEVE	PLASTIC LIMIT	SHEAR STRENGTH & TROUBLESON OF TO 15 OF 15
45	-thick bedded	100			
555					
50	-				
COMPLETIO	DATE: 5/4/81	DEPTH TO		ER: 9. TE: 6/	

Γ	LOG OF BORING NO. 8-186 OKLAUNION POWER STATION - UNIT NO. 1												
			WILBARGER							'			
1.	vae	20	RING: Undisturbed Sample L	200	TION	٠.٠	. 00		c D	ings, Plate			
}-	TE	i i	KING. Ondistgrad Somple C	3	1	1		30 0	30F		STREN	GTH.	] 
[		ES	SON DESCRIPTION	₩.Š	1 -	SING	8 E	윤	S L	IN TONS			<u>~</u>
DEPTH	SYMBO	SAMP	SOIL DESCRIPTION		alows PER	PASSII 200 SII		LASTI	125				ΔŌ
\ \frac{\pi}{2}	্	(%	ELEVATION: 1202.7	SFCOV	Į ģ	%5	_	٦	200	0.5 !!	3 I.S	5	雪
	-77	Ú	Hard dark brown silty clay,	Ī		-						71	-
	X	ď	w/weathered calcareous nadules	-	<del></del>			_		<del>╵╴╵╵</del> ╏┇┇		• <del>• • • • •</del>	
	W	N	(CL) / Hard reddish-brown silty clay							<u> </u>	11114	<u> </u>	1
	-0	N	-w/numerous calcareous filled		1					<del>┤┆┋</del> ┪╗┼┤	1111	<del>[</del>	
5	N	N	fissures and packets at 4.0°		-				Ì			111	3
	$\mathfrak{M}$	У	-w/accasional calcareous nodules and coarse gravel at 6.01	100	)						<del>!   </del>	<del> </del>	
	N	ď	-w/occasional bluish-gray silly	!						<del>┋</del> ┼┼┼ <del>╏╏┇┋</del> ┊┤	╂┼╁┼┤	╅	1
-10	N	ď	clay inclusions	100			<b>'</b>					<u> </u>	]
	N	XI	-								<u>         </u>	<u> </u>	1
	N								ŀ	┦┦ <b>╒</b> ┤╃ <del>┦┇╏</del> ┇	╼┋┼┼┞	<del>┊</del> ┠┠╅╴	
	77	ÇΧ	( <u>C</u> L)	ļ <u> </u>	<b>30/9</b>						<del>-          </del>	<del>╽</del> ┥╍╄ <del>╏╸</del>	
-15		$\mathbb{F}$	Soft reddish-brown claystone, thick bedded				ì				: [ ] [	Ш	]
	122 122	7						}	- }	<del>┋┇┇┋┋</del>	┊┼┨┼╂	╀┼┼	1
	12.	Ì	-w/accasional high angle fractures	100					ŀ		11111		=
	Z	3	-w/occasional bluish-gray clay-	ĺ		ľ	!						-
-20	<b>E</b>		stone seams and inclusions				i	ļ	-		╀┼┼┼	1	4
	7	3	-w/occasional high angle			-		İ	ŀ	╏╂╂╂┼┼┼┼┼	<del>┇┦┨</del> ╈		1
		2	fractures	100	1 1		ı		Ĺ				=
	2,2	Ĭ	_		<b>30/4</b> °	- 1		-	ļ	<del>┊</del> ┃╽┆┇┃┃┇╻	<del>                                     </del>	<u> </u>	- 1
-25			Far carryl> 26 01			ŀ			H	<del>╒╏┋</del>			-
	17	7	-fine grovel seam of 26.01					- 1					1
	77	Ì		100		İ	}	j	H		11.4	.	- [
	77						ı	-	H			╃╂┞╡	4
-30·	Œ					j	]					<u> </u>	4
	77				!	İ	-	-				Щ	
												~ <del>-</del>	
-25	Soft reddish-crown silty clay- stone, thick bedded, w/occa-												
-33													
		1	Stone inclusions		ļ				$\mathbb{H}$	<del>┞╏╏╏╏</del> ┩┪┪	╁╬╏		1
	-		(Continu	;ed)	<del></del>					<del>++++</del>	<u> </u>	. 111	7
1073/	1/MATONAL SOC. MERVICES.												
	WET.	T UNIX	CHOINCES							LEV	E 11:	-	

			LO 6 OK LA	OF BOF UNION PCV WILBARG	VER S	TΑ	IIC	)N -	UN	II N	td.) 40. T
DEPTH, FT.	SYMBOL	SAMPLES	SOIL DESCRIPT	TON	Lu oud and ig	Of DASCONS	NO. 200 SIEVE	LIMIT LIMIT	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH LANGER IN TONS/SQFT AND LANGE IN 15 15 15
40			-w/some selenitic cryst	1/s	30						
45-										, ,	
-50 ·											
80								ļ   			
-65-											
70- 	OMPL	ĔŤ	ION DEPTH: 40.0° DATE: 5/6/81	CEI	PTH	ŤŌ				V 0 0 0 1 1 / 8	ar 6.7'
PATTOMAL COMMUNICATI	904L	SERV MAE	ecie, 186, Sta	-							PLATE 120

	LOG OF BORING NO. B-190 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
<u> </u>	1P€	801	RING: Undisturbed Sample	Loc	OITA			lan e	of Bor	ings, Plate 3			
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	CORE	BLOWS PER FT	171	1.10 UID	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH ALL IN TONS/SQ FT. ALL			
		V	ELEVATION: 1198.0	-		2.5	<u> </u>		2Ω	0.5 1.0 1.5			
			Hard dark brown silty clay, w/numerous fine roots and calcareous nadules (CL) Hard reddish-brown silty clay,	<u>\</u>	<u> </u> 			 					
• 5			w/calcareous nodules -w/calcareous nodules and fine gravel at 6.0'	80									
	$\overline{N}$		-w/bluish-gray clay bails (CL)	80		100	35	16	10	27			
-10		GALERAKH K.	Soft raddish-brown silty clay- stone -w/clay balls	80	50/4								
-15-			Very soft reddish-brown clayey shale, extremely slickonsided	100		96	36	20	18	-3.90x101 cm/sac11e			
-20-		X	Soft reddish-brown sifty clay- stone, thick bedded, slightly slickensided	100	g0/3"								
25			Soft reddish-brown clayey shale, slightly slickensided	100									
199			Soft reddish-brown silty clay- stone, thick bedded -w/occasional large bluish-gray silty claystone inclusions	700									
	(Continued)												
100 / FC	TIONA	L SOAL	. Whereis							PLATE 121			

LOG OF E OKLAUNION F WILBA	OWE	₹ ST.	ATIC	)N -	· UN	III" N	10, 1
SYMBOL SANPLES SANPLES NOUTHINGS SANPLES	CORE RECOVERY %	GLOWS PER FT.	% PASSING NO. 200 SIEVE	LIMIT	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH XI.
-w/inclined iron stained seam at 39.6!  -4545555555-	100						
COMPLETION CEPTH: 40.0°  DATE: 5/5/81	0EPTH	TO		TER		/12/	81 PLATE 122

					100 05		131.5					
f				CKIA	LOG OF I							
i				UKUA	UNION POWE WILBARGE	ין כאיב כאים ל	4   ] ( A   ] (	.ν • ν		iιΝ	O. !	]
1					WILLIAMOC		(MN)	17, 1	EXA	3		
TY	ρĘ	905	ung:	Undĭsturbe	d Sample	Loc.	AT10	<u>N:</u> S	ee P	lan :	of So	rings, Plate 3
		ارما				, ,	% F					SHEAR STRENGTH
DEPTH. FT.	SYMBOL	AMPLES		C31) SEA			2	120	TIME!	읟	KE	IN TONS/SQ FT >
] [ ]	¥ .	Ы		SOIL DES	CAIPTION	ŽŽ.	Ş 3	86	33	PLASTIC	E E	CO
12	ŝ	8				CORE	MECOVERY	% <u>5</u>	<b>∦</b> ⊐	ᆲᆔ	NOS NOS NOS	<u>⊨</u> g
<u> </u>	444	7		ION: 1191.			2 급	J =			رکدر	0.5 1.0 1.5 5-
		Ĭ	Hord N	annish-brow	n clayey silt,		ļ	]	Ī	ļ		
ļ —	W	<b>3</b>	_roots	areous node	ules and fine (tur	ـــلم.	↓_	ļ	<u> </u>			
	W	4		Innishbrow	n silty clay	4			l			
	W	3	-w/acc	asional fin	e roots at 4.0"	10	n	62	28	14	11	4 1 62 x 1 1 i chi/sed 1 1 6
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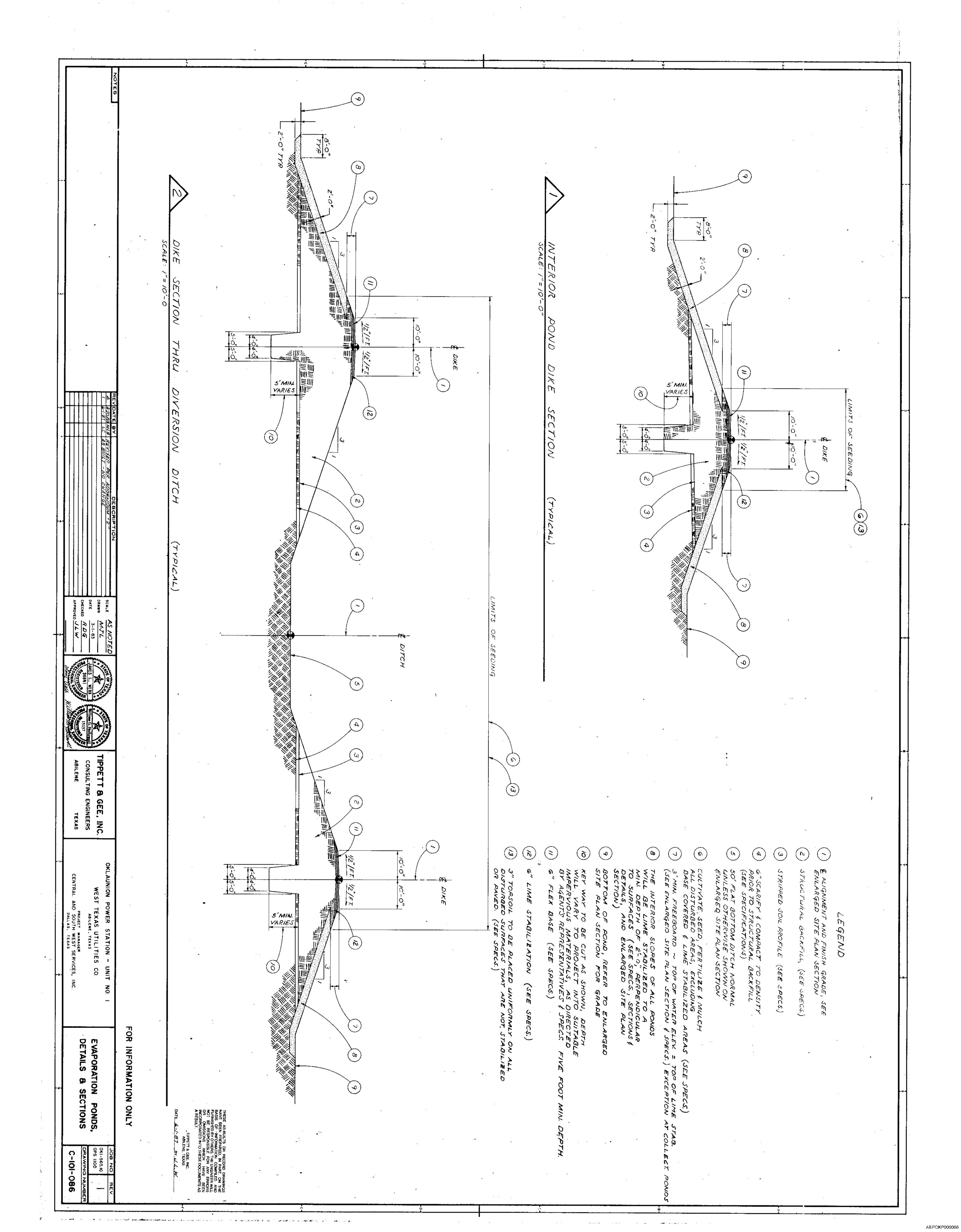
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	LOG OF BORING NO. 8-224 OKLAUNION POWER STATION - UNIT NO. 1										
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## APPENDIX A

# **Document 3**

Plans Pond Details 1



## APPENDIX A

# **Document 4**

Original Specifications

TIPPETT & GES, INC. CONSULTING ENGINEERS ABILENE, TEXAS

OK1-559,10 (OPS-1022)

CONFORMED AND CONTROLLED COPY

#### SPECIFICATIONS

£ 0 ₽

### PHASE I CONSTRUCTION (SITE PREPARATION)

#### OKLAUNION POWER STATION

UNIT NO.1

#### DIVISIÓN 1 - GENERAL

101. PROJECT DESCRIPTION

Central and South West Services, Inc., will construct a plant to be located in Wilbarger County, approximately four miles south of Oklaunion, Texas. The Jobsite may be reached by a fair-weather road. A vicinity map showing both road and railroad locations is given on page 1-2.

102. PROJECT DATES

The unit is scheduled for Commercial Operation on December 1, 1986.

103. EQUIPMENT/MATERIALS SUBSTITUTION

where specific brand names are used, they are a measure of quality only and equipment accepted as equal by Agent or Engineer may be substituted.

104. SITE CONDITIONS

Existing elevations are shown on the drawings. Solid lines are existing contours and dashed lines are proposed contours. Ambient temperature range is -5°F to 115°F. Seismic zone is '1".

201.02	Drawing Number	Revision	<u>Title</u>						
	C-102-073 C-102-074 C-102-075 C-103-023 C-103-024 C-103-025 C-103-026 A-110-001	0 0 0 0 0	Culvert Details Collection Pond Overflow Details Collection Pond Overflow Details Barbed Wire Fence Details Project Sign Elevation Sects. & Dets. Fence Details Fence Details Prefabricated Guard Building						
202 .	GENERAL SCOPE OF	efthition (c	ONTRACTOR)						
	scope of the Wor an itemized list tion of complete	rk under thi ting. Contr e facilities uirements of	to provide a general definition of the is Contract and shall not be construed as ractor shall be responsible for constructs conforming in all respects to the fithis Specification, Drawings and other						
202.01	Clearing and grubbing of ground surfaces within the construction areas as delineated on the Orawings.								
.02	Excavation, backfill, compaction and grading of generation plant area, chimney area, cooling tower area, switchyard area, perimeter fence area, pond areas, coal storage and handling areas.								
. 03	collection pond storage ponds as includes all exe	, one (1) ma nd ten (10) cavation, ba	cor collection pond, one (1) lower take up water supply pond, five (5) evaporation ponds. Pond construction ochfils, embankments, slope protection, outfall structures, and any required						
.04	roads and consti	ruction park Ation, lime	Trood subgrade, plant access roads, ing lot including all excavation, fills, stabilization, fly ash stabilization, culverts.						
.05	Final grading of struction to pro ground areas.	f all ground ovide unifor	l sunface areas disturbed by the con- me surfacing and effective drainage of						
.06	Construction of tainment areas.	diversion d	litches and required construction con-						
. 07	Supply and erect	t one (1) pr pundations	efabricated guard building complete with						

#### 401. JOBSITE WORK

#### 401.01 Applicable Codes and Standards:

All references to the following publications are to be latest issue of each, together with the latest additions and/or amendments thereto, as of the effective date of Contract. References to the sponsoring agencies will be made in accordance with the abbreviations indicated.

<u>ASIM</u> - American Society for Testing and Materials Standard Specifications

ACI - American Concrete Institute

AASHIO - American Association of State Righway and Iransportation Officials Standard Specifications

THO - Texas State Department of Highways and Public Transportation

TEX - Standard Specifications Texas State Department of Highways and Public Transportation, Test Method

#### ,02 Lines and Grades:

Contractor shall employ a competent, licensed land surveyor to determine lines and elevations.

Contractor shall lay out lines and grades from existing property lines and bench marks on the Jobsite and be fully responsible for correctness of such lines and grades and for proper execution of the Work to such lines and grades. Contractor shall correct at its own expense all errors in the Work arising from its inaccuracy.

Agent reserves right to verify correctness of lines and grades during progress of the Work. Such verification by Agent will not relieve Contractor of its responsibility.

Contractor shall preserve and maintain all bench marks and reference points established by Agent. Should Contractor, during execution of the Work, destroy or remove any bench marks and/or reference points established by Agent, the cost to Agent of reestablishing these bench marks and/or reference points will be charged to Contractor.

### 401.03 Surface Preparation:

Prior to performing excavation or fill work, the ground surfaces within the construction area shall be cleared, grubbed and the top-soil removed.

401.03

a. Clearing:

Clearing is defined as removal and disposal of all trees, down timber, snags, brush, hedges, bushes and all other vegetation or organic materials, and also all rubbish, debris or other foreign or objectionable materials above ground surface, except removal of sod and topsoil.

ъ. Grubbing:

Grubbing is defined as removal and disposal of all stumps, large roots, buried logs and all other objectionable material from below ground surface. Explosives may be used only if specifically approved and their use shall conform to all applicable laws and safety regulations.

c. Disposal:

All materials from clearing and grubbing operations shall be promptly removed from the construction area and disposed of by and at the expense of Contractor. Accumulation of such materials on premises is not permitted. If Contractor desires to burn materials, the obtaining of a burning permit from the appropriate regulatory authorities shall be Contractor's responsibility.

d. Removal of Topsoil:

Topsoil in areas to be excavated or filled shall be removed, stockpiled and saved at various locations on the Jobsite near where it is to be reused. The depth of topsoil to be excavated or stripped is estimated to be six to twelve incres in depth. Stockpile locations shall be approved by Agent. Topsoil shall be carefully stripped, placed in stockpiles and kept clean and free of all foreign material. Topsoil shall be utilized where indicated on the Drawings and required by this Specification (reference Section 404.02, c.).

401.04 Excavation:

Excavation is defined to include all incidental clearing, all disposal of excavated materials, all protection, sheeting, shoring, bracing, all dewatering, and preparation of bearing areas as required to properly install and complete the Work, regardless of portions of Work for which required, and regardless of nature of materials, encountered in excavating.

401 04

a. Protection and Support:

Banks at excavations shall be protected and supported, where necessary or where requested, so that the banks and bottoms will be maintained and adjacent structures or other construction will be protected from damage caused by an earth movement.

b Bearing Areas:

- b.01 Bearing areas for all foundations shall be inspected and approved by Agent before any concrete 's placed. If bearing areas are not suitable, Contractor may be requested to carry the excavations desper to more suitable bearing material.
- .02 All foundations shall be placed on undisturbed soil unless otherwise indicated or approved.
- 401.05 Structural Backfill:

Structural backfill includes general backfilling around all Work excavated by Contractor, and also all other backfill indicated on Drawings as by Contractor. All backfill or ordinary fill shall be classified as structural backfill as defined herein unless indicated otherwise on the Drawings.

a. Material:

Unless indicated otherwise on the Drawings, all backfill material shall be approved materials previously excavated at the Jobsite or materials obtained from approved borrow pits and shall be free of sod and topsoil or other deleterious or foreign matter. This material shall be approved by Agent.

b. Compaction:

Backfill shall be built up to the grade elevations indicated on the Orawings or as directed, with suitable moisture control and compaction throughout placing. All backfill soils and embankments, unless indicated otherwise on the Orawings, shall be compacted equal to or greater than 95 percent of the maximum dry unit weight as defined by the Standard Compaction Test (ASTM D-698) for plastic clays and the TRD Method (TEX-113E) for sandy clays, clayey sands, silty sands and sands. The moisture content may vary from two percent dry of optimum to four percent wet of the optimum when compacted. The thickness of backfill lifts shall not exceed 9".

401.05

c. Inspection and Testing:

Contractor shall perform all backfill testing necessary to ensure the Work meets the specified requirements. Agent will conduct a quality control test monitoring program in addition to Contractor's basic testing program. Failure of backfill to meet the specified densities will be cause for rejection, and Contractor will be required to remove and replace all backfill not meeting these requirements at no additional cost to Agent.

d. Backfill Sand:

Backfill sand shall be a free-flowing clean sand of fairly uniform gradation. Clay and soil content shall be absent in any quantities that in the opinion of Agent makes use of the material undesirable. The sand shall be vibratory compacted greater than 95 percent of the maximum dry unit weight obtained using THO Compaction Test Method (TEX-1138).

e. Embankments:

Embankments are defined as any fill section. This definition includes the pond embankments, railroad embankments, road embankments or any area requiring a build-up of soil.

Prior to construction of any embankment, the foundation area shall be stripped to remove the topsoil, roots and weak surface soils. The stripping depth will be six to twelve inches, except in areas of uneven topography or in existing stock ponds and gullies. For these areas it will be necessary to strip to a deeper depth to remove the excessively wet and weak soils. All stumps and large roots shall be removed to a depth of two feet. All stripped areas shall be inspected by the on site testing laboratory and Agent's representative to determine if additional excavation is required to remove weak or otherwise objectionable materials that would adversely affect the intended integrity of the embankment.

After completion of stripping, the exposed soils shall be scarified to a depth of nine inches; the moisture shall be adjusted to two to four percentage points above optimum, and the soils recompacted. The optimum moisture value, compaction density and construction of embankment shall be as defined in the Structural Backfill Section 401.05 of this Specification.

f. Out and Fill Slopes:

All slopes except pond slopes shall have a maximum inclination of 2.5 horizontal to 1.0 vertical or as indicated on the Drawings.

401.05 f.

All exposed slope surfaces shal! be cultivated, seeded and mulched as defined in the Seeding Section 404.02.

401.06 Grading:

Consists of rough grading and finish grading as follows:

a. Rough Grading:

Cut, fill, spread and level during course of Work to elevations indicated.

b. Finish Grading:

After all excavation, backfill, compaction and rough grading has been completed, all ground surface areas disturbed by Contractor shall be finish graded. The grading shall be finished to the contours and elevations indicated on the Grawings and shall provide a smooth uniform surfacing free of debris, foreign matter, objectionable stones, clods, lumps, pockets or high spots and properly drained to provide effective drainage of the ground areas. Finish elevations shall be within two inches (plus or minus) of those elevations shown on the Drawings in all areas except the power block (turbine generator area, boiler, scrubber, and chimney) and the switchyard area. Finish elevation for the power block and switchyard area shall be within one inch (plus or minus).

An excess of backfill materials is anticipated. This excess material shall be utilized in a manner acceptable to Agent. The excess backfill shall be placed at locations approved by Agent. Disposal areas that are proposed by Contractor and approved by Agent shall be shaped, compacted and seeded as directed by Agent. Disposal areas that affect pond capacities or plant operations will not be approved. Seeding and compaction of backfill shall be included in the total Contract Price. Unit prices are not applicable to the disposal of excess backfill.

401.07 Pand Construction:

Pond construction shall conform to the shapes, locations and dimensions as shown on the Drawings, to this Specification and the items described as follows:

a, Criteria:

Construction of all ponds shall conform to current criteria established by the Texas Department of Water Resources (TBWR) relative to waste ponds.

401.07

ъ. Slopes:

Interior and exterior slopes shall be no steeper than 3.0 horizontal to 1.0 vertical.

#### c, Pend Battoms:

Elevation of pond bottoms for the evaporation ponds, makeup supply gond and the collection ponds are indicated by existing contours or excavated to elevations shown on the Drawings - whichever is lowest. The finish grades or elevations of pond bottoms for the five (5) storage ponds shown on the Drawings reflect finish grades

Pond bottoms in cut areas shall be scarified to a depth of nine inches. The moisture content shall be adjusted to between two to four percentage points above the optimum value. Then the scarified subgrade shall be compacted. The optimum moisture value and compaction density shall be as defined in the Structural Backfill Section 401.05. Within 48 hours of compacting the pond bottom, a 12-inch layer of semi-compacted clay shall be spread over the entire bottom of each pond bottom in cut areas only to preserve the moisture content of the subgrade. Semi-compacted clay is defined as being greater than 90 percent of the maximum dry unit weight as defined by THO test method TEX-1138. The top of the semi-compacted clay shall be set at finish grade; therefore, for cut areas, Contractor shall overexcavate pond bottoms one foot to properly achieve finish grade.

### d. Pond Embankments:

Pond embankments shall be constructed as defined in the Embankments Section 401.05.

## e. lime Stabilization of Slopes:

The slopes shall be lime stabilized as indicated on the Crawings. The percent lime and method of placement of lime shall be as defined in the lime Stabilization Section 404.03. The lime stabilized materials shall be placed in lifts such that the thickness of the lime stabilized materials is two feet measured perpendicular to the slope.

#### f. Seeding:

The pond slopes shall be seeded as indicated on the Drawings and as required by this Specification. The seeding shall be as defined in the Seeding Section 404.02

401.07

g. Pervious Soils:

All pond bottoms and side slopes must have a permeability coefficient less than 1 x 10  $^{\prime}$  cm/sec. Out of numerous permeability tests conducted during the initial soils investigation only one \_7 site demonstrated a permeability coefficient greater than 1 x 10  $^{\prime}$  cm/sec and was considered pervious.

in the event that zones of pervious scils are disclosed in the pond bottoms or side slopes, these pervious zones must be removed by overexcavation to a depth of two feet and replaced with impervious materials. The placement and compaction of these impervious naterials shall be as defined in Structural Backfill Section 401.05. The total contract price shall provide for excavating 50,000 cubic yards of pervious materials and replacing with 50,000 cubic yards of impervious materials. Unit prices shall be utilized for quantities above or below the 50,000 cubic yards that is included in the total Contract Price. The unit prices per cubic yard means to excavate one cubic yard of pervious materials and replace with one cubic yard of impervious materials.

401.08 Erosion and Sediment Control Requirements:

Contractor shall implement erosion and sediment control procedures as defined herein and shown on the Orawings.

a. Limitations:

The rainfall runoff from construction activities has the following limitations: 1) Total suspended solids - daily maximum of 50 milligrams per liter and 2) pH - between 6.0 and 9.0.

Contractor is required to conduct earthwork operations in such a manner than these limitations are met. To meet these limitations, Contractor shall comply with the following procedures:

ъ. Procedures:

Contractor shall conduct earthwork operations in the following sequence:

b.01 First - Contractor shall construct the three diversion ditches.

Currently, approximately 150C acres of surface area off the Jobsite drain through the Jobsite. Also, there is considerable acreage in the Unit No. 2 evaporation pond area that will be unaffected by Contractor. These areas must be allowed to flow through the plant site unimpeded and unaltered.

401.08 5.02 Second - Secondly and concurrently to the first procedure, Contractor shall construct improvement to the diversion ditches to force certain area runoff into the diversion ditches. Accordingly, it is necessary to construct some of the access road with drainage structures to allow drainage of the Unit No. 2 evaporation pond area into diversion ditch number 2. It is also necessary to construct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the railroad berm in Sections 42, 44, 45, 56, struct a portion of the Jobsite to flow into the flow through the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the force runoff water from the west of the Jobsite to flow into the Jobsite to flow into the Jobsite to flow into the Jobsite to flow into the Jobsite to flow into the Jobsite to flow into the J

- 163 Third Contractor shall construct the makeup water supply pond, the upper and lower collection ponds, evaporation pond number 4 and other ponds sufficiently to allow their use as sediment ponds. Contractor shall add temporary construction berms and diversion ditches as required such that runoff from all earthwork activities would drain into one of these ponds. Contractor may also install permanent drainage features as necessary to achieve these drainage/collection requirements.
- .04 <u>Fourth</u> Contractor can then execute any required earthwork activity if the rainfall runoff is directed into one of the sediment ponds.
- c. Pumping Requirements:

As water and sediment builds up in a particular sediment pond and the water has been clarified (contains less than 50 milligrams of suspended solids per liter) and as directed by Agent, it shall be pumped out by Contractor. The water shall be pumped into a diversion ditch or an existing stream that leaves the Jobsite.

Additionally, Contractor shall cooperate with Agent by pumping water between sediment ponds if required and as directed by Agent.

d. Cleanout of Sediment Ponds:

When all Work has been completed, Contractor shall pump out sediment ponds after they meet the required limitations and remove sediment if necessary to establish the required pond bottom elevations. Spoil areas for sediment shall be determined by Agent.

404.02 d.

Sideoats Grama (El Reno) and 5 pounds per acre of Caucasion Bluestem.

e. Fertilization:

Fertilizer rates, seed purity, and seed germination rates will be in accordance with current THO Specifications, Item 164 and Item 166. The fertilizer shall have an analysis of 16-20-0 and shall be applied uniformly at the average rate of 300 pounds per acre.

404,03 Lima Stabilization:

Where indicated on the drawings line stabilized materials shall be provided in accordance with the following procedure:

Excavate the existing clay soils to the depth indicated on the drawing and stockpile the excavated material.

Scarify the top six inches of the subgrade to receive lime stabilized materials, add moisture as required and compact to a density not less than 95 percent of the maximum dry unit weight as defined by the THD Compaction test. (TEX-113E) and ASIM D-698. The moisture content should be between optimum and four percent above aptimum at the time of compaction.

Treat the excavated clays with the required percentage of lime, (approximate)y 4% by dry weight) add water as necessary, and recompact at a moisture content between optimum and four percent above optimum, as defined by the THD compaction test, TEX-113E and ASTM D-698. The fills should be placed in loose lifts not exceeding nine (9) inches in thickness and compacted to a minimum density of 95 percent of the maximum as determined above. Failure to have adequate moisture content during mixing and compaction shall be cause for rejection of the Work.

Lime treatment (pulverization, incorporation of lime, repulverization, curing, etc.,) shall be accomplished in accordance with the applicable provisions of Item 260 of the THD Standard Specifications for Construction of Righways, Streets, and Bridges, 1972 Edition.

Seal the treated area of road beds and foundation areas with an asphalt membrane using .40 gallons of asphalt per square yard of surface - if the lime stabilized materials are to be left exposed for more than seven (7) days. Sealing with asphalt is not required for the lime stabilization areas on pond slopes.

Troth

## DIVISION 6 - GEOTECHNICAL INFORMATION

OK1-559.10 (OPS-1022)

#### 601. GENERAL

Agent has previously conducted a subsurface soil investigation. This section provides Contractor with information pertaining to the results of that investigation.

### 602. POSSIBLE HARD MATERIALS

The subgrade soils are hard. These soils may prove difficult to excavate and difficult to use as backfill materials. From the soil borings operations, it is anticipated that ordinary earth moving equipment can excavate the materials without blasting, even though blasting may prove advantageous to Contractor. It also appears that these hard soils should break down rapidly when exposed to sunlight and could then be broken apart and used as backfill material.

It is incumbent upon Contractor to satisfy himself as to his ownability to excavate and compact these hard soils. Arrangements can be made by Contractors to bring equipment on site to experiment with these soils prior to submitting proposals.

## 603. GEOTECHNICAL DATA

- At the end of this section there are copies of the borings made at the Jobsite. The location of the borings are shown on the Drawings. This information is furnished for Contractor's convenience. Contractor will be permitted to make his own soil investigations, but same shall be made at no cost to Agent.
  - .02 From these logs, Contractor should determine the materials which Contractor will be excavating and compacting, apparent water table levels, possible sources of usable backfill materials and other pertinent information associated with his different construction techniques.
- 603.03 The following information is included hereinafter:
  - Rock and soil classification.
  - Maps of boring locations.
  - various soil profiles.
  - Boring numbers.

603.04	The following	is a listing of the boring i	logs which follow:
	B- 101P	8-155	8-203P

-	
B- 101P	;
B-102	·
B-103P	
B-104	
B-105P	
B-106	
8-107P	
8-108 8-1092	
B-114	•
B-116	
B-I17	ì
B-118P	Í
B-119	
8-120	£
8-122	
B-123	ŧ
B-125	1
B-126 B-129	ì
8-131	
8-132	{
9-132 8-134	È
B-135	
B-136	E
B-137P	E
B-138	[
B-139	Ē
8-140 8-141	9
3-142	6
8-143	
3-144	ě
B-145	Ē
B-146	В
B-147	3
8-149	В
8-150 8-151 8-152	В
3-131 2-152	B
J-194 2-163	8 8
3-153 3-154	B

8-155	8-203P
8-156	8-204
B-157	8-205
8-158	8-206
8-159	8-207
8160	8-208
8-161	8-209
8-162P	8→210
8163	, B-211
B-164	B212
8-165	8-213
8-156	8-214
B-167	8-215
8-168	B-216
8-169P	8-217
B- 170	B218
8-171	8-219
8-172	8-220
8-173	8 <del>-</del> 221
8-174	B-222
8-175	B-223
a-176	B-226
B-177P	8-225P
8-178	B- 226
B-179	
B-180	8-227
B-181	B-228
	B-229
B-182	8-230
9-183	8-231
6-185 2-186	8-232
8-186	8-233
8-190	B-234
8-192	8-235
8-193	3-236
B-194P	3-237
3-195	8-239
B-196	B-240
B-198	B-241
B-199	B-242
8-200	8-243
8-201	8-244
8-202	

	LOG OF BORING NO. 8-108											
OKLAUNION POWER STATION UNIT NO. 1 WILBARGER COUNTY, TEXAS												
TYPE BORING:Undisturbed Sample	and Core Lo	OÇA"	TION	II Se	e Pf	an o	f 8or	ings, Plate 3				
SAMPLES SAMPLES SAMPLES SAMPLES		#qp %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	Liguid	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH A LANGE OF LANG				
Very stiff reddish-brow	m silty	_		-				05 10 15 3-1				
Soft reddish-brown same fine grained, thin bedden we numerous soft bluish sandstone laminations a inclusions at 6.0°.  Soft reddish-brown silts flat bedding, we numerous bluish-gray siltstone inclusions at 6.0°.  Soft reddish-brown silts gantly dipped bedding a clayey at 13.0°.  -high angle fractures  -soft reddish-brown clay seam, thick bedding from 20.7°.  soft bluish-gray sandy seam from 20.7-21.0°, grave!	calcareous nodules at 3.0° (CL)  Soft reddish-brown sandstone, fine grained, thin bedding  -w/numerous soft bluish-gray sandstone laminations and inclusions at 6,0°.  Soft reddish-brown sillstane, thin flat bedding, w/numerous soft bluish-gray siltstone inclusionssoft bluish-gray siltstone seams, gantly dipped bedding at 11.0°.  -clayey at 13.0°.  -inje angle fractures  -soft reddish-brown claystone seams, fine flat bedding from 18.0-20.7°.  -soft bluish-gray sandy claystone seam from 20.7-21.0°, coarse gravei  -soft bluish-gray sandy claystone seam, w/fine gravei from 27.5-  28.5°  Very stiff reddish-brown sifty clayst stiff reddish-brown sifty clay											
- NOV	sifty	+	-			+	- ! !	[]				
clay	(C1)	$\frac{1}{1}$	1				Ī					
Soft reddish-brown clays thick bedding, w/occasi soft bluish-gray silty cla inclusions	onal											
(Continued)												
WS/MATIONAL SOIL SERVICES COMMUNICATION ENGINEERS	<u> </u>	-				_		PLATE 24				

	LOG OF BORING NO. 8-108 (Cantd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
ОЕРТН. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	RQD %	CORE RECOVERY*2	% PASSING NO. 200 SIEVE	LIGUID	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH ALL OF IN TONS/SQ FT. MO/SQ FT.	
40			-w/numerous high angle fractures at 35.0'	79	80						
15			-w/numerous high angle fracturessoft clayey shale seam from 43.0-44.0*								
2)			-soft bluish-gray claystone seam from 44.8-45.1' -w/numerous high angle fractures	70	300				- - - - -		
5 5			-extremely slickensided								
			-soft bluish-gray claystone seam, w/fine gravel from 57.0-57.6' -w/numerous slickensides,	93	100						
15 15 15 15 15 15 15 15 15 15 15 15 15 1			indurated -w/numerous high angle fractures	97	100						
	777777				100			_	-  -  -  -  -		
(Continued)											
447]0844 COMBNI, 7:	PLATE 25										

SOIL DESCRIPTION  SOIL DESCRIP		LOG OF BORING NO. 8-108 (Canid.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
stone inclusions —moderately herd bluish-gray clayey silistone seam at 73.3- 74.6¹ —moderately hard reddish-brown, indurated, w/accasional moderately hard bluish-gray silistone inclusions and numerous fractures  -slightly slickensided, w/high angle fractures -very soft clayey shale seam at 85.1-85.8¹  Very soft reddish-brown clayey shale, w/soft reddish-brown claystane interbeds to 97.0¹  84 100	DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION		PECOVERY %	% PASSING NO. 200 SIEVE	Clouid Likit	PLASTIC	MOISTURE CONTENT, %	IN TONS/SOFT X:00/SE			
101 CT 10		moderately hard bluish-gray clayer sillstone seam at 73.3-74.6' -moderately hard reddish-brown, indurated, w/occasional moderately hard bluish-gray sillstone inclusions and numerous fractures  -slightly slickensided, w/high angle fractures -very soft clayer shale seam at 85.1-85.8'  Very soft reddish-brown clayer shale, w/soft reddish-brown clayer alloystone interbeds to 97.0'	91	100								
COMPLETION DEPTH: 101.0'   DEPTH TO WATER: 3.0'   DATE: 4/25/81   DATE: 5/2/81   PLATE 26			DEP1	H 1								

LOG OF BORING NO. 8-167 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS	
TYPE BORING: Undisturbed Samole LOCATION: See Plan of Borings	
SAMPLE SOIL DESCRIPTION  RECOVERY  RECOVERY  RECOVERY  NO. 200 SIENS  RECOVERY  LIMIT  LIMIT  ROUSTURE  LIMIT  LIMIT  ROUSTURE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  LIMIT  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  OM TENTIFE  ASSIMO  ASSIMO  OM TENTIFE  ASSIMO	EAR STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE STRENGTH ST. IONS/SQFT AND SMILE ST. IONS/SQFT AND SM
Herd dark brown silty clay, w/small weathered calcareous nadules -readish-brown at 4.0' -w/numerous calcareous and magnesium nodules at 5.0' (CL) Soft reddish-brown silty claystone, thin gently dipped bedding -decreasing silt -10 -crassbedded, w/bluish-gray silty claystone seam at 2.0-9.3'  -thick bedded  100  -thin flat bedding -thin flat bedding -20 -35-	
COMPLETION DEPTH: 25.0' DEPTH TO WATER: Caved at 2.2'	
DATE: 6/23/91	
	TE 85

	LOG OF BORING NO. 8-168 OKLAUNION POWER STATION - UNIT NO. I WILDARGER COUNTY, JEXAS													
					•									
17	TYPE BORING: Undisturbed Sample LOCATION: See Plan of Sorings, Plate 3													
DEPTH. FT.	SYMBOL	AMPLES	SOIL DESCRIPTION	COVERY %	200 SIEVE	LIGUID	LASTIC	NYENT 9			R . SNC			T DRY WT S./cu. FT.
Ľ		(")	ELEVATION: 1194.8	£	ళ్ళచే			38		Ģ5	- 1.	2	1,5	35
			Hard light tan to brown clayey siit,	_	87	43	14	17			<u> </u>		<b>1</b>	115
		1,	w/numerous fine roots (ML) / Hard brown silty clay		8/	43	1-4-	: ! !			111			a''
		1	-w/numerous calcareous nadules at 3.0°							1		$\prod$		
5		1	-light brown, w/calcareous and							<u> </u>	†#	<del>     </del>		
		7	magnesium nodules at 5.0° -reddish-brown, w/numerous pockets			ļ			$\prod$	11	<u> </u>	$\prod$	<b>P</b>	]
		Ĭ	of weathered calcareous material						H	+++	<del>         </del>	╫		1
-10-	M	3	and fine sand at 7.0' -w/occasional magnesium nodules	!					Щ	ij		Щ		] ]
			and bluish-gray silty clay				j		₩			╁╁	<del>┇</del> ┇┇┇	-
	W	1	inclusions at 9.0"w/calcateous Filled fissures and		۱	Ì	Ì	ļ	#	ij	Щ			] ]
	$\mathbb{N}$	Ĭ	7 mail: 12 mail: 17 /04	100	•			ļ	╫	╬	<b>. !</b>   !	╁┼┼		
15	<b>X</b>		Soft raddish-brown silty claystone,		$\neg$				Ш	ijį	Ш	ПÌ		13
	翻		thin flat bedding, w/occasional				İ	}	╫	╁	<del>                                     </del>	╁╂┼		┦ ∄
	177 172		bluish-gray sifty alaystone inclusions				ł	ļ	##	#				1 1
20-			-crossbedded, w/occasional pyrite	100	•		j	į į	<u>  [                                   </u>	<del>!                                    </del>	<b>!</b>	H	d	1 1
	挺			! <b> </b>		į			Ш	$\parallel$	<b>*</b>			] ]
	X		-thin flat bedding, w/occasional	ĺ	i	[	Į	ŀ	:		╁┼┼╁		╀┼┼	- 4
	猫	L	codrse sand pockets	60					<u> </u>	<u> </u>		Ш	<b>3</b>	1 1
	A.									┇╂╬┑		Ш	<u> </u>	
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	İ			ŀ				-	∭		#	Ш		]
-35-				ı		-	]	H	#	111		╫	<u> </u>	
										<u>†</u>		∭		
	COMPLETION DEPTH: 25.0' DEPTH TO WATER: 5.0'													
			DATE: 5/15/81	144		DAT		5,	/15,	/81				
A8757 NJ CO	PLATE C6													

LOG OF BORING NO. 8-170 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
*YPE_BORING:Undisturbed_Sample_and_Core!			-			F Para	rings, Plate 3			
SYMBOL SYMBOL SAMPLES SAMPLES	ROD %	SEE ERY %	PASSING 200 SIEVE	LIGUID	LIMIT	OISTURE	SHEAR STRENGTH X			
ELEVATION: 1213.0	, "	<u> </u>	%.5			38	0.5 LO (5 379)			
Hard brown silty clay, w/fine roots -reddish-brown, w/occasional coarse sand and fine gravel, w/weathered calcareous nadules  (CL)		100								
Soft reddish-brown silty clay- stone, w/numerous large bluish-	d	<del>-</del> —			- <del>!</del>	$\dashv$				
gray silty claystone inclusions,		100 -					+++++++++++++++++++++++++++++++++++++++			
w/some fine sand   10-2-15   Hard reddish-brown silty clay,   somewhat friable (CL)   Soft reddish-brown silty clay-		100								
stone, crossbedded, w/occasional bluish-gray silty claystone inclusions -rossbedded, w/occasional	<u> </u> 	100				-				
bluish-gray silty claystone laminations and very soft clay- stone and increasing silt at 14.0'		100	į							
-w/numerous yellow inclusions, thick bedded, decreasing silt		100				 				
-w/bluish-gray silty claystone		100				-  -  -  -  -				
seam at 30.1–30.4'  w/coarse sand and fine gravel to 33.0'										
Soft recidish-brown silty shale,  w/occasional bluish-gray silty shale inclusions	85	100		-	1	-				
						}	111111111111111111111111111111111111111			
(Cont	inua	d)								

AFS/HATIONAL STR. SERVICES CONSELISE DAMNERS

	LOG OF BORING NO. B-170 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS									
DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	RQD %	CORE RECOVERY%	% PASSING NO. 200 SIEVE	LIGUID	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH S	LBS./CU. FT.	
10 stor	reddish-brown silty clay- te, w/bluish-gray silty clay- te seam, w/coarse sand at 1-38.4' occasional bluish-gray kets and seams	39	97						آل المعادا البيباء بهيا البيداء بالعبيدة بيدويده الداستياء بالفلية وليمناه فالمعنوية معتنية معتنية معتنية المشاكية	
COMPLETION	DEPTH; 50.0° DATE: 5/12/81	DEPT	нт		ATER			/a1		

MATIORAL LOST STAWORS, INC.

PLATE 90

<u></u>													
1	LOG OF BORING NO. 3-171												
			OKLAUNION POWER	ST.	ATIC	ЭN -	UN	111	10.	1			
			WILBARGER	CO	UNI	Υ,	IEX/	45					
TV	9=	BV16	RINGT loation to the Court In the Court	004						ataura ne a			
<b>+</b>			RING: Undisturbed Sample and CareL	UÇA	i jos	(, ) <sub>(</sub>	20 P	<u> </u>	1 301				
1 =	یے ا	8		30	3	55 E	ا ا	روا	ي بيا	SHEAR STRENGTH €			
DEPTH FT	SYMBOL	립	SOIL DESCRIPTION		照	188		E E	Š	IN TONS/SOFT			
6	₹.	SAMP		ş	اٰکجَ	<b>2</b> 8	[은]	ڐڒٳ	25	7 D			
۵		("]	ELEVATION: 1210.3	_	J. J.	%5	-	, ,	풀음	5 io :5 i∋ai   0.5 io :5 i∋3-7i			
	N	Ŧ	Hard dark brown silty clay,		,			_					
	W	3	w/weathered calcareous nodules			ŀ				<del>▐▐</del> <del>▐▐</del> <del>▐</del>			
1	M	1	and fine roots						'				
	3	1	mincreasing calcareous nodules		;				į				
1	W		gt 3.0'	i			! i		[				
	W	7	-brown and fan, w/packets of fine sand at 5.0'		92		i		<u> </u>				
		<b>4</b>	-reddish-brown, w/occasional		72								
	42	4	bluish-gray silty clay seams,				1	ſ	ŀ	-11:11:11:11:11:11:11:11:11:11:11:11:11:			
	Æ¥	<b>a</b> (	crossbedding at 7.0' (CL)	1	100	į		-	1	<del>╎┟╎┊╏┝┊┥</del> ┾ <del>╽</del> ┥╏╏┤┇╬╀ <b>┋</b> ┥			
<u> 10-3</u>	11	7	Soft reddish-brown silty clay-	- 1		j			ŀ	1			
	<b>FF</b>	!	stone, w/soft to moderately hard			- }		ļ	H	<del>┟┝═┩┡</del> ╂╏┼┼╁╄┼╃╇┞ <del>╏</del> ╏╴ <u>┨</u>			
	邳		clayey sandstone interbeds from 7.0-12.0'	ļ		İ		ſ	-	<del>╏</del>			
	從	1	-w/bluish-gray silty claystone	İ		ı							
<u>\</u>	岱	7	seams, w/coarse sand at 8.9-9.1		100	ļ	ļ		_ []				
	**	f	-crossbedded at 11.0'	- 1			İ	- [					
			-w/some coarse sand and bluish-			į		- [	<u> </u>				
			gray silty claystone inclusions			- 1							
	4		at 15.0'	[,	col	- 1		1		<del>┇</del> ┼╬╃╬╬╬┼╬╎╏┆┋┋╏┷╵┆┈╏			
-20-5	1		-decreasing silf -thin flat badding	- [	~	-	1		H	<del></del>			
	77		- Timi har badding	-	ı			ĺ	} <del> </del>	<del>╃╏┇┋┋</del> ╬╫ <del>╏┋╇╬╇╬</del> ╬╬┼┼┼┤			
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25.7	4		-w/bluish-grey silty claystone	;	log				竹	<del>╶</del> ┼┤ <del>╎╎╎</del> ┼┼┼┼			
44.7	<b>1</b> 7.		inclusions, crossbedded	1		1		-	- 17				
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<u>— 3</u>	뫷					ĺ			[]				
<u>—3</u>	袋		32.2						<u> </u>	3			
30-1	1		-w/bluish-gray silty claystone	יו	ᅇ	ļ	1		4				
	猁	•	seam at 30.0-31.0'		7	]	Ì	1	-	<del>┇</del> ┪┪┪┩┩┪╏╏┪┪┪			
<u>-</u> <u>-</u> <u>-</u> <u>-</u> - <u>-</u> <u>-</u> - <u>-</u> - <u>-</u>	A		1	1					- }-}-	<del>╵┆</del> ┆┼┼╃┆			
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35													
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		_					1.	<u>.</u>					
	(Continued)												
WEST MATICINAL SOR, SERVICES DE ATC OT													
<b>004d</b>	COMMATTING CHAMETERS PEATE 91												

	LOG OF BORING NO. 8-171 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS									
DEPTH, FT. SYMBOL SAMPLES	SOIL DESCRIPTION	ROD %	CORE RECOVERY %	% PASSANG NO. 200 SIEVE	LIOUD LIMIT	PLASTIC LIMIT	HOISTURE CONTENT, %	SHEAR ST IN FONS/	RENGTH SO FT.	UNIT DRY WT
40	Very soft reddish-brown clayey shale, w/occasional bluish-gray shale inclusions	58	58							-
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	Soft reddish-brown silty clay- stone -w/accasional bluish-gray seams, w/coasse sand at 43.01 -w/bluish-gray silty claystone seam; w/coarse sand at 45.8- 16.11	93	95			,			9	4       6   1   1   2   4   4   4   4   4   4   4   4   4
-55	,						- HITTHEFT			
36 35										
COMPLET	ON DEPTH: 50.0° DATE: 5/12/81	0EP1	TH 1		ATES DATE			<b>'81</b>		

MATIOGRAL EDIL SERVICES, MO., COMMUNICATION ENGINEEMS.

PLATE 92

	LOG OF BORING NO. 3-172 OKLAUNION POWER STATION - UNIT NO. 3 WILBARGER COUNTY, JEXAS											
TY	PΕ	801	RING: Undisturbed Sample and CareL	Q CA	T(ON	:: 5	ee P	lan	of Bo	orings, Plate 3		
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: J207.4	RQ0 %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	IQUID LIMIT	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH IN TONS/SQ FT		
5 1			Very stiff reddish-brown silty is clay, w/accasional fine gravel and organics increasing silt and gravel at 3.0' -hard, increasing coarse sand and fine gravel, very friable		100					C.5 (.0 1.5 = -		
-10-	THE STATE OF THE S		-gravel seam at 5.0-6.0" (CL)  Soft reddish-brown silty clay- stone, thick bedded, w/occa- sional bluish-gray silty clay- stone inclusions		100		<u> </u>		<u>{</u>			
-15			-increasing silt and crossbedding -medium gently dipped bedding, w/moderately hard siltstane soom at 14.0-14.2' -w/occasional bluish-gray silty claystone seams and inclusions at 15.0'		100							
20			-thick bedding	ļ	100							
25	25 -w/numerous small bluish-gray silty claystone inclusions											
30 77 77 77 77 73 75 75 75 75 75 75 75 75 75 75 75 75 75	THE THE PERSON	] .	-decreasing silt -severe water loss at 30.0' -heavily fractured at 30.0-32.0'		100							
	(Continued)											
COMMITTIONAL SON SERVICES PLATE 93.												

LOG OF BORING NO. 8-172 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
SYMBOL SYMBOL SAMPLES TIGGS	800 % 800 %	88	% PASSING 40, 200 SIEVE LIQUID LIMIT	PLASTIC LIMIT MOISTURE CONTENT %	TH DS/SMOT MI					
-w/accasional large blu silty alaystone inclusions -extremely slickensided -w/accasional high angle fractures -5565656570	972 Ge	100	WATER	Cove						
COMPLETION DEPTH: 50.0' DEPTH TO WATER: Coved at 20.5'  DATE: 5/11/8! DATE: 6/1/8!  PLATE 94										

AEPOKP000119

	LOG OF BORING NO. 8-173 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS											
TYP	ÞΕ	80	RING:Undisturbed Sample and Care L						f 8ar	inos. Piote 3		
рерти. Рт.	SYMBOL	SAMPLES	SOIL DESCRIPTION	RQD %	CORE COVERY %	6 PASSING 200 SIEVE	LIQUID	PLASTIC LIMIT	OISTURE	SHEAR STRENGTH AT		
	ו ערו	V	ELEVATION: 1203.9	 	. 62	°`2			Σŏ	0.5 I.0 i.5 5		
		1	Hard dark brown silfy clay, w/calcareous and magnesium			_						
		1	nodulas and numerous fine roots (CL) Hard reddish-brown silty clay,		001							
			increasing weathered calcareous (CL) Soft reddish-brown clayey silt-		98							
10-2	然		stone, w/small bluish-gray clayey siltstone inclusions -slightly slickensided at 8.0'		100		[ 		ļ 			
			-w/increasing claystone lamina- tions, crassbedded at 11.01									
15 1		1	Soft reddish-brown silty clay- stone, w/bluish-gray silty clay- stone seam at 14.2-14.6'		95							
			-w/occostanal bluish-gray stilty claystone inclusions and seams		96							
25 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	100 Till Till Till Till Till Till Till Ti											
	TOTAL WANTER	i	rcrossbedded, w/numerous large fluish-gray silty claystone nclusions w/bluish-gray silty claystone eam at 33.0-33.51		co							
33												
(Continued)												
PLATE 95												

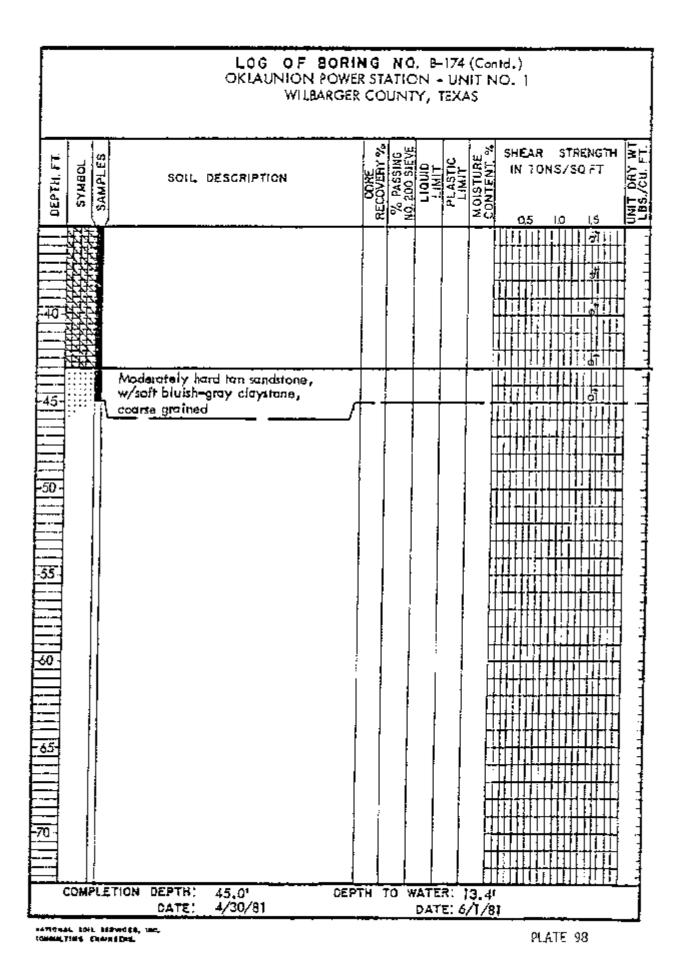
MATTORAL BOOL I (RYCCE), INC.

	LOG OF BORING NO. 3-173 (Contd.) OKLAUNION POWER STATION - UNIT NO. I WILBARGER COUNTY, TEXAS												
71 100 0	DEF 151. F. I.	SYMBOL	SAMPLES	SOIL DESCRIPTION		RQD %	RECOVERY %.	% PASSING NO. 200 SIEVE	1,0010 1,0017	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH SIN TONS/SQ FT SE	LBS./cu. FT.
-50		S. C. C. C. C. C. C. C. C. C. C. C. C. C.	TOUR OF THE PROPERTY OF THE PR	-w/bluish-gray silty claystone seam, w/coarse send at 39.0-34 -w/coarse send at 39.0-34 -w/coarse send at 39.0-34 claystone inclusions		73			YATE	R			ارين _ ا ۱۰ د و و بايد و دو دو دو دو دو دو دو دو دو دو دو دو
				DATE: 5/14/81				- '			5/14,	/81	1

AEPOKP000121

PLATE 95

LOG OF BORING NO. 8-174 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
TYPE BO	RING: Undisturbed Sample L	OCAT	TION	II Se	e P!	an o	ıf Bor	rings, Plate 3		
OEPTIL FT. SYMBOL. SAMPLES		CORE RECOVERY %	S PER FT.	% PASSING NO. 200 SIEVE	Jour HMT	PLASTIC LIMIT	MOISTURE	SHEAR STRENGTH ALL TO STRENGTH		
	Hard reddish-brown silty alay, w/numerous fine roots and calcareous nodules -w/increasing weathered calcareous nodules at 3.0' (CL)				· ·					
	Hard reddish-brown silty clay -w/large weathered calcareous									
	soft reddish-brown silty claystone, w/black coarse gravel seam at 8.0° w/numerous colcareous nodules, gravel pockets and occasional iron stained inclusions -decreasing silt  -w/occasional soft bluish-gray claystone inclusions	00	57/5	39	34	14		z; =c luxly   am/sec   123		
35		00	· +		 					
(Continued)										
PLATE 97										



AEPOKP000123

	LOG OF BORING NO. 8-176 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS								
TYPE BOR	IING: Undisturbed Sample and Care L	OCA	TION	i∶Se	e Pl	on o	f Bor	ings, Plate 3	
DEPTH, FT. SYMBOL SAMPLES	SOIL DESCRIPTION ELEVATION: 1210.9	% do8	CORE RECOVERY %	% PASSING	dinoi.	PLASTIC	MOISTURE CONTENT %	SHEAR STRENGTH AND TONS / SO FT. AND TONS / SO F	
	Very stiff reddish-brown silty clay, w/some fine sand and calcareous nodules -hard, w/fine gravel and calcareous nodules and magnesium nodules at 3.0' (CL) Soft reddish-brown silty clay-			96	46	17	13	**************************************	
	-w/numerous seams of bluish- gray silty claystone inclusions -decreasing silt		100	97	32	16	10		
20	-crossbeddad, slightly frectured is and w/some fine sand		100						
25	-w/clay laminations, fissured		100	59	30	16	9	137	
	-w/bluish-gray silty claystone seam at 29.5		100			-  -			
		_]			[	_	_}		
(Continued)									
MT3/NATIONAL SOL SERVICES									

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	LOG OF BO OKLAUNION PO WILSAR	OWER	( ST/	411C	NN →	· UN	11 14	
DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	RQD %	CORE RECOVERY %	% PASSING NO. 200 SIEVE	TIMIT CIUDIT	PLASTIC LIMIT	CONTENT %	SHEAR STRENGTH ST.
	-w/numerous large bluish-gray silty claystone inclusions	76	92					
		94	96					
50 3						2		
60-								
70		:						
CCMP	LETION OEPTH: 50.0' DATE: 5/8/81	Dī	PTH	, TÇ	WA	TER	. Ωry . 57	r - Coved at 14.1" 28/81

ALTIORAL BOIL SERVICES, INC. CONSULTING ENGESTEE

LOG OF BORING NO. 8-177? OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS								
TYPE 808	RING: Undisturbed Sample L	OCA	T108	i ( Se	e Pj	an o	<u>f Bot</u>	rings, Plate 3
DEPTH, FT. SYMBOL. SAMPLES	SOIL SESCRIPTION ELEVATION: 1207.3	CORE RECOVERY %	S PER	% PASSING NO. 200 SIEVE	LIQUID	PLASTIC LIMIT	MOISTURE CONTENT, %	HTDRATT RABHE IN TONS/SOFT IN T
	Very stiff dark brown silty clay, w/numerous organic material (CL) Hard reddish-brown silty clay, decreasing silt, w/occasional fine gravel and roots -w/numerous weathered cal-							
	careaus nadules at 4.0' (CL)	52	:	<u> </u>				
	Soft reddish-brown silty clay- stone, w/numerous weathered calcareaus nodules -crossbedded, w/occasional soft bluish-gray silty claystone lominations and inclusions at 8.0' -thin appyel seam at 10.0' Soft reddish-brown claystone, thick bedding, w/occasional soft bluish-gray claystone inclusions	100 100 100 100 100 60		99	34	15	13	
	(Continu	ed)		'				
	· · · · · · · · · · · · · · · · · · ·							

PLATE 103

	LOG OF BORING NO. 8-177(Confd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
DEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	RECOVERY %	% PASSING NO, 200 SIEVE	LEGUID	PLASTIC	MOISTURE CONTENT, 72	SHEAR STRENGTH XX IN TONS/SQ FT XX IX IX IX IX IX IX IX IX IX IX IX IX						
	-w/numerous soft bluish-gray clay- stone inclusions	100				3							
COMPLE	TION DEPTH: 49,5' DE DATE: 4/30/81	PTH	то ч		R; 2 (E) 6								

PATIONAL SME TORNICES, INC.

silly claystone inclusions		LOG OF BORING NO. B-178 OKLAUNION POWER STATION - UNIT NO. 1												
SOIL DESCRIPTION  BLEVATION: 1203.6  Very stiff brown silty clay, w/numerous fine roots and creanics  Were stiff brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Hard dark brown silty clay (CL)  Were stiff brown silty clay (CL)  Hard dark brown silty clay (CL)  Soft reddish-brown silty clay-  wy/occasional gravel and bluish-  gray silty clay inclusions  -w/some fine sand, fissured  ct 7.0'  Soft reddish-brown silty clay-  stene, thick bedding  -increasing silt, crossbedded,  w/some fine sand at 12.0'  -thick bedding  -increasing silt, crossbedded,  w/some fine sand at 12.0'  -thick bedding  -increasing silt  -decreasing silt  -decreasing silt  -w/small bluish-gray silty  claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions  -w/accasional large bluish-gray  silty claystone inclusions		· ·												
SOIL DESCRIPTION  SOIL DESCRIPTION  BLEVATION: 1203.6  Very stiff brown silty clay, w/numerous fine roots and caranics (CL)  Hard dark brown silty clay, w/weathered calcareous nodules readiles and accasional fine gravel at 4.0'	TYP	<u>ع</u>	SORING: Undisturbed Sample and Core L	OCA.	TION	: S	ee P	ал с	of Bo	rings, Place 3				
Very stiff brown silty clay, w/numerous fine roots and creanics  Hord dark brown silty clay, w/weathered calcareous nodules reddish-brown, w/soft pockets and accasional fine grave!  at 4.0'	DEPTH FT.	SYMBOL.			CORE RECOVERY %	% PASSING NO. 200 SIEVE		PLASTIC LIMIT	MOISTURE CONTENT, %	IN TONS/SQ FT AND/SQ LINE				
w/numerous fine roots and cranics (CL) Hord dark brown silty clay, w/weathered calcareous nodules -reddish-brown, w/soft pockets and accasional fine grave! at 4.0' -w/accasional gravel and bluish- gray silty clay inclusions -w/some fine sand, fissured at 7.0' Soft reddish-brown silty clay- stone, thick bedding -increasing silt, crossbedded, w/some fine sand at 12.0' -thick bedded, w/magnesium flakes at 15.0' -w/bluish-gray silty claystone seam at 16.5-16.8' -decreasing silt -increasing silt -increasing silt -w/smatl bluish-gray silty claystone inclusions  100 -w/accasional large bluish-gray silty claystone inclusions		Z					_							
-w/small bluish-gray silty claystone inclusions  -w/accasional large bluish-gray silty claystone inclusions  -w/numerous bluish-gray silty	10		w/numerous fine roots and arganics (CL) Hard dark brown silty clay, w/weathered calcareous nodules -reddish-brown, w/soft pockets and occasional fine gravel at 4.0' -w/accasional gravel and bluish- gray silty clay inclusions -w/some fine sand, fissured at 7.0' (CL) Soft reddish-brown silty clay- stone, thick bedding -increasing silt, crossbedded, w/some fine sand at 12.0' -thick bedded, w/magnesium flakes at 15.0' -w/bluish-gray silty claystone seam at 16.5-16.8'											
(Continued)	25 GA A A A A A A A A A A A A A A A A A A	THE THE PARTY OF T	-w/small bluish-gray silty clayatona inclusions  -w/accasional large bluish-gray silty claystone inclusions  -w/numerous bluish-gray silty claystone inclusions		00									

METANATIONAL, SON, SERVICES CONSULTING ENGINEERS

	LOG OF BORING NO. 8-178 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS													
OEPTH. FT. SYMBOL SAMPLES	SOIL DESCRIPTION	Rab %	CORE RECOVERY?	% PASSING NO. 200 SIEVE	Liguid	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH ST.						
	-w/clayey shale seem at 38.19 38.51 -extremely slickensided at 39.  -w/occasional bluish-gray silts claystone seams	94	94											
COMPLE	TION DEPTH: 50.0° DATE: 5/11/81	DEP.	TH T	0 W	ATER DATE	₹: 6, :: 5,	/5' /11/	'81						

MATTOWER, SOME SERVICES, MICH.

P1 0TT 106

	LOG OF BORING NO. 8-179 OKLAUNION POWER STATION - UNIT NO. !												
ļ	WILBARGER COUNTY, TEXAS												
1.7	YF	ıĒ.	<u> 50</u>	RING: Undisturbed Sample and Care L	OCA	<u> 110 N</u>	I : Se	e Pi	an o	f Sor	ings, Plate 3		
DEDTH CT		SYMBOL	SAMPLES	SOIL DESCRIPTION	ROD %	CORE ECOVERY %	% PASSING 0, 200 SIEVE	LIGUID	PLASTIC LIMIT	ADISTURE ONTENT %	SHEAR STRENGTH M. L. IN TONS/SQ FT: LEG / SG / LEG / L		
Е	4	X	Y	Very stiff dark brown silty clay,	<del> </del>	1025	Ž			20	05 to 15 5 <sup>25</sup>		
	=}	W	1	w/numerous fine roots (CL)									
	云	N	1	Hard reddish-brown silty clay,									
	_	N	1	w/calcareous and magnesium	Ì	[ i							
F 5	-{	N	Į	nodules									
-		W	1			100	:	ĺ		·			
		N	1				ŀ	ļ	į	1	<del>                                     </del>		
	$\pm$	N	Ĭ	-w/occasional large calcareous	ĺ	100	ļ	ľ					
F10	Ŋ	N		and magnesium nodules		Ì		-	- 1				
	-7							- 1	İ	-			
	N	$\mathcal{N}$						ļ		ŀ	<del>┊┋┋┋┋┋┋┋┋</del>		
	Ŋ	$\mathcal{X}$	,					İ	Ì	Ì			
F15	N	N		-w/numerous bluish-gray silty		85	ı						
	Э	$\mathbb{R}$		clay inclusions (CL)	-		<b>-</b>	<u> ļ</u>	-	- 1			
	<i>‡</i> .	$^{*}$		Saft reddish-brown sitty clay- stone, crossbedded, w/occasional			- 1	ĺ		H	<del>╎╎┞┞╎┍┩╎┞╏╏┆╏╏╎┆</del> ┼┼		
	X	13		bluish-gray silty claystane		-			ľ				
-20	找	舒	1	nefusions	j	100							
	J.	铽	İ	ļ				Į		-  -	<del>▗</del> <del>▗</del> <del>▗</del> <del>▗</del> <del>▗</del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del> <del></del>		
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-25-	42	Ţ	ļ		Ī	00		ſ					
	抝	贸	1	increasing silt		-		-	-	-	<del>                                      </del>		
		묎		j						H	┟┼╁┇╟╁╏╟┼╁╏╇╂╅╏╴┋		
	Ž.	\$. \$.	-	fhick bedded				j	-	} <del>[</del>			
-30-	Ŧ	#		Ĺ	1	co		Ì	-	Ĭ.			
	Ü									H	<del>                                      </del>		
{	徔		_	thin flat bedding	1		Į	-		<b>}</b>	<del>╎</del> ┼┼┼┼┼┼┼┼┼┼┼		
$\equiv$	抸	4	-	w/numerous large bluish-gray					1		<del>                                      </del>		
35-	Ž	7	si	Ity claystone inclusions	<del></del>	_	$\perp$		$\perp$				
$\exists$											111111111111111111111111111111111111111		
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	(Continued)												
	(Continued)												

OKLAUNION P	DRING NO. B-179 (Contd.) DWER STATION - UNIT NO. 1 RGER COUNTY, TEXAS
SYMBOL SYMBOL SAMPLES HOLLES	RQD %  RECOVERY %  PASSING  LIQUID  LIMIT  PLASTIC  LIMIT  MOISTURE  CONTENT %  TABBE  ONTENT %  HIDSTORY
	100 100 100 100 110 110 110 110 110 110
DATE: 5/14/87	OATE: 5/14/81 PLATE 108

WE FRATIONAL SOR SERVICES

	LOG OF BORING NO. 8-180 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
77	TYPE BORING: Undisturbed Sample LOCATION: See Plan of Borings, Plate 3												
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: 1198.4	CORE RECOVERY %	BLOWS PER F.E.	% PASSING NO. 200 SIEVE	L MAIT	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR IN TO		ENGTH Q FT 1.5	UNIT DRY WT
	1,177		Hard brown clayey silt, -w/numerous calcareous nodules and line roots				00		100			6† i   5	
- 5			-w/large calcareous nodules  at 3.0'  Hard reddish-brown silty clay,  w/numerous weathered calcaroous  nodules  -w/large calcareous nodules,	08		90	38	16	13			70 - 75	
-10-		X	coarse sand, and medium to coarse gravel at 6.0'  -w/coarse gravel at 8.0' (CL)  Soft reddish-brown silty clay- stone, w/bluish-gray silty clay- stone inclusions		40/3								
-20-				100		ļ							100000000000000000000000000000000000000
25			-w/occasional high angle fractures -w/bluish-gray clay seam at 24.5-25.51	00									1
30		1	Hard reddish-brown silty clay		Q/4°								
35			-w/occasional bluish-gray silty clay inclusions (CL) Soft reddish-brown silty clay- stone, thin flat bedding	00	-	-		-					
	(Continued)												

	LOG OF BORING NO. 8-180 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, IEXAS											
DEPTH. FT. SYMBOL.	SOIL DESCRIPTION	CORE RECOVERY %	% PASSING NO. 200 SIEVE	Uldul Ulmi:3	PLASTIC LIMIT	MOISTURE CONTENT, %	CO CO CO CO CO CO CO CO CO CO CO CO CO C					
	-bluish-gray claystone, w/gravel at 36.0"	100										
40	Hard reddish-brown silty clay (C1)	100				-						
	Soft reddish-brown claystone, thick bedded	100										
	Very soft reddish-brown clayey shale, w/occasional small bluish- gray clayey shale inclusions	100										
-60-10-10-10-10-10-10-10-10-10-10-10-10-10	ETION DEPTH: 45.0' DEP	714		WATE	io. 1							

MATICULA, LOIL METHERS, AME

91ATE 110

$\lceil$	LOG OF BORING NO. 3-181 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
TY	۶E.	ВОЯ	ung: Undisturbed Sample L	OCA	TION	l∷_Se	e 21.	a <b>u</b> a	f Bor	ings, Plate 3	╝		
DEPTH. FT.	SYMBOL	SAMPLES	SOIL DESCRIPTION	CORE	BLOWS PER FT.	% PASSING NO. 200 SIEVE	LIQUID	PLASTIC LIMIT	IDISTURE ONTENT, %	SHEAR STRENGTH A	BS./cu. FT.		
<u> </u>		Ű	ELEVATION: 7206.0	i de	<u> </u>	아			≆೮	0.5 LD 1.5 3	긔		
- 5			Hard dark brown silty clay, w/calcareous nodules and numerous fine roots (CL) Hard reddish-brown silty clay, w/numerous weathered calcareous pockets and black		•						يبليينينيني		
- 2-			gravel (CL)  Soft reddish-brown siltstone, w/thin gently dipped very soft claystone laminations -w/some coarse gravel at 8.0' -crossbedding at 8.3-8.7', w/occasional bluish-gray silt- stane inclusions	60	50/4°								
-15 -20-			Soft reddish-brown silty clay- stone, thick bedding, w/occa- sional bluish-gray silty clay- stone inclusions  -thin flat bedding	100	ar∕a.								
				100							<u> </u>		
	(Continued)												

Warnational Son, Structs Communical Engineers

		LOG OF BOR OKLAUNION POW WILSARGER	er sta	ATIC	:N -	UNU	IT N	itd.) IO. 1
DEPTH. FT.	SAMPLES	SOIL DESCRIPTION	RECOVERY %	% PASSING NO. 200 SIZVE	LIGUD	PLASTIC	NOISTURE CONTENT, %	SHEAR STRENGTH ALL SHEAR STRENGT
		-slightly slickensided	100					
45						Ŀ		
-50 -								
-55-					ļ			
65-								
770 ·							1_1	
		TION DEPTH: 40.0' DE DATE: 5/6/81	PTH 1	FO Y		R:14 E:6/		DI ATE 112

	LOG OF BORING NO. 8-182 OKLAUNION POWER STATION - UNIT NO. 1												
	WILBARGER COUNTY, TEXAS												
TY	먇	зония: Undisturbed Sample	L	DCA	TION	: Se	e 21a	en of	<u> 8∞r</u>	ings, Plate 3			
DEPTH. FT.	SYMBOL	SOIL DESCRIPTION	N	CONERY %	ROWS PER FT.	6 PASSING 3. 200 SIEVE	나보는	PLASTIC	OISTURE	SHEAR STRENGTH ALL			
	***	ELEVATION: 1203.7	-	REC	골	~5			ತನ	05 ID 15 34			
- 5 :		Hard brown silty clay, w/ roots, accasional coarse w and weathered calcareous nodules Hard reddish-brown silty o w/numerous weathered cal	and <u>(CL)</u> / :lay,							(b)			
		eous nodules  -extremely friable, w/fine gravel at 5.01  -w/some fine gravel and i nodules at 7.01  -w/occasional bluish-gray silty clay inclusions at 10, -w/bluish-gray silty clay	e Iron	100		99	40	20	12	(a)   50xil(0   cm//sec			
-15-5	沉	pockets	(CL)		seat								
		Soft reddish-brown silty all stane, thin to medium bedd w/numerous line roots	ding,	100		24	20	, ,					
20		-continuing bluish-gray po			37/5 seat	34	30	15	7   1   1   1   1   1   1   1   1   1				
-30-8		Very soft raddish-brown classical shale  -w/bluish-gray silty clay inclusions	· · · · · · · · · · · · · · · · · · ·	00									
35	<b>施雅</b>	Soft reddish-brown silty che stone, thick bedded -slightly slickensided		00									
									-  -  -				
,	(Continued)												

	LOG OF BORING NO. 3-182 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS													
DEPTH. FT.	SYMBOL	SAMPLES	SOIL D	ESCRIPTION		CORE RECOVERY %	% PASSING NO. 200 SIEVE	Liguto	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH A LA IN TONS/SQ FT A LA IN			
45-55-65-70-			-very soft claye 38.5-40.0'	sy shale seam at		100								
	COM	PLE	TION DEPTH: OATE:	40.0' 5/5/81	DEP	TH	70	ATE DATE	(R; C	2ve	d at 7.5 /81			

LOG OF BORING NO. 8-183 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS												
TYPE BORING: Undisturbed Sample	le <u>LOCA</u>	TIGN	: 5e	e Pla	ın of	Вог	ings, Plate 3					
SAMPLES SOIL DESCRIPT STANDIES	% <u></u>	_	% PASSING NO, 200 SIEVE	CIQUED	PLASTIC LIMIT	MOISTURE CONTENT %	SHEAR STRENGTH AT TONS/SQ FT. AT TON					
Hard brown silty clay, w/weathered calcareou and iron nodules -reddish-brown at 3.0' -w/occasional coarse so fine gravel, w/some fin at 4.0' -w/fine gravel and iron at 6.0' -w/occasional pluish-g silty claystone inclusion -w/numerous fissures	and and ne roots 80 n stains 80	ŀ										
Soft reddish-brown silty stone -w/same sand at 13.7*  -13  -w/decreasing silt -w/occasional bluish-sclaystone inclusions	100 100	50/4	,			7						
-crossbedded, w/some	fine sand 10		-									
	(Continued)											

	LOG OF BORING NO. 8-183 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILEARGER COUNTY, TEXAS											
DEPTH. FT.	SYMBOL	SAMPLES	SOIL	DESCRIPTION		CORE RECOVERY %	% PASSING NO, 200 SIEVE	LIQUID	PLASTIC	MOISTURE CONTENT %	SHEAR STREN	1 15
	<u> </u>	9	Very soft redo	lish-brown claye	y shale						<del>▊</del> ▊ <del></del> ▋▋▋	
40 -			-w/accasiona	i gravel	<del></del> .	30				-		
	, <u>, , , , , , , , , , , , , , , , , , </u>											
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-50-												
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70 -				`				'   				
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	COM	PLE	THON DEPTH:	40.0° 5/5/81	DEP	тн	TO 1		R: E:6		ed at 3.8° /81	

SATISMAN, SOIL REPORTED, INC. COMMUNITARY SHAREFUL

MASSIMATIONAL NOW SERVICES COMMETING ENGINEERS

	LOG OF BORING NO. 8-185 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS										
	Ϋ́	宅	8CI	RING: Undisturbed Sample (	OCA	TIO	<u>∜∶</u> Se	e Pla	on of	3or	ings, Plate 3
FO 01000	DEF 17. F.	SYMBOL	SAMPLES	SOIL DESCRIPTION ELEVATION: 1198.3	CORE 7.	E E	4 P	•	PLASTIC	MOISTURE CONTENT, %	SHEAR STRENGTH IN TONS/SQFT. LY DEA MILL OF LO 1.5
E	4	$\mathcal{M}$	Ì	Hard tannish-brown clayey silt,	<del></del> 		<del> </del>				
			777777	w/numerous calcareous nadules and fine roots (ML) Hard brown silty clay, w/numerous packets of calcareous nodules and gravel -w/numerous fine gravel at 4.0° -w/numerous medium to coarse			72	39	15	11	( = F 20 k 10 T cm/sec 130 t
10	dictory			gravel and weathered calcareous nodules at 5.0° (CL)  Soft reddish-brown silty claystone, w/occasional calcareous filled fractures  -w/occasional soft bluish-gray silty claystone inclusions		<b>30/5</b> "					
-20	Character Condon			-medium bedding	100		76	30	14	10 1 1 1 1 1 1 1	(=4 36×10 fsm/sec 30
30-	があれてもなりからなるから	A CHANGE AND A CHANGE		increasing silt, crossbedded		C/5"					
									ļ		
	(Continued)										

	LOG OF E OKLAUNION P WILBA	BORING POWER STA RGER CO	۱TIQ	N -	· UN	lî N	fd.) IO. I
SYMBOL SAMPLES	SOIL DESCRIPTION	CORE	% PASSING NO. 200 SIEVE	CHOUR	PLASTIC LIMIT	MOISTURE CONTENT %	SHEAR STRENGTH 3.1. IN TONS/SOFT, 3.1. LIGHT OF 10 15 07
45	thick bedded	100					
COMPLETION	DATE: 5/4/81	DEPTH TO				3º 12/e	PLATE. 138

AEPOKP000141

Γ	LOG OF BORING NO. 8-186 OKLAUNION POWER STATION - UNIT NO. 1										
				WILBARGER							`
Ţ	ΥF	E	308	UNG: Undisturbed Sample L	oc.	TION	ł:Se	e 21	<u> </u>	f Bor	ings, Plata 3
DENTH CT		SYMBOL	SAMPLES	SOIL DESCRIPTION	CORE WEHY 97	85	PASSING DO SIEVE	LIQUID	ASTIC	STURE TENT, %	SHEAR STRENGTH AT AN TONS/SQFT.
1	3	Š	8	ELEVATION: 1202.7	RFCOV		26.5 2		۳,	S C C	0.5 1.0 1.5 173
	_	V	ľ	Hard dark brown silty clay,	<u> </u>	112	-				
			ħ	w/weathered calcareous nadules (CL)	<del> </del>	<del> </del>					
			2	Hard reddish-brown silty clay -w/numerous calcareous filled							
	$\pm$	N	1	fissures and packets at 4.0° -w/accasional calcareous nodules		-					
	7	W	7	and coarse gravel at 6.0'	1100		[				<del>╎</del>
	=}	N	1	-w/occasional bluish-gray silly							<del>╿╎╎┦╏╏</del> ┼┼╫╏
	<del>/</del>	N	1	clay inclusions	100						
		N	}]	-						[	
	-	W			Ì						┩┧ <del>┋</del> ┧ <del>┪┩┋┋┋╸┋</del> ┾┡╒╬┾╂╬┩╴╶ <b>┇</b>
	⇉	$\overline{\Omega}$	<u>¥</u> _	(CL)	<u> </u>	<b>30/9</b>					<del>{-++++++++++++++++++++++++++++++++++++</del>
		ŹŹ		Soft reddish-brown claystone,				- 1			
	1	$z_{z_{z}}$		thick bedded					-	[	
	- \$	77.	ł	-w/accasional high angle	100			į		}	<u>╎╎┊</u> ╎┼╎╎╎╎╏╏
	7	7		fracturesw/accasional bluish-gray clay	1100		ļ	ļ		-	<del>╏</del> ┾ <del>╞</del> ┼┼┼┼┼┼┼┼┼ <del>╬</del> ┼┼┼╏
	4	77		stone seams and inclusions				:	1	ŀ	<del>┆</del> ┩┼ <del>┆</del> ┆┼ <del>╏┆</del> ┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼┼
20	- 2	22							F	<u>ַ</u>	
	₹	72		-w/occasional high angle	100			ļ		ļ	<u> </u>
-	1	72	×	fractures	100	30/4		- [		-	<del>                                     </del>
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<u> </u>	乜	7		-fine gravel seam at 26.0'			İ			r	
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	払	拟		oft reddish-brown silty clay-			į		-	H	<del></del>
-35	ř	717		tions, thick bedded, w/occa-			$\dashv$	<del></del>	+	<u> </u>	╫╫╫╫╫
	•			tional bluish-gray silly clay- tona inclusions		·			-	H	<del>                                     </del>
	_	_ [									
<u>_</u>				(Continu	ed)						
1073/	COMPLETORS ENGINEERS FLATE 319										

WILSARGER	CO	VIIO	N -	UNIT	antd.) NO. I
SYMBOL SYMBOL SAMPLES SAMPLES		%ള	LIMIT	PLASTIC LIMIT MOISTURE	SHEAR STRENGTH IN TONS/SOFT OF 10 18 CONSTRUCT OF 15 CONSTRUCT
	30 30		-		
45-					
-50					
-55-					
65-					
-70-					
COMPLETION DEPTH: 40.0° CEPTH DATE: 5/6/87	i Ti			Cave 6/11,	2LATE 120

į		LOG OF BORING NO. B-190 OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS																	
											·								
	77	PE.	BOF	ling:	Undist	urbed S	cmple		Loc.	OITA	N: 5	ee P	lan e	of 3α	rings,	•			<del></del>
	DEPTH. FT.	SYMBOL	SAMPLES				RIPTION	4	CORE	BLOWS PER FT	% PASSING	diodi.	PLASTIC LIMIT	ONTENT %	•	AR Tons		ENGTH FT.	11 DRY WT 89./CU. FT.
l			V		ATION:			<u>.</u>	6	1 2	3.5	<u>{</u>		20	<u>a</u> .	5 1.	0	1.9	33
				w/nu		fine ro	lty clay ots and		$\perp$	<u> </u>	_	-	ļ						
	5			Hard w/ca -w/c	raddish Icareou	r-brown is nodu. ius node	silty o	ldy,	80							13:4	111; 01;		
F		<u> </u>	1	-w/b	luish-g	ray cla	y bails	(CL)	80		100	35	16	סד	<del>,</del>		- - - - - - - - - - - - - - - - - - -	4111	127
	10-		4 4 4 4 7 7	stone			sîlty cl	oy-	80										1
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	157						own ck ckersic		100		96	36	20	18	<del>-</del> 3.	90×1	01 i c	m/9ac	118
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					casiona layston		bluish- sions	- '	100										
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LOG OF BORING NO. 8-190 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS  F 193 SHEAR STRENGTH S										
DEPTH. FT. SYMBOL SANPLES SANPLES	1 3	GLOWS PER FT.	% PASSING NO. 200 SIEVE	LIMIT	PLASTIC LIMIT	MOISTURE CONTENT, %	SHEAR STRENGTH AT A TONS/SQ FT AT A TONS/SQ FT AT A TONS/SQ FT AT A TONS/SQ FT A TO			
-w/inclined iron stained at 39.6'	100 seam 80	1 :								
-30- -55- -60-										
COMPLETION CEPTH: 40.0° DATE: 5/5/81	0EPT	H TO		TER		1.11	PLATE 122			

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1			LOG OF B	081	NG	NO	ე. ც	-192		
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]			WILBARGER	CO	UNI	Υ, τ	EXA	S		
1										
TY	۶Ę	90	NNG: Undisturbed Sample	<u> Loc</u>	AT10	N: S	ae P	lan s	of Soi	ring≰, Plate 3
		إررا	· · · · · · · · · · · · · · · · · · ·	Ţ	% F				38	
[ <u>F</u>	占	MPLES		ڏِ ا	- 2	184	امد	≌	LE -	SHEAR STRENGTH >
] ∄	9	릴	SOIL DESCRIPTION			1880	,∣⊋≡	흔	글곱	10.437.3QF1 EE
DEPTH	SYMBOL			ଧ୍ୟ	3 ≨	ାଙ୍କ	LIGUID	PLASTIC LIMIT	읂휥	
=		["]	ELEVATION: 1191.4	CORE	ALDWS PER	%°2			JžSI	0.5 10 15 S
	X	Ì	Hard tannish-brown clayey silt,	†	<u> </u>	+	<del> </del>	<u> </u>	<del></del>	
	$\mathcal{W}$	ŧ,	w/calcareous nodules and fine		ł	1	;	<u> </u>	]	<del>┇┇</del> ╏╽╏┆ ╇ <del>┇┇</del> ┩╃╃╄╄┨╂┎┎╼ <sub>╇┡╬</sub> ╌┇╤┥
	*	ď٦	roots (ML)	┈	┿	╀	!	ļ	<u> </u>	[
$\square$	N	4	Hard tannish-brown silty clay	1	1				ļ., į	<del>}                                    </del>
	N	3	-w/accasional fine roots at 4.0'	100	n	62	28	14	1	
- 5 -	W	Ŧ	-redaish-brown, w/fine to	1,00	1	[	i l	ĺ	!	
	W	4	coons gravel at 5.0' (CL)			1		·		<u>                                     </u>
	<b>113</b>	#	Soft reddish-brown silty clay-	80	1		<u> </u>	i		11: - 14: - 1 - 1 - 1 - 1 - 1 - 1 - 1
	14.	1	stone, thick bedded, w/bluish-	ļ		أيما				
<u></u> }	(1)	7	gray silty claystone seam at	1		94	33	20	13	
-10-	14.		7.8-8.0		!	;		[	ļ,	
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	42	<b>)</b>			!					
	77.	ì	Soft bluish-gray claystone,	100			ŀ	- 1	- []	<u> </u>
<u></u>	77		w/numerous coarse sand and	-					<u> </u>	<del>                                     </del>
	77	1	fine gravel		, ,	ļ	- (	- 1		[
20-5	$\Xi$			•			ļ		H	<del>                                     </del>
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	*		Soft reddish-brown silty clay-	100		96	29	17	12%	=5 65x10 \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
<u></u> ;	#		itone, w/occasional bluish-gray	1104		1	ŀ	Æ	ļ	
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25	<u>7</u> 4			ا ا	·	[	İ	- [	<u> </u>	
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			(Contin	ued)						ļ
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30N3	Ú.,	E	MANGES MEENS							PLATE 123

	LOG OF BORING NO. 8-192 (Contd.) OKLAUNION POWER STATION - UNIT NO. 1 WILBARGER COUNTY, TEXAS													
DEPTH, FT. SYMBOL SAMPLES	SOIL DESCRIPTION	BLOWS HER FT		LIGUID	PLASTIC LIMIT	MOISTURE CONTENT %		SHE IN	TQI		/50	ENG°	ГН	THIT DRY WT
Very	soft reddish-brown clayey							11 			<u> </u>	_	i : i	
shate -w/1 38.0	e olivish—gray claystone seam at 1–39,5°	<u>80</u>				-			<u> </u>	; ] 				
45														
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<u>65</u>	•				   					╃╃ ╈┿				***
70:				!			<del>                                      </del>			-  -  -				44.111.44
	DEPTH: 40.0° C	ЕРТН		ATE:										

MATIONAL COLL SEMPLES, MC. COMBULTING- ENMARESC.

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LOG OF BO OKLAUNION POWER	RING STATU	NO NAC	), B	-195 UT 6		
SEASTAIN SEASTAIN	COUN.	υ(4 · ΓΥ, 1	EXA	01 P <b>\\$</b>	٠٠,	1
<b>1</b>						
	CATIO	<u>N : S</u>	ee P	on s	f Bo	rings, Plate 3
[	5	925		ပ	ان س بيرا	SHEAR STRENGTH
SYMBOL SYMBOL SAMPLES	贈	550		E.	25	IN TONS/SOFT
	් විද් වි	8.5	12-	125	SY	J / S
ELEVATION: 1196.3		×	<u> </u>		≱ರ	0.5 10 1.5 13 13
itard light brown silty clay, w/fine roots and weathered calcareous	•					1
nodules and some fine grave!	İ				}	<del>┊</del> ╃┾╃ <del>╎┊</del> ╅╁ <del>┊</del> ╃┼ <u>╏</u> ╬╏╄╇╸ <b>ॏ</b>
-tan and reddish-brown, w/numer-	$\int_{0}^{\infty}$				<del></del>	111111111111111111111111111111111111111
5 Soft reddish-brown silty claystone,	$\mathcal{I} _{100 }$	88	29	14	11	111111111111111111111111111111111111111
thick bedded, w/occasional			İ	ļ	_	
calcareous filled fissures	100	' <b>i</b>	ļ	]	-	╫╫╫╫╫╫╫
-increasing silt and crossbedded	1,00	ł	ļ	-	h	<del>┟┞┋</del> ┼ <del>╏╏╏╏╏╏╏</del>
at 6.0' -10-10 -w/bluish-gray silty claystone	40	Į	ĺ	- 1	۲	┞╀┼┼┤┼ <del>╿╅┩</del> ┾┼┼ <del>╏┇</del> ╄┤┼┦ <b>┋</b>
inclusions at 7.0'		ļ		1	Ţ	
-slightly indurated at 8.0"					H	
-thick bedded at 10.0'	80	ł		İ	1	<del>╃</del> ╊╇╋╊┼╬╌╏┾┪╃╬ <u>╏</u> ╏┞┝╇╸╶┇
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# APPENDIX A

# **Document 5**

Inspection Report 06.15.09

# 2009 DAM & DIKE INSPECTION REPORT WASTEWATER POND COMPLEX

**GERS-09-025** 

OKLAUNION POWER PLANT

AMERICAN ELECTRIC POWER

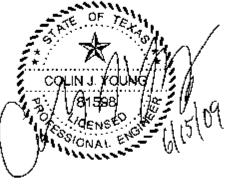
VERNON, TEXAS

PREPARED BY

URS CORPORATION 9400 AMBERGLEN BLVD. AUSTIN, TEXAS 78717

June 2009

The technical material and data contained in this report were prepared under the supervision and direction of the undersigned, whose seal as Professional Engineer is affixed below:



Colin Young Texas License No. 81598 URS Corporation Texas Firm No. 3162

## ANNUAL DAM AND DIKE INSPECTION REPORT OKLAUNION POWER STATION WASTEWATER POND COMPLEX YEAR 2009 GERS-09-025

INTRODUCTION	:
General Information	
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APPENDIX A: VICINITY MAP AND PLAN VIEW

APPENDIX B: INSPECTION PHOTOGRAPHS

#### INTRODUCTION

AEPSC (American Electric Power Service Corporation) Civil Engineering manages the Dam and Dike Inspection and Maintenance Program (DIMP) at AEP facilities. As part of DIMP, staff from the Geotechnical Engineering Section conducts dam and dike inspections annually. The 2009 inspection of the wastewater pond complex dikes at the Oklaunion Power Plant was performed by URS Corporation. Messrs Colin Young, P.E. and Lance Finnefrock were accompanied by Messrs. William Smith, P.E., and Kenneth Patton, P.E. of AEP. This report was prepared by Mr. Colin Young, P.E. and serves as a summary of the inspection and an assessment of the general conditions of the facility.

Mr. Kenneth Patton, P.E. of AEP Plant Engineering Region 5, was the facility contact for the inspection. The inspection was performed on April 2, 2009. Weather conditions were very windy, with temperatures in the 50's and 60's.

#### **General Information**

The Oklaunion Power Plant is owned by American Electric Power and is located at 12567 FM Rd 3430, Vernon, TX 76384. The plant is a coal-fired facility, which features a number of wastewater evaporation ponds containing cooling tower blowdown. A few of the wastewater ponds also contain some byproducts of the coal combustion process. Earthen fill dikes retain the waste until it is sufficiently dry to be hauled away and landfilled. The plant has 11 wastewater evaporation ponds, with a total area of 335.9 acres. Two proposed evaporation ponds at the northwest corner of the site would have a total area of 54.6 acres. In addition, there is one make-up water supply pond (52.8 ac.), a coal pile runoff pond (27.3 ac.), and a wastewater/sludge pond (22.6 ac.).

#### SUMMARY OF VISUAL OBSERVATIONS

The summary of the visual observations presented herein uses terms to describe the general appearance or condition of an observed item, activity or structure. Their meaning is understood as follows:

Good: A condition or activity that is generally better or slightly better than

what is minimally expected or anticipated from a design or

maintenance point of view.

Fair or satisfactory:

A condition or activity that generally meets what is minimally expected or anticipated from a design or maintenance point of view.

Poor: A condition or activity that is generally below what is minimally

expected or anticipated from a design or maintenance point of view.

Minor: A reference to an observed item (e.g., erosion, seepage, vegetation,

cracks, concrete surface etc.) where the current maintenance condition is below what is normal or desired, but which is not currently causing

concern from a structure safety or stability point of view.

Significant: A reference to an observed item (e.g. erosion, seepage, vegetation,

cracks, concrete surface etc.) where the current maintenance program has neglected to improve the condition. Usually, conditions that have been identified in previous inspections, but have not been corrected.

Excessive: A reference to an observed item (e.g., erosion, seepage, vegetation,

cracks, concrete surface etc.) where the current maintenance condition is above or worse than what is normal or desired, and which may have affected the ability of the observer to properly evaluate the structure or particular area being observed or which may be a concern from a

structure safety or stability point of view.

Results of the visual inspection performed on April 2, 2009 are summarized below. Pond water elevation is presented in the instrumentation data section of this report. The inspection focused on the exterior western and southern dikes, as these were the only locations where dike failure could lead to uncontrolled release of impounded water off-site.

#### **Outfall Spillway**

The outfall spillway is located on the south slope of Wastewater Evaporation Pond #7, and runs adjacent to the east slope of Pond #6. Brush and trees were recently cleared from the channel area, leaving behind disturbed soil and minimal vegetative cover. Several small

trees remain in the concrete-lined spillway chute itself, situated on the south downstream slope of Pond #7.

#### **Wastewater Evaporation Pond #6**

Pond #6 is located at the south-central edge of the site. No signs of slope failure, slumping, or seepage were observed on the downstream slope. Vegetative cover on the east downstream slope of Pond #6 is very poor due to recent tree clearing. At the southwest corner of the pond, vegetative cover is also very poor and excessive erosion gullies (up to 2 feet deep) (Photographs 2-6) have developed on the downstream slope extending from the crest. Aside from the potential threat of headcutting, the crest of the dam appeared to be in good condition with no unusual deformation or misalignment.

#### **Wastewater Evaporation Pond #7**

Pond #7 is located on the southeastern corner of the site. The crest of the dam appeared to be in good condition with no unusual deformation or misalignment. No evidence of slope failure, slumping, or seepage was observed on the downstream slope (Photograph 1). Vegetative cover on the south downstream slope is fair to poor. As previously mentioned, there are trees growing in the outfall spillway on the downstream slope. Wave action has resulted in significant erosion on its upstream slope, with near vertical scarps observed a short distance above the break height of the waves.

#### **Wastewater Evaporation Pond #8**

Pond #8 is located near the western boundary of the site and adjacent to Pond #9. There were no observed signs of slope failure, slumping, or seepage on the downstream slope. Vegetative cover ranges from fair to very poor, and minor to significant erosion is widespread. Areas of excessive erosion (Photographs 11-14) are found at the northwest corner of the pond, where erosion gullies, scarps, and sloughs are present on the downstream slope. Additionally, channelization due to stormwater runoff at the north of the pond is starting to cut away at the toe of the slope, which could eventually lead to stability concerns if left unaddressed. The crest did not exhibit any unusual deformation or misalignment, but erosion rills and gullies have begun headcutting at the downstream edge of the crest.

#### **Wastewater Evaporation Pond #9**

Pond #9 is located near the southwest corner of the site and adjacent to Pond #10. No evidence of slope failure, slumping, or seepage was observed on the downstream slope. The quality of vegetative cover on the downstream slopes of Pond #9 generally ranges from fair to poor. However, the occurrence of minor to significant erosion rills and gullies was widespread on these slopes (Photograph 7), even where vegetation would be considered

acceptable. Erosion is excessive in localized areas of very poor vegetative cover, including slough (shallow slide) areas and gullies up to 1 foot deep. The crest did not exhibit any unusual deformation or misalignment, but erosion rills and gullies have begun headcutting at the downstream edge of the crest.

#### **Wastewater Evaporation Pond #10**

Most of Pond #10 is an at-grade impoundment; the southeast corner is the only location at which there is a dike. Vegetative cover on the downstream slope is generally poor, with minor erosion rills. No evidence of slope failure, slumping, or seepage was observed on the downstream slope, and the crest is in good condition.

#### CONCLUSIONS AND RECOMMENDATIONS

There was no evidence of significant distress that would indicate immediate concern regarding the integrity of the wastewater pond dikes. As such, it is concluded that the dikes are performing as designed with respect to water retention, but not with respect to erosion control. It appears that a widespread erosion problem is negatively affecting the exterior slope of the main containment dike around ponds 6 through 10. Several items should be addressed in order to mitigate/prevent future or current progressive deficiencies. The recommendations presented below address those items as well as the continued care and routine maintenance of the facility:

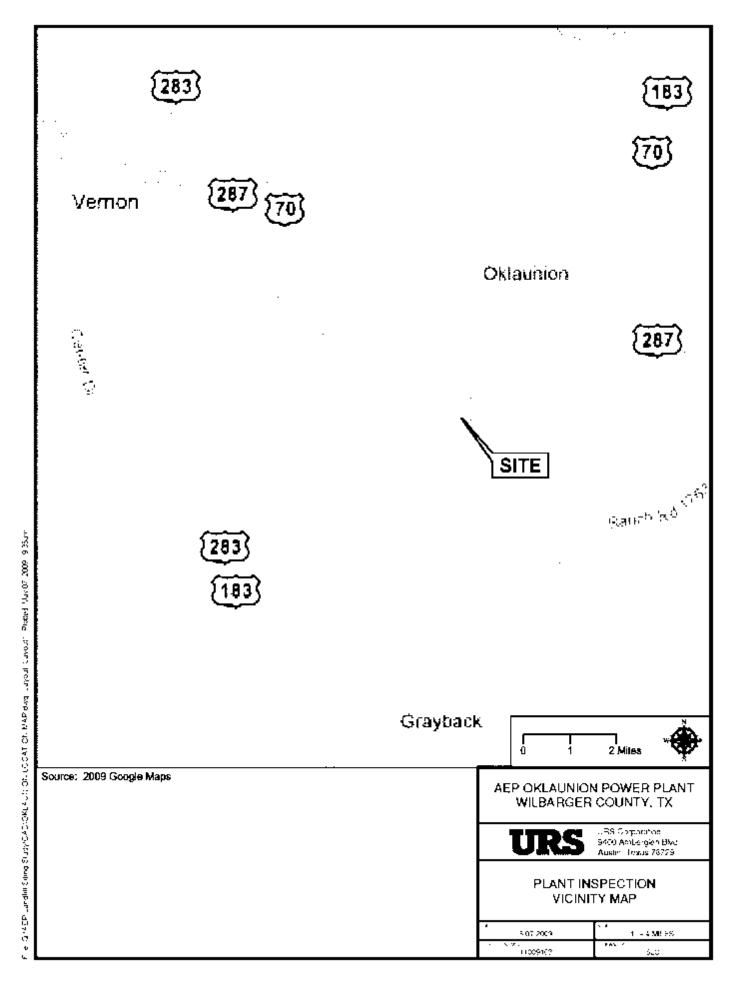
- 1. Any erosion gullies and slough areas that are encountered should be stabilized as soon as possible. Erosion gullies and slough areas may be stabilized by re-dressing the slope and placing riprap or revegetating depending on the slope gradients and propensity for concentrated water flow.
- 2. The upstream erosion at Pond #7 should be mitigated as soon as possible, and can be achieved either by placing rip rap on the slope or by constructing a wall to dissipate wave energy.
- 3. Vegetation should be established on the bare slopes of Wastewater Evaporation Ponds # 6, 8, 9, and 10. The soils in the area are highly erosive as evidenced by the deep gullies. The U.S. Dept. of Agriculture Natural Resource Conservation Service (NRCS) office can provide suitable seed mix design for the local climate and soils.
- 4. The earth fill slopes of the dikes should be maintained free of excessive brush and woody vegetation. It appears that AEP has been diligent in these efforts, however, it is important to establish a grass cover as soon as possible after disturbing the ground for brush cutting activities. Grassed areas should be mowed regularly to prevent the growth of woody vegetation.
- 5. The small trees near the toe of the outfall spillway at Pond #7 should be removed.

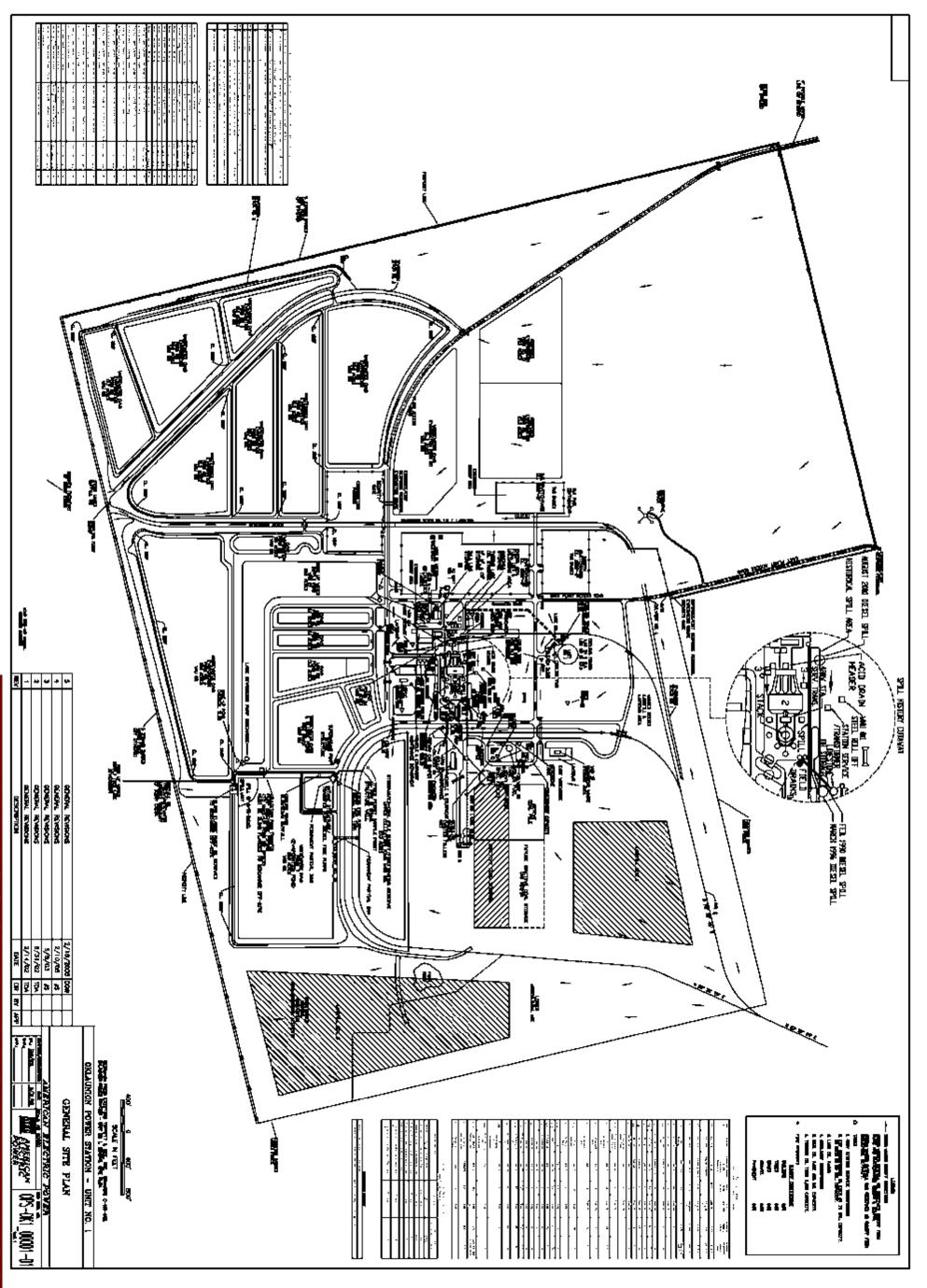
- 6. Monitoring procedures and maintenance activities should be implemented in coordination with the AEP Geotechnical Engineering Group.
- 7. If allowable under state environmental regulation, URS recommends that AEP consider utilizing some of the water that would otherwise go to evaporation ponds to irrigate the slopes of the dikes. This would promote the growth of healthy grass ground cover, thus reducing future crosion damage. If implemented, it should be done after the presently eroded areas are repaired and re-seeded.

Based on the inspection and review of relevant documents, URS Corporation believes that the Oklaunion Power Station wastewater ponds have a general satisfactory appearance and are currently in satisfactory condition. Inspections and monitoring should continue. If you have any questions with regard to this report, please do not hesitate to contact Mr. Colin J. Young, P.E. at 512,419,5903.

## APPENDIX A

VICINITY MAP AND PLAN VIEW





## APPENDIX B

# INSPECTION PHOTOGRAPHS

Page 1 Photo #1 Spillway on downstream side of Wastewater Evaporation Pond #7. Photo #2 Erosion gullies on east downstream bank of Wastewater Evaporation Pond #6. Photo #3 Toe of south embankment for Pond #6, looking west.

## Page 2 Photo #4 South crest and downstream slope of Pond #6. looking east. Photo #5 Erosion gullies on downstream slope at southwest corner of Pond #6.



Close up view of erosion gullies on Pond #6.



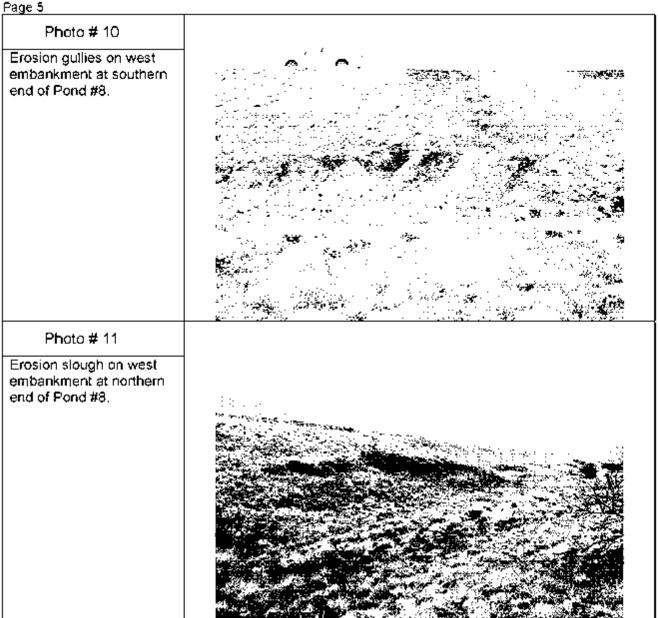
Photo #7

Downstream side of west embankment at Wastewater Evaporation Pond #9. Notice erosion gullies.



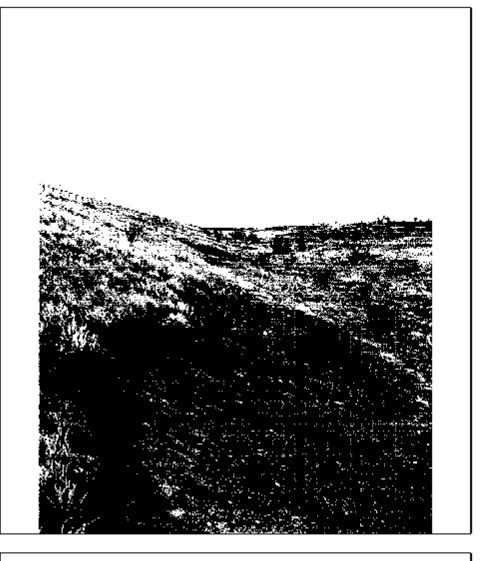
April 2, 2009 Oklaunion Power Plant - Dam and Dike Inspections

## Page 4 Photo #8 West downstream slope on southern end of Wastewater Evaporation Pond #8. Notice erosion gullies. Photo #9 Erosion scarp on west embankment at southern end of Pond#8.



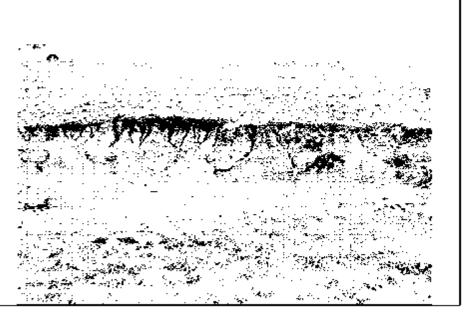
#### Photo # 12

Close up view of erosion slough on west embankment at northern end of Pond #8.



#### Photo # 13

Erosion scarp on west embankment at northern end of Pond #8.



April 2, 2009 Oklaunion Power Plant — Dam and Dike Inspections Page 7

# Photo # 14 Erosion channel at northern toe of embankment for Pond #8.



### APPENDIX A

### Document 6

Inspection Report 8.04.10

### DAM & DIKE INSPECTION REPORT

OKLAUNION POWER STATION WASTEWATER POND COMPLEX VERNON, TX

INSPECTION DATE August 4, 2010

PREPARED BY With K Style DATE 10 29-1010

William R. Smith, P.E.

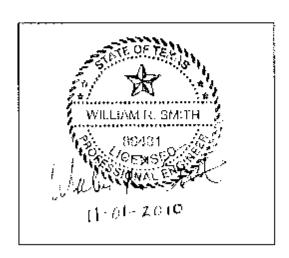
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Gary F. Zych, P.E.:

APPROVED BY A PROVED BY A PROVED DATE 11/2/2016

Gary F., Zych, P.E.

Manager - Geotechnical Engineering



PROFESSIONAL ENGINEER
SEAL & SIGNATURE

#### DAM AND DIKE INSPECTION REPORT OKLAUNION POWER STATION WASTEWATER POND COMPLEX YEAR 2010 GERS-10-040

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APPENDIX A: VICINITY MAP AND PLAN VIEW

APPENDIX B: INSPECTION PHOTOGRAPHS

#### INTRODUCTION

American Electric Power Service Corporation's (AEPSC) Civil Engineering Division administers the Oklaunion Power Station Dam Inspection and Maintenance Program (DIMP). As part of the DIMP, staff from the Geotechnical Engineering Services Section periodically conducts dam and dike inspections. The 2010 inspection of the wastewater pond complex dikes at Oklaunion Station was performed by Mr. William R. Smith, P.E. of AEPSC Civil Engineering. The report presents a summary of the inspection and an assessment of the condition of the facilities.

The inspection was performed on August 4, 2010. Mr. Steve Lewis, maintenance supervisor at the Oklaunion Plant, was the facility contact and provided access and coordination activities. Weather conditions were clear with good visibility, winds were from the southwest at approximately 1 to 5 mph and temperatures ranging between 90 and 95°F. Inspection observations were briefly discussed with Mr. Lewis after completion of the field work.

#### General Information

The Oklaunion Power Station is owned by American Electric Power and is located at 12567 FM Rd 3430, Vernon, TX 76384. The plant is a coal-fired facility, which includes a number of wastewater evaporation ponds containing cooling tower blowdown. A few of the wastewater ponds also contain some by-products of the coal combustion process.

Earth-fill dikes retain plant wastes until they are sufficiently dry to be hauled away and landfilled. The plant has 13 wastewater evaporation ponds, with a total area of 385.9 acres. In addition, there is one make-up water supply pond (52.8 ac.), a coal pile runoff pond (27.3 ac.), and a wastewater/sludge pond (22.6 ac.). A facility map and plan view are provided in Appendix A.

For reference purposes in this report, the main evaporation pond complex area refers to the group of ponds located on the south side of the plant access road. Two recently constructed diked ponds, #12 and #13, are situated north of the plant access road separately from the main evaporation pond complex area.

#### SUMMARY OF VISUAL OBSERVATIONS

The summary of the visual observations presented berein uses terms to describe the general appearance or condition of an observed item, activity or structure. The meaning of these terms is understood as follows:

Good: A condition or activity that is generally better or slightly better

than what is minimally expected or anticipated from a design or

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Fair/Satisfactory: A condition or activity that generally meets what is minimally

expected or anticipated from a design or maintenance point of

view.

Poor: A condition or activity that is generally below what is minimally

expected or anticipated from a design or maintenance point of

view.

Minor: A reference to an observed item (e.g. erosion, seepage, vegetation,

etc.) where the current maintenance condition is below what is normal or desired, but which is not currently causing concern from

a structure safety or stability point of view.

Significant: A reference to an observed item (e.g. crosion, seepage, vegetation,

cracks, concrete surface etc.) where the current maintenance program has neglected to improve the condition. Usually, conditions that have been identified in previous inspections, but

have not been corrected.

Excessive: A reference to an observed item (e.g., erosion, seepage, vegetation,

cracks, concrete surface etc.) where the current maintenance condition is above or worse than what is normal or desired, and which may have affected the ability of the observer to properly evaluate the structure or particular area being observed or which may be a concern from a structure safety or stability point of view.

Results of the visual inspection performed on August 4, 2010, are summarized below, with inspection photographs included as Appendix B. The inspection focused on the exterior western and southern dikes, impounding the main complex area, and the dikes enclosing the newly constructed Ponds #12 and #13 as these were the only locations where dike failure could lead to uncontrolled release of impounded water off-site.

#### Outfall Spillway

The outfall spillway is located on the south dike of Wastewater Evaporation Pond #7, and the discharge channel runs adjacent to the east dike of Pond #6. The spillway has been

blocked by a concrete wall, approximately 4 ft, in height, built across the spillway channel at the control section.

The spillway control section is in generally in poor condition with extensive cracking of concrete elements. A general view of the spillway control section is provided in Photo 1 and a closer view showing the extensive cracking of the concrete is shown in Photo 2, taken in March 2010. The shore protection revetment of stacked, sand-cement mix paper bags, shown in Photo 1, was added in front of the spillway control section and extending along the shoreline beyond the spillway in both the left and right directions in 2009. This revetment was added to provide wave crosion protection and to replace the front portion of the control section that had previously been undermined from wave crosion and broken off as shown in Photo 3, taken in May 2008.

The spillway discharge channel was in generally fair condition. All brush and trees noted in the downstream channel during the 2009 inspection had been cleared. However, the channel bed was barren of a protective grass cover because of the recent clearing as depicted in Photo 4.

#### Wastewater Evaporation Pond #1

Pond #1 is located at the northwest corner of the main evaporation pend complex area. The upstream slope of this embankment was under construction, being refined with a compacted clay and HDPE composite liner system, at the time of inspection. As a consequence, the crest and upstream slope were not observed,

The downstream slope was in generally fair condition. There were no observed signs of slope failure, slumping, or seepage on the slope. Vegetative cover was well-established but about 2 feet in height precluding a thorough inspection of the slope. Significant erosion from stormwater runoff was observed to have cut the foc of the slope along the entire slope. This is shown in Photo 5. This could eventually lead to stability concerns if left unaddressed.

#### Wastewater Evaporation Pond #6

Pond #6 is located at the south-central edge of the main evaporation pond complex area. The upstream slope has been buried with solid waste materials to the crest and is not visible as shown in Photos 6 and 7. The crest of the dam appeared to be in good condition with no unusual cracking, rutting, settlement, deformation, or misalignment. Photos 6 and 7 provide views of the crest.

The downstream slope was in overall fair condition. No signs of slope faiture, slumping, or scepage were observed on the downstream slope. However, vegetative cover on the downstream (east and south) slopes of Pond #6 was in fair to prior condition at the time of inspection. The slopes had been seeded with native, perennial grasses in March 2010, shown in Photo 8, but the vegetation at the time of inspection consisted of dead grasses and live weeds 2 to 3 feet in height as shown in Photos 9 and 10. No erosion gullies, as

observed during the 2009 inspection, were noted on the downstream slopes; however, the excessively high vegetation made observation of the entire slope very difficult.

#### Wastewater Evaporation Pond #7

Pond #7 is located on the southeast corner of the main evaporation pond complex area. The upstream slope was in generally fair to poor condition. As noted in the Outfall Spillway section of this report, shore protection revetment in the form of stacked, sand-cement mix paper bags was added in front of the spillway control section that extends along the shoreline beyond the spillway in both the left and right directions as shown in Photo 1. This revetment was added to replace the failed front section of the spillway control section and to provide wave crosion protection for the upstream slope in the area. The stacked-bag revetment itself was in good condition and is providing shore protection within the armored area. However, the soil shoreline immediately beyond each end of the revetment was significantly croded with embankment material sloughing as shown in Photos 11 through 13. The slope area above the revetment was very sparsely vegetated or barren and had many crosion rills developing as shown in Photo 13.

The downstream slope was in generally fair condition. No evidence of crosion, slope failure, slumping, or scepage was observed on the slope. However, vegetative cover on the slope was 2 to 3 feet in height and sparse in some areas at the time of inspection as shown in Photos 14 and 15. The crest of the dam appeared to be in good condition with no unusual cracking, rutting, settlement, deformation, or misalignment.

#### Wastewater Evaporation Pond #8

Pond #8 is located near the western boundary of the main evaporation pond complex area, adjacent to and immediately north of Pond #9. The upstream slope of this embankment is covered with a high-density polyethylene (HDPE) liner and was not directly observable. No undulations, bulges, depressions, or undue stresses on the liner were observed. The crest of the embankment appeared to be in fair condition with no unusual eracking, settlement, deformation, or misalignment. However, at this location the crest has no surface cover of gravel to provide protection from rutting due to vehicular traffic and there is very little, if any, access to the area by vehicle during inclement weather conditions because of the slippery road surface.

The downstream slope was in generally fair condition. There were no observed signs of slope failure, slumping, or seepage on the slope. Vegetative cover ranged from fair to poor with very similar features along the central and southern portions of the slope as those noted for the downstream slope at Pond #6 (recent seeding but dead covergent grasses and live weeds 2 to 3 feet in height). A typical view of the southern portion of the slope is provided in Photo 16. Along the northern portion of the slope, erosion rills have begun to develop in a sparsely vegetated area as shown in Photo 17. An area of significant erosion at the top of the slope due to stormwater ranoff was observed at the northern end of the pond as shown in Photo 18. This could eventually lead to stability concerns if left unaddressed.

#### Wastewater Evaporation Pond #9

Pond #9 is located near the southwest corner of the mein evaporation pond complex area, adjacent to and immediately north of Pond #10. The upstream slope of this embankment is covered with an HDPE liner and was not directly observable. No undulations, bulges, depressions, or undue stresses on the liner were observed. The crest of the embankment appeared to be in fair condition with no unusual cracking, rutting, settlement, deformation, or misalignment. However, at this location the crest has no surface cover of gravel to provide protection from rutting due to vehicular traffic and there is very little, if any, access to the area by vehicle during inclement weather conditions because of the slippery road surface.

The downstream slope was in generally fair condition. There were no observed signs of seepage on the slope. Vegetative cover ranged from fair to poor with very similar features as those noted for the downstream slopes at Ponds #6 and #8 (recent seeding but dead emergent grasses and live weeds 2 to 3 feet in height). A typical view of the slope is provided in Photo 19. One area of sparse vegetation and incipient slumping was noted at the northern end of the slope near the southern border of adjacent Pond #8. This area is depicted in Photo 20.

#### Wastewater Evaporation Pond #10

Pend #10 is located at the southwest corner of the main evaporation pond complex area. The upstream slope of this embankment is covered with an HDPE liner and was not directly observable. No undulations, bulges, depressions, or undue stresses on the liner were observed. The crest of the embankment appeared to be in fair condition with no unusual cracking, rutting, settlement, deformation, or misalignment. However, at this location the crest has no surface cover of gravel to provide protection from rutting due to vehicular traffic and there is very little, if any, access to the area by vehicle during inclement weather conditions because of the slippery road surface. A view of the crest from the southwest corner of the pond, looking north is provided in Photo 21.

The downstream slope was in generally fair condition. No evidence of crusion, slope failure, slumping, or scepage was observed on the slope. Vegetative cover ranged from fair to poor with very similar features as those noted for the downstream slopes at Ponds #6, #8, and #9 (recent seeding but dead emergent grasses and live weeds 2 to 3 feet in height). A typical view of the slope is provided in Photo 22.

#### Wastewater Evaporation Pond #12

Pond #12 is situated north of the plant access road at a location separate from the main evaporation pond complex area. The pond was constructed during the latter part of 2009. The upstream slope of this embankment is covered with an HDPE liner and was not directly observable. No undulations, hulges, depressions, or undue stresses on the liner

were observed. The crest of the embankment appeared to be in good condition with no unusual cracking, rutting, settlement, deformation, or misalignment.

The downstream slope was in generally fair condition. No evidence of crosion, slope failure, slumping, or scepage was observed on the slope. Vegetative cover ranged from fair to poor. A view of the south downstream slope, with the vegetation in fair condition, is provided as Photo 23. A view of the north downstream slope and crest, with the vegetation on the slope in poor condition, is provided as Photo 24.

#### Wastewater Evaporation Pond #13

Pond #13 is situated north of the plant access road at a location separate from the main evaporation pond complex area. The pond was constructed in 2010 with construction complete prior to the date of inspection. The upstream slope of this embankment is covered with an HDPE liner and was not directly observable. No undulations, bulges, depressions, or undue stresses on the liner were observed. The crest of the embankment appeared to be in good condition with no unusual cracking, rutting, settlement, deformation, or misalignment. A view of the crest, in good condition, is provided as Photo 25.

The downstream slope was in generally good condition. No evidence of erosion, slope failure, slumping, or seepage was observed on the slope. Vegetative cover was generally good with some minor areas of sparse vegetation. Vegetation height was about 4 to 5 inches. A view of the south downstream slope is provided as Photo 26.

#### CONCLUSIONS AND RECOMMENDATIONS

Based on the visual observations during the dike inspection at Oklaunion Station, the dikes containing the main evaporation pend complex area and Pend #12 are generally in fair condition, and the dikes containing Pend #13 are in good condition. A summary of our conclusions and recommendations for general maintenance and continued monitoring, as well as any recommendations for remedial activities, is provided as follows.

There was no evidence of significant distress that would indicate immediate concern regarding the integrity of the wastewater pond dikes. As such, it is concluded that the dikes are performing as designed. There were significant areas where the establishment and control of vegetation has been somewhat problematic, but the widespread crosion problems over exterior slope of the main containment dike around ponds 6 through 10 noted in the 2009 report had been addressed through an extensive program of regrading and seeding with native perennial grasses. Recent communication with the plant, since the date of inspection, indicates that areas where dead grasses were observed during the inspection are re-emerging with native grass species that were in the original seed mix, and that the dead grasses referred to in this report were from a species in the mix that was

used to establish a quick first-year cover that was stressed by the dry conditions prior to the inspection,

#### Recommendations for General Maintenance and Monitoring Activities

- Any crosion gullies and slough areas that are encountered should be stabilized as soon as possible. Erosion gullies and slough areas may be stabilized by redressing the slope and placing riprap or revegetating depending on the slope gradients and propensity for concentrated water flow.
- The earth fill slopes of the dikes should be maintained free of excessive brush and
  woody vegetation. It is important to establish a grass cover as soon as possible
  after disturbing the ground for brush cutting activities.
- Grassed areas should be moved regularly. Moving at least twice per year and maintaining vegetation height at a maximum of 6 to 8 inches is recommended. High vegetation obstructs visual observations during inspection, encourages burrawing animal activity, and thins the ground cover by decreasing vegetation stem density and encouraging the growth of annual grasses and other invasive weeds. Any areas that are not accessible to moving equipment should be controlled by the use of weed trimmers, power brush-cutters, or other suitable vegetation control processes.
- Any animal burrows on the dikes should be filled with an impervious meterial or comentious grout, dressed with topsoil, and regraded followed by seeding any disturbed ground with native grasses to establish a complete ground cover for evosion protection.
- Monitoring procedures, maintenance activities, and reporting should be implemented in coordination with AEP Civil Engineering.

#### Recommendations for Specific Remedial Activities

- Shore protection beyond the ends of the revetment around the spiffway at Wastewater Pond #7 should be added to prevent further erosion of the dike at these two locations. Extension of the revetment is not recommended since this would likely transfer the problem to the ends of the new revetment. We recommend regrading to a uniform slope and installing riprap shore protection over a geotextile or gravel filter layer.
- An engineering analysis should be performed to verify that the blocking of the spillway at Wastewater Pond #7 will not cause the dikes to be overtopped during a severe storm if this has not been performed.
- The discharge channel at the spillway at Wastewater Pond #7 should be seeded with native, non-invasive perennial grasses for the entire length where it is

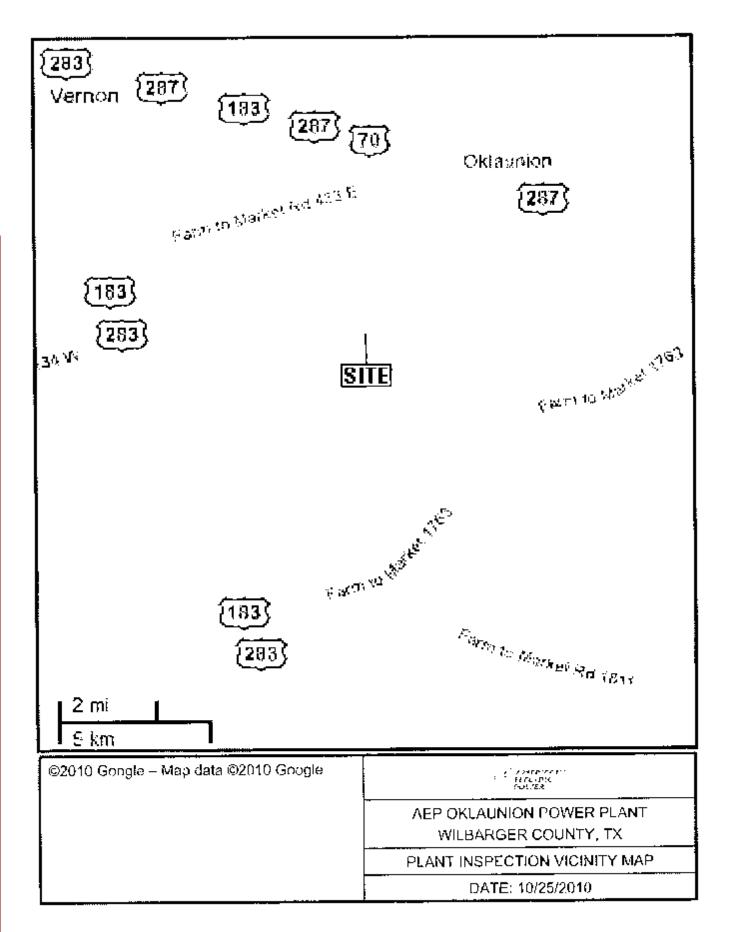
adjacent to the east dike of Wastewater Pond #7 to suppress the growth of woody vegetation, invasive weeds and annual grasses. The barren upstream slope at Pond #7, extending about 250 feet left of the spillway where the embankment meets natural ground and about 150 feet to the right of the spillway, should be regraded and similarly seeded to prevent further development of crosion rills.

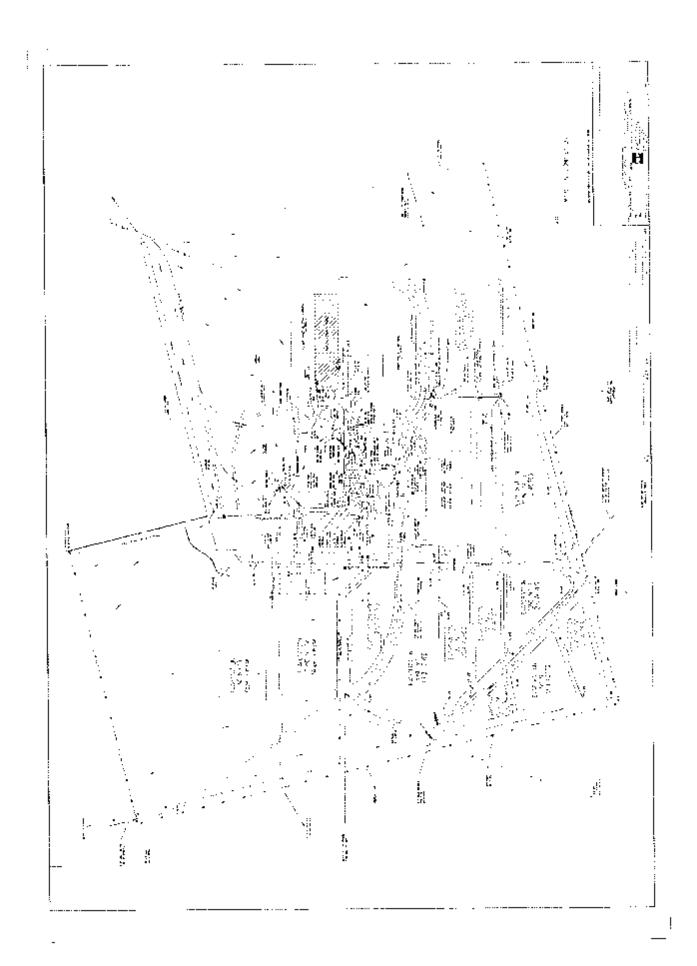
Erosional features identified in this report, specifically the cutting away at the toes
of the slopes at Ponds #1 and #8, and the incipient slumping at the north end of
Pond #9 should be regraded to a uniform slope, with any croded material replaced
with suitable compacted fill, and seeded with native, non-invasive percunial
grasses to suppress the growth of woody vegetation, invasive weeds and annual
grasses.

If you have any questions with regard to this report, please do not hesitate to contact Mr. William R. Smith, P.E. at 614-716-2906 (Audinet: 200-2906) or Gary Zych, P.E. at 614-716-2917 (Audinet: 200-2917).

#### APPENDIX A

VICINITY MAP AND PLAN VIEW

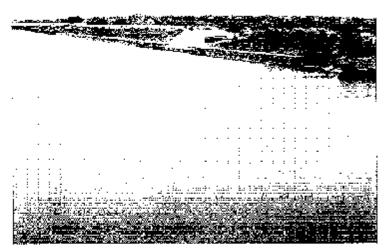




#### APPENDIX B

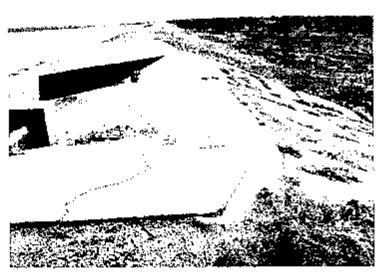
#### INSPECTION PHOTOGRAPHS

## APPENDIX B OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



#### Photo 1

General view of Pond #7 spillway area showing the control section blocked by a concrete wall and recently installed shore protection revetment, in front, in good condition but erosion progressing beyond revetment.



#### Photo 2

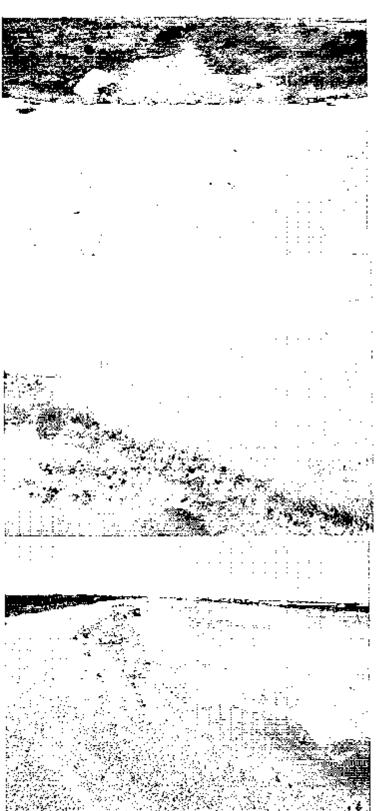
Pond #7 photo taken in March 2010 showing spillway control section in generally poor condition with extensively cracked concrete elements. The concrete wall blocking potential flow through the spillway is at the left in the photo.



#### Photo 3

Pond #7 photo taken in May 2008 showing failed front of spillway control section that was replaced in 2009 with the revetment shown in Photo 1.

#### APPENDIX B OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



#### Photo 4

The discharge channel downstream of the spillway was cleared of woody vegetation and brush. However, the channel was barren.

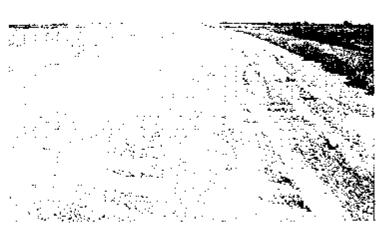
#### Photo 5

Typical view of downstream slope at Pond #1 looking north. Note significant erosion cutting along the toe of the slope.

#### Photo 6

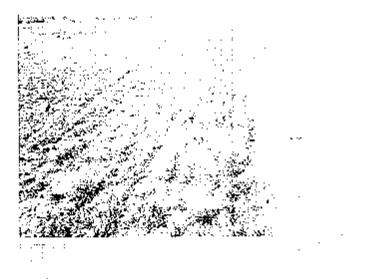
Crest and buried upstream slope of Pond #6 looking west from near the southeast corner of the pond.

#### APPENDIX B OKLACNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



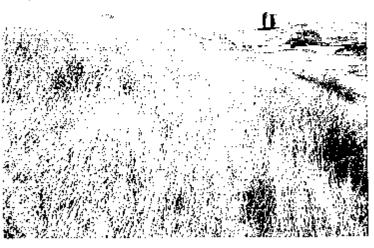
#### Photo 7

Crest and buried upstream slope of Pond #6 looking east from near the southwest corner of the pond.



#### Photo 8

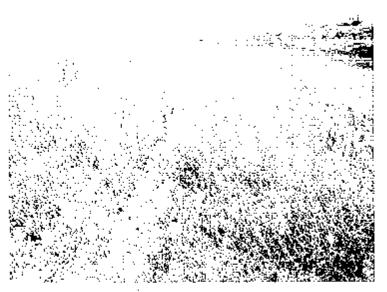
Downstream slope of east dike at Pond #6 in March 2010 sceded with native, perennial grasses.



#### Photo 9

Downstream slope of cast dike at Pond-#6 at time of inspection with vegetative cover of dead grasses and live weeds 2 to 3 feet in height.

## APPENDIX 8 OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



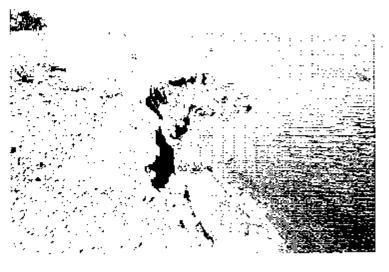
#### Photo 10

Downstream slope of south dike at Pond #6 at time of inspection with vegetative cover of dead grasses and live weeds 2 to 3 feet in height. The biodegradable cord from recent seed matting installation is visible in the photo foreground.



#### Photo 11

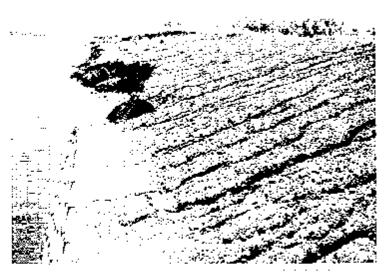
Pond #7 upstream slope at spillway area with significant erosion progressing around the western end of the shore protection revetment. The western end of the revetment is at the bottom right in the photo.



#### Photo 12

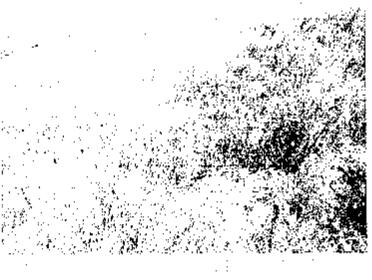
Pond #7 upstream slope immediately east of the revetment-reinforced spillway area, looking west, with significant wave erosion progression and barren slope.

## APPENDIX 6 OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



#### Photo 13

Pond #7 upstream slope area above the east end of the shore protection revetment around the spillway, looking east, with many crosion rills forming on the barren ground and embankment crosion beyond the end of the revetment (opposite view from Photo 12).



#### Photo 14

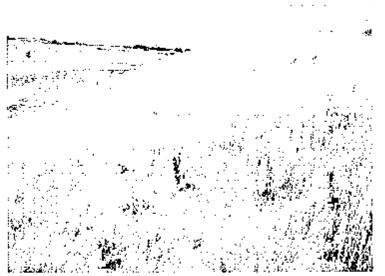
Downstream slope at Pond #7 with grass cover at 2 to 3 feet in height over most of the slope and some sparsely vegetated areas with a cover of broomweed and other native weedy vegetation.



#### Photo 15

Downstream slope at Pond #7 near spillway discharge channel with grass cover at 2 to 3 feet in height and sparsely vegetated areas with a cover of broomweed and other native weedy vegetation.

#### APPENDIX B OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



#### Photo 16

Southern portion of downstream slope at Pond #8 with vegetative cover of dead grasses and live weeds 2 to 3 feet in height.



#### Photo 17

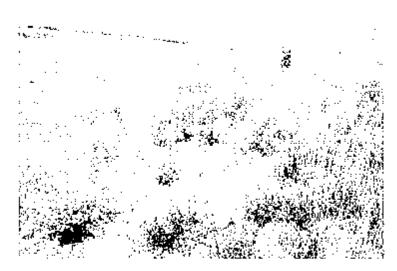
Northern portion of downstream slope at Pond 48 with development of crosion rills at a barren area.



#### Photo 18

Significant erosion cutting at the toe of the north end of the downstream slope at Pond #8.

#### APPENDIX IS OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



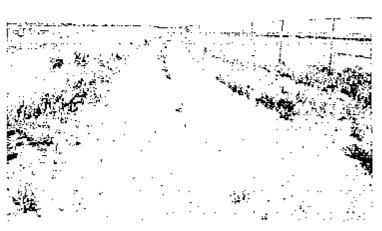
#### Photo 19

Downstream slope of west dike at Pond #9 with vegetative enver of dead grasses and live weeds 2 to 3 feet in height along with some sparsely vegetated areas.



#### Photo 20

Sparsely vegetated area with incipient slumping at the north end of the western dike at Pond #9, looking north.



#### Photo 21

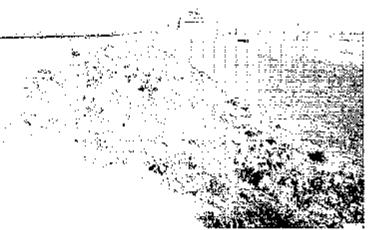
View of crest of western dike from southwest corner of Pond #10 looking north. The crest along the west side of Ponds #8, #9, and #10 has no surface cover of gravel.

## APPENDIX 12 OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS



#### Photo 22

Downstream slope of west dike at Pond #10 with vegetative cover of dead grasses and live weeds 2 to 3 feet in height and a sparsely vegetated area in the photo foreground.



#### Photo 23

Downstream slope of south dike at Pond #12 with recently planted vegetation in fair condition.



#### Photo 24

Downstream slope and crest of north dike at Pond #12 with recently planted vegetation in poor condition and crest in good condition.

## APPENDIX D OKLAUNION WASTEWATER POND COMPLEX DIKE INSPECTION PHOTOGRAPHS

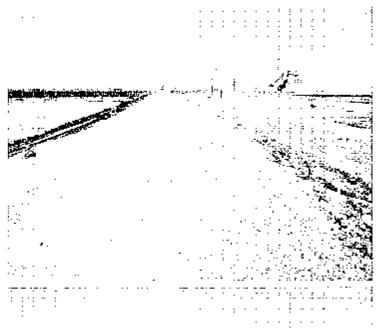


Photo 25

Crest of south dike at Pond #13 in good condition.



Photo 26

Downstream slope of south dike at Pond #13 with recently planted vegetation in good condition.

### APPENDIX A

### **Document 7**

TCEQ 2009 Inspection Report

### Appendix A: Inspection Report



### Inspection Results—Dam Conditions

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Guidelines for Operation and Maintenance of Danis in Texas

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Guidelines for Operation and Maintenance of Dams In Texas	
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Guidelines for Operation and Maintenance of Danis in Texas

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Guidelines for Operation and Maintenance of Dema in Texas

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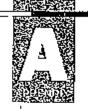
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TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

## APPENDIX A

## **Document 8**

TCEQ 2010 Inspection Report



## Appendix A: Inspection Report

## Inspection Results—Dam Conditions

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Water supply has in ceest of dam. 🗇 Other:	Type of pizetien:
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Guidelines for Operation and Maintenance of Dams in Texas

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Reservoir Drawdown Capability  Maximum Drawdown:	Method as Diawdown:
Baskup Power (2) Piesent (2) Adap	

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TEXAS COMMISSION ON ENVIRONMENTAL QUALITY



## Suidelines for Operation and Maintenance of Dams in Texas

## Inspection Monitoring Form

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Inspector
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Item Reing Monitored
Extent of Area
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Current Description
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Change From Previous Inspections
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TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

## APPENDIX A

## Document 9

Evaporation Pond No. 6 Stability Analysis, June 10, 2011 June 10, 2011 011-11497-043



Mr. William R. Smith, P.E. American Electric Power 1 Riverside Plaza Columbus, OH 43215

Re: Evaporation Pond No. 6 Stability Analysis

Oklaunion Power Station, Evaporation Pond Complex

Vernon, Texas

Dear Mr. Smith:

BBC&M Engineering. Inc (BBCM) has completed stope stability analyses of existing Evaporation Pond No. 6 located at the Oklaunion Power Station in Vernon, Texas. The purpose of this report is to summarize our work and demonstrate that the slope stability analyses performed for the cross-sections examined exhibit adequate factors of safety relative to typical US Army Corps of Engineers (COE) requirements.

### INTRODUCTION

Evaporation Pond #6 is located on the south side of the evaporation pond complex. The pond was constructed as a continuous upground earthen embankment with 3H:1V inboard and outboard slopes and crest width of 20 feet. The design elevation of the crest is 1208 feet, msl, and the maximum water level Elevation is 1205 feet, msl, resulting in a minimum freeboard of 3 feet. The inboard slopes are lime stabilized to a minimum depth of 2 feet from the maximum water level to approximately 8 feet beyond the toe.

### SLOPE STABILITY ANALYSIS

### Methodology

Procedures established by the United States Army Corps of Engineers in the *Slope Stability* Manual (EM-1110-2-1902) were followed for the analysis of the evaporation pond earth dam. The following loading conditions were considered for this project.

Design Loading Condition	FS,,,,	Analyzed Slopes
Rapid Drawdown from Max Water Level	1.3	Inboard
Steady-State Seepage at Max Water Level	1.5	Inboard & Outboard
Steady-State Seepage with Surcharge Water Level	1.4	Outboard
Seismic	1.0	Inboard & Outboard

Although there is currently no mechanism in place within the pond for an uncontrolled drawdown of the water level, BBCM performed a rapid drawdown analysis using the conventional method whereby the phreatic surface is positioned at the drawdown level and extended up the inboard embankment slope to the maximum water elevation and effective stresses are used to estimate the undrained shear strengths that would exist during rapid drawdown. A 10 foot drawdown was considered to occur from the maximum operating water level for this analysis. This condition assumes a steady state seepage condition has been reached at the maximum water level prior to the water level being drawn down in a rapid manner (excess pore pressures cannot dissipate).

The End of Construction loading condition was not performed as the pond was constructed in the 1980s and the embankments have not been modified since that time. Slope stability of the outboard slope was also analyzed for the surcharge loading condition whereby a surcharge water level equal to the top of the crest was analyzed with steady-state seepage conditions as developed from the maximum water level. Seismic slope stability analyses were performed based on a pseudo-static force slope stability approach.

The stability analyses were performed with the aid of the computer program SLIDE™ (Version 6.0) developed by Rocscience, Inc. Spencer's method (Spencer, 1973) was utilized in the program to perform 2-D limit equilibrium slope stability analyses with a deterministic approach. The critical slip surface corresponding to the lowest factor-of-safety is shown in the graphical output, presented in the Appendix. Additional factors of safety are shown to demonstrate the approximate factors of safety for failure surfaces in other locations.

### **Cross Sections**

Two surface profiles, designated Cross-Section A and Cross-Section B were developed from the existing topographic data provided by AEP. Both cross-sections are located near the southwest corner, as shown on the Plan of Cross-Sections presented on Plate 1 of the Appendix, where the perimeter drainage channels outlet resulting in the maximum embankment height. It should be noted that the perimeter drainage channels are only utilized during rainfall events, and are otherwise dry throughout the year. The inboard toe elevation of the Pond near the cross-sections is 1188 feet, msl. Cross-section A was chosen to carry out the analysis as it represents the maximum embankment height and the as-built outboard slopes are slightly steeper than cross-section B. The outboard toe at Cross-Section A is near Elevation 1185, resulting in an embankment height of 23 feet. Cross-sections A and B are shown on Plate 2 of the Appendix.

### **Shear Strength Parameters**

Shear strength and unit weight values were developed by BBCM for recently constructed Evaporation Ponds 12 and 13 located at the evaporation pond complex based on laboratory index test results, published values and engineering judgment. Additional laboratory index test results were available from borings performed near Pond 6 which were used to verify the strength parameters developed for nearby Ponds 12 and 13. The same strength parameters were used for Pond 6 and are intended to be representative of long-term conditions. The embankment fill was modeled with an effective cohesion value of 50 psf to force the stability program to focus on deeper failure surfaces as historical observations of the slopes have indicated good performance in relation to shallow sloughing failures. The shear strength parameters of the lime-stabilized inboard slope were assumed to be equal to the embankment

Evaporation Pond No. 6 Stability Analysis Oklaunion Power Station Vernon, Texas BBC&M Engineering, Inc.

fill. Strength gain from the lime treatment was assumed negligible for long term conditions as the slope is exposed to moisture and freeze/thaw cycles.

### Groundwater

Data from the Groundwater Monitoring System at the plant was used to develop the phreatic surface levels within the embankments. Three wells are located along the crest of the south embankment of Pond 6 as part of the monitoring system. One of the three wells, which is located near the southwest corner, was used specifically for Cross-Sections A and B. The groundwater elevations reported for this well from November 4, 2010 and March 2, 2011 were 1179.27 feet, msl, and 1179.31 feet msl, respectively. As a reference, the bottom of the drainage channel at Cross-Section A is near Elevation 1185 feet, msl.

### **RESULTS**

Static and seismic analyses were performed for the critical cross-section to determine the factor of safety against rotational failures using drained soil strength parameters. The graphical computer outputs for these analyses have been included with this report in the Appendix as Plates 3 through 8.

Seismic analyses were performed using a pseudo-static analysis with a horizontal seismic coefficient of 0.06g. This coefficient was determined from the 2008 USGS National Seismic Hazard Maps for the "Peak Acceleration (%g) with 2% Probability of Exceedance in 50 Years". This map is provided as Plate 9 of the Appendix.

The results of the analyses indicate acceptable factors of safety for each loading condition. The following table summarizes the lowest factors of safety determined for each analysis case. As noted in the USACE Slope Stability Manual, acceptable values of factors of safety for existing dams may be less than those for design of new dams, considering the benefits of being able to observe the actual performance of the embankment over a period of time.

Loading Condition	Minimum Allowable Factor of Safety*	Slope	Computed Factor of Safety
Rapid Drawdown	1.3	Inboard	1.38
Standy State Seenage (May Mater Level)	1.5	Inboard	2.24
Steady-State Seepage (Max Water Level)	1.5	Outboard	1.69
Steady-State Seepage with Surcharge Water Level	1.4	Outboard	1.69
Soigmin (May ) Mater Loyal)	1.0	Inboard	1.61
Seismic (Max Water Level)	1.0	Outboard	1.45

<sup>\*</sup>Based on USACE EM-1110-2-1902 requirements for new earth dams (advisory for existing dams).

Evaporation Pond No. 6 Stability Analysis Oklaunion Power Station Vernon, Texas BBC&M Engineering, Inc. We appreciate having been given the opportunity to be of continuing service on this project. Please do not hesitate to contact this office if you have any questions with regard to the information provided.

Sincerely,

BBC&M ENGINEERING, INC. Dublin, Ohio

Michael T. Romanello, P.E.

Project Engineer

S 10 1/2

Stephen J. Loskota, P.E.

Vice President

MTR/mr File 011-11497-043 OKLAUNION POND 6 STABILITY.DOC

Submitted: 1 Electronic Copy:

Enclosures: Appendix: Plate 1 - Plan of Cross-Sections

Plate 2 - Cross-Sections A and B

Plates 3 through 8 - Slope Stability Graphical Output

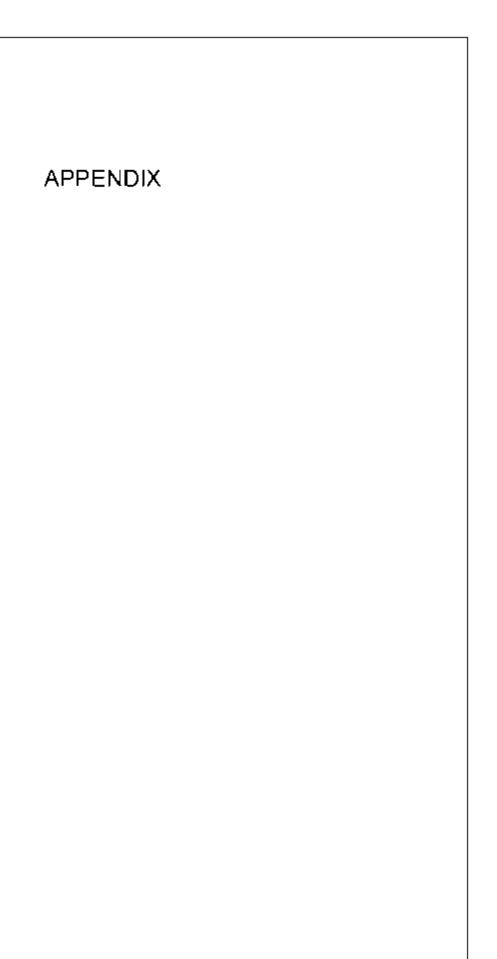
Plate 9 - USGS Seismic Hazard Map

Electronic Copy: Mr. William R. Smith, P.E.

American Electric Power

wrsmith@aepicom

Evaporation Pond No. 6 Stability Analysis Oklaunion Power Station Vernon, Texas BBC&M Engineering, Inc.



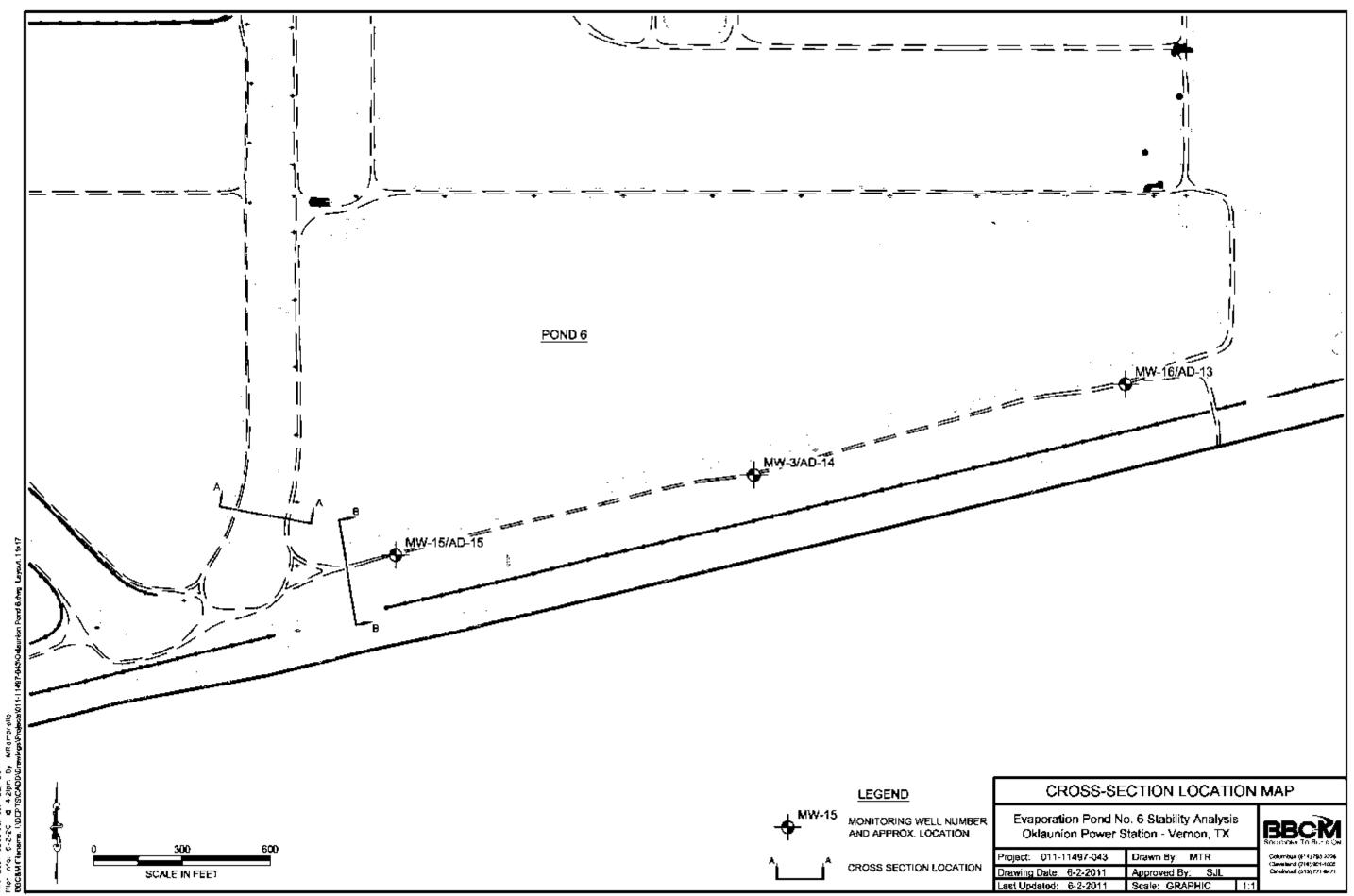


PLATE 1

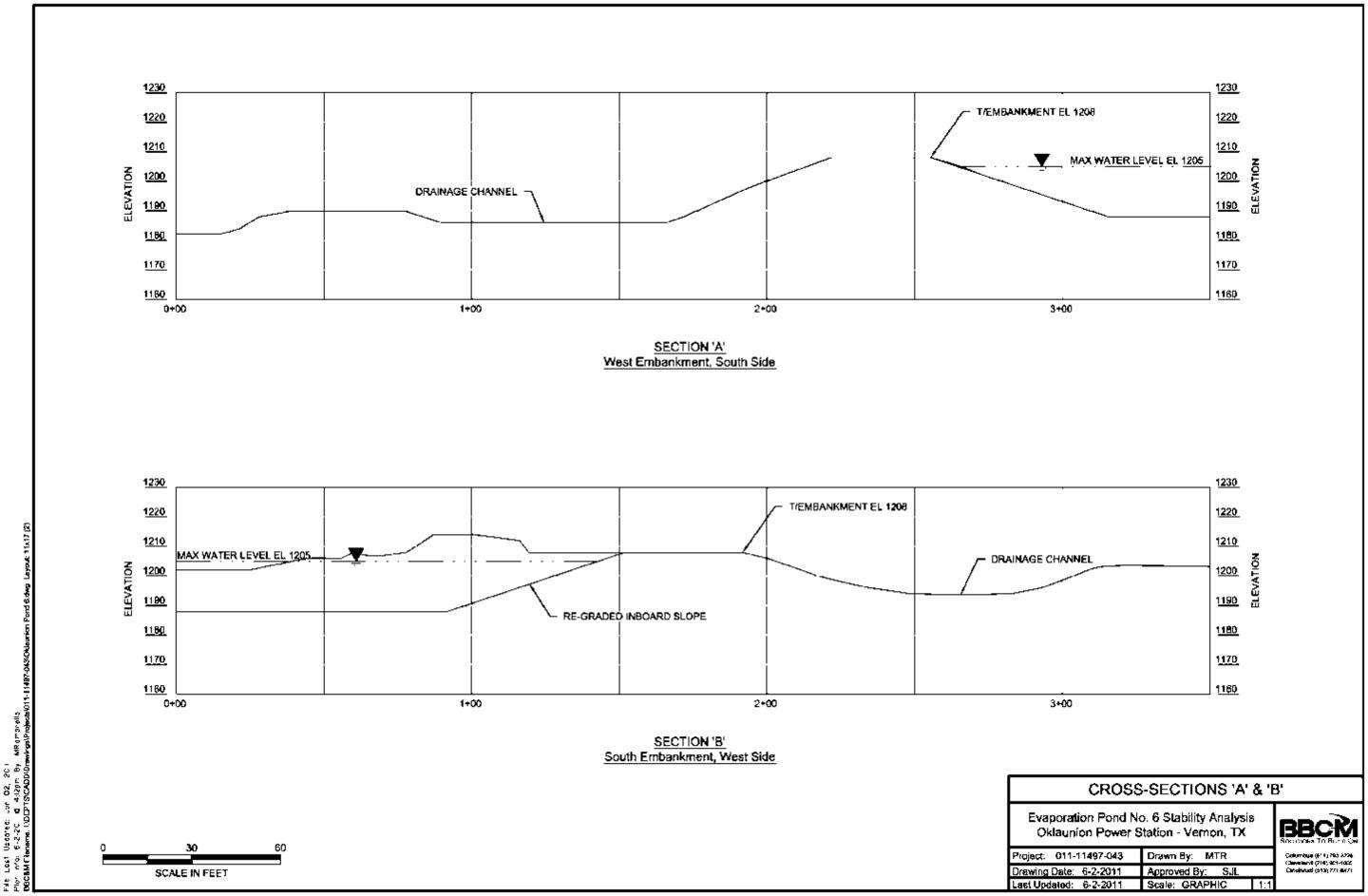
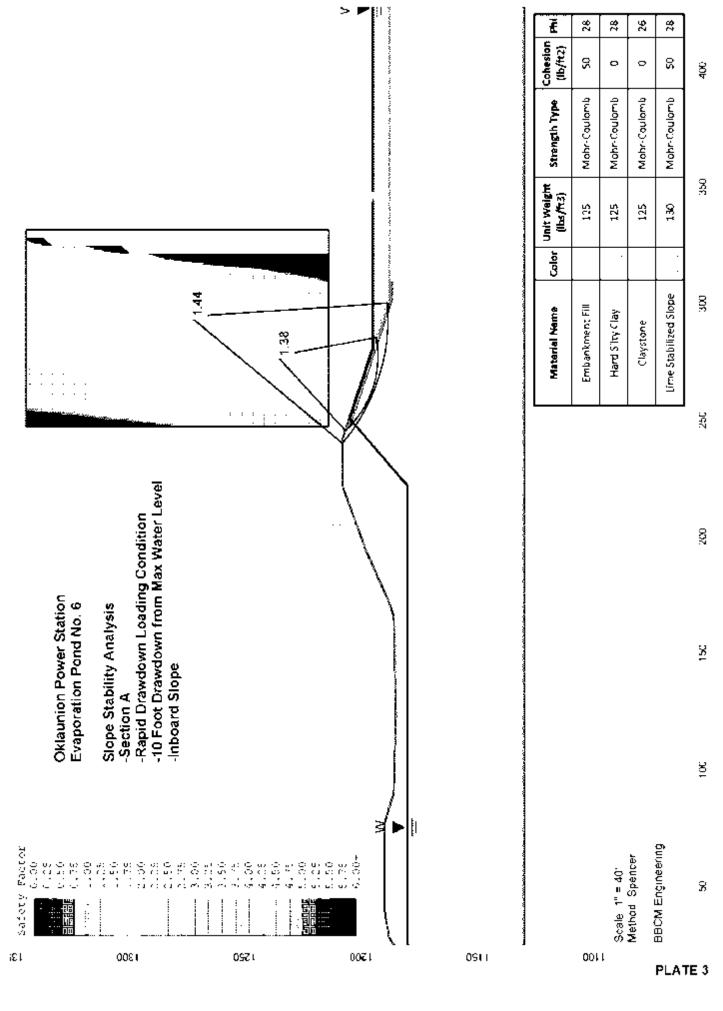
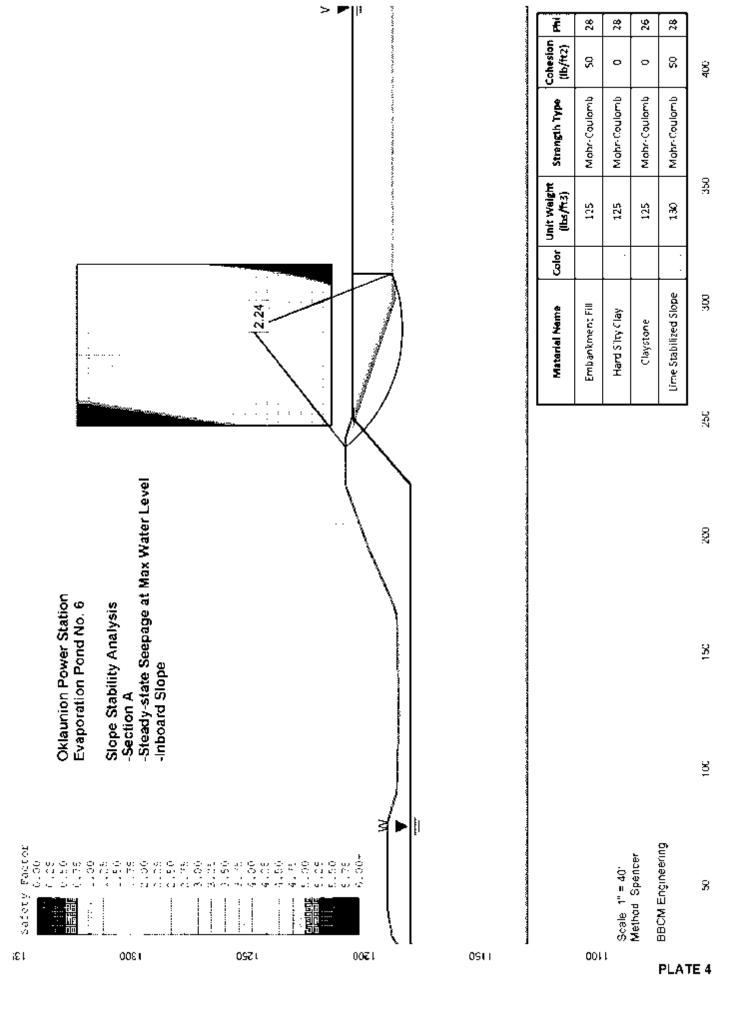
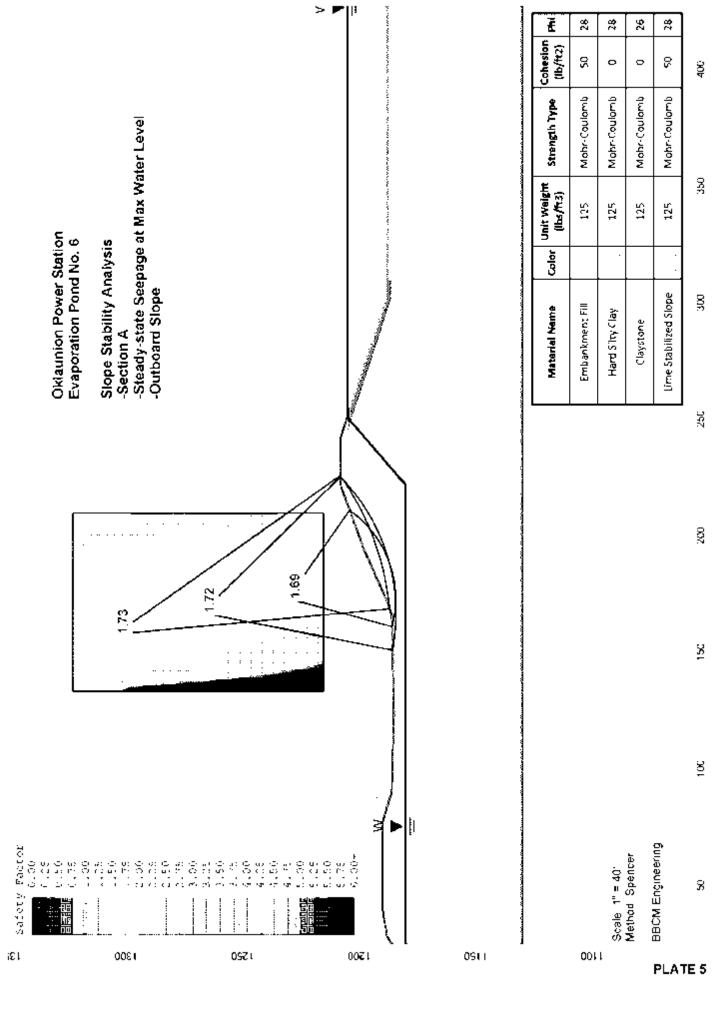
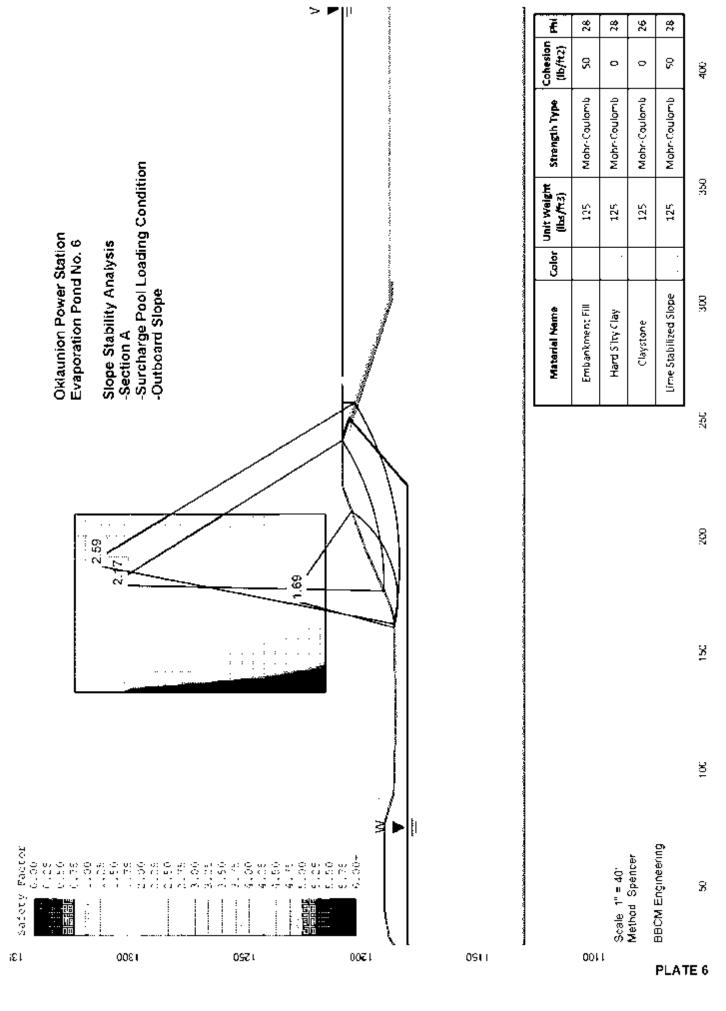


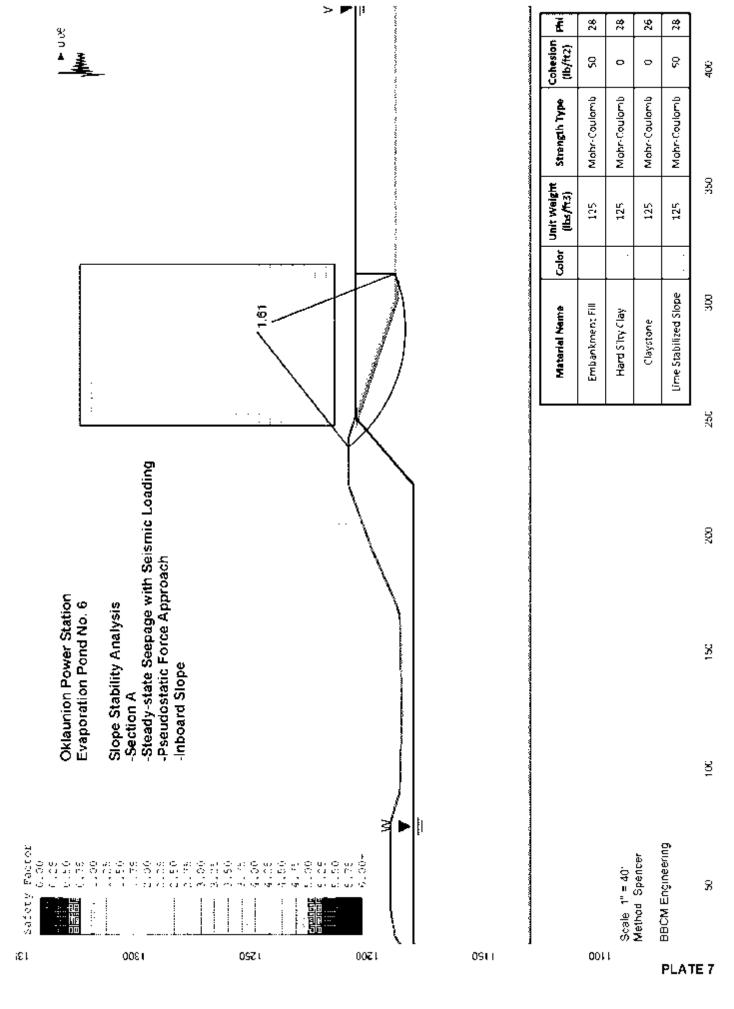
PLATE 2

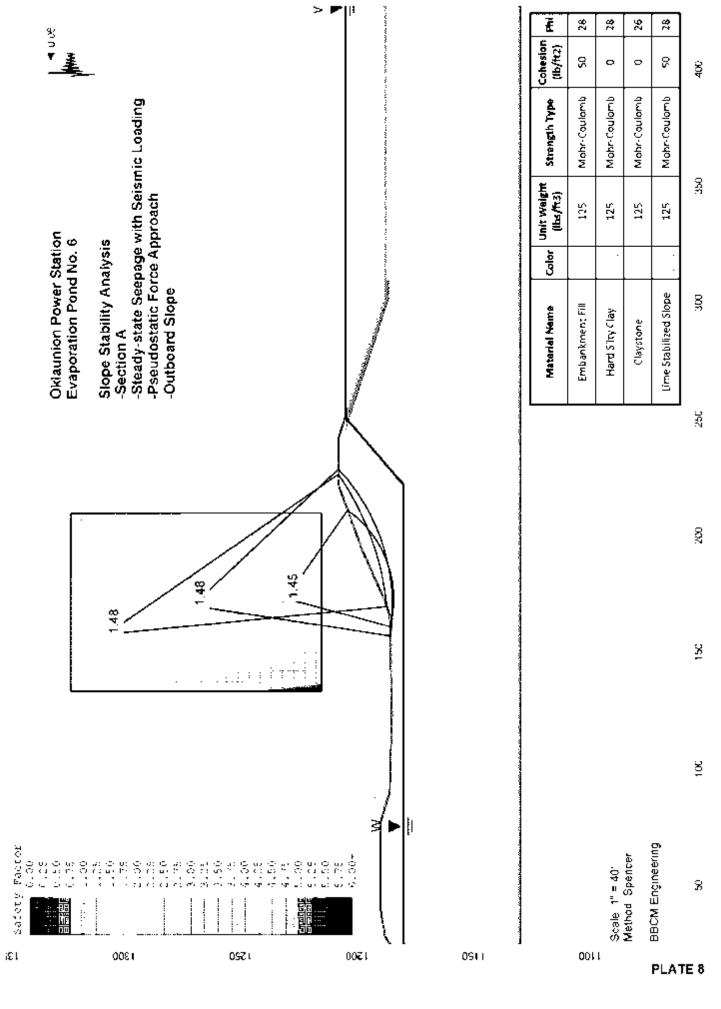












USGS: National Seismic Hazard Maps - 2008

Peak Horizontal Accertation with 2% Probability of Exceedence in 50 Years

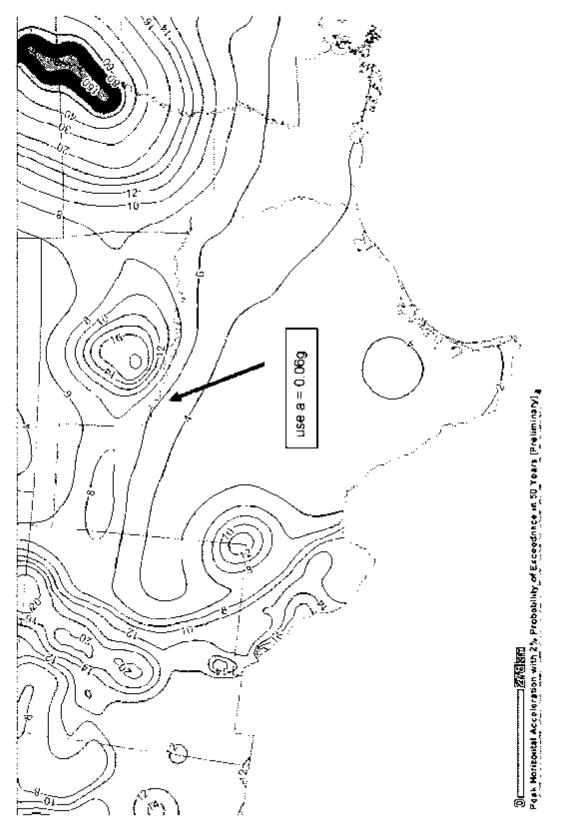


PLATE 9

## APPENDIX A

## Document 10

Pond 6 Waste Water Management Unit, Hydrology and Hydraulic Analysis American Electric Power
Oklaunion Power Plant
Pond 6 Waste Water Management Unit

Hydrology and Hydraulic Analysis

Pond 6 Waste Water Management Unit has been constructed as a partially diked/partially incised pond currently being used as a solid waste management unit. The pond volume has been used to permanently store solids wastes that are removed from the other ponds at the power plant.

The surface area of Pond 6 at the outer edge of the road along the crest of the diking system is 68.6 acres. The crest of the pond is elevation 1208. Presently, the pond has been divided by an internal splitter dike that forms an eastern and western area. Each area has a shallow accumulation of water. The elevation of the water surface is approximately 1202. At this elevation the water surface areas are 5.6 and 11.1 acres for the eastern and western pool areas, respectively. The areas draining to these pools are 36.2 acres to the eastern pool and 32.4 acres to the western pool.

Pond 6 only receives direct rainfall and there are no other flows into the pond area. There is no outlet structure for the pond as it functions purely as an evaporation pond.

A study was conducted to evaluate the hydraulic/storage capacity of the pond during several rainfall events. The basic assumptions of the study were: (a) 100 percent runoff occurred for each rainfall event: (b) the existing pool areas did not increase with rising water levels (treated as vertical walls); (c) no discharge or overflow; and (d) the splitter dike is lower than the crest of the perimeter dike which would allow the two pools to merge during an extreme rainfall event.

The pond system was designed based on a 10-yr, 24 hour rainfall event at the time of permitting in the late 1970's. Since the pond is a waste water management unit, the pond was approved and currently regulated by the Texas Commission on Environmental Quality Waste Water Group. The TCEQ Dam Safety Group does not have jurisdiction on the ponds at the power plant. However, Pond 6 would be categorized as a small size, low hazard structure and the design flood would be the 25% PMF. This analysis was conducted for multiple rainfall events ranging from the 10-year, 24-hour to the 25% 72-hour PMP.

The results of the simplified hydraulic/storage evaluation indicate that the eastern pool area can accommodate a rainfall event equivalent to 10-yr, 24-hr rainfall of 5.5 inches. The western pool area can accommodate a rainfall event equivalent to 25% 72-hr PMP of 11.5 inches. The total Pond 6 area can store a rainfall event equivalent to 25% 12-hr PMP of 8.6 inches without overtopping the perimeter diking system.

Therefore, Pond 6 has adequate storage capacity for events larger than its original and current design basis. The attached provides calculations of area, storage and runoff volumes.

Gary F. Zyen, P.E.

Manager - Geotechnical Engineering Section

AEP Service Corporation

William R. Smith, P.E. Geotechnical Engineer

OKLAUNION PLANT POND # 6

		total	vol ac-#	0.0	249.4	299.2	
	sa 585 x 415	Volume-acit		0.0	83.6	100.3	117.C 16.7
1202	Eastern pool area	Area-ac Volu	<del></del>	9:3	5.6	5.6	5.6
Poal elevation	1160 x 415	Volume-acft		Q:	165.8	198.9	232.1 33.2
Stage - storage data	stem pool area	v Area-ac Vo			.202 11.1	.205 11.1	1,11
ö	ž	ă					

Note: Boxed values are available flood storage in ac-ft

as measured from outer edge of road	å
36.2 ac	32.4 ac
1,577,228 sf	1,412,931 sf
Area draining to Eastern Pool 1,5	guiug

Operating conditions require a minimum 3 feet of freeboard above maximum operating level. Based on the crest elevation of 1208, the max operating level would be elevation 1205.

eas	P40	P40	P.40	P40					
As a conservalive analysis, assume 100 percent runoff from each area draining into the respective gool area	5.5 Value from TP40	6.5 Vatue from TP40	7.3 Value from TP40	8.3 Value from TP40					
unto the res	8.8	6.0	7.3	6.9 6.3	7.7	8.6	9.6	10.8	11.5
area dra.ning	È	Ĕ	بة	-h					
from each	10-yr 24-	25-yr. 24-	50-yr, 25-hr	100-yr. 24-hr	25% PMF				
ercent runaf	ement unit				1000				
stume 100 p	rater manage				ard Design F				
analysis, as	Design criteria as per waste water management unit				TOEQ Dam Safety - Low Hazard Design Flood				
conservative	n cribera as				2 Dam Safel				
As a	Desig				ŢČĘ				

Rainfall values from HMR 51

сшфир

28.5 34.5 38.5 5.5 5.5 5.5

12hr pmp 24hr pmp 48hr pmp 72hr pmp

Total runoff Pend 6	31.46	37.18	41.76	47 48	40.76	49.34	55.06	61.49	65.78
East	16.60	19.61	22.03	25.04	21.50	26.02	29.04	32.44	34.70
West	14.87	17.57	19.73	22 44	19.26	23.31	26.02	29.06	31.08
Runoff volume	10-yr, 24-hr	25-yr, 24-hr	50-yr, 24-hr	100-yr, 24-hr	<b>е</b> нгртр	12hr pmp	24hr pmp	48hr pmp	72hr pmp

## ENGINEERING DEPT. AMERICAN ELECTRIC POWER SERVICE CORP. 1 RIVERSIDE PLAZA COLUMBUS, OHIO

	SHEET /	_OF_ <i>-\f</i> /
DATE 4/2	/// BY 2777	ск
COMPANY_		G.O
DIANT	OKINNOSIMA	)

SUBJECT POND 6 - DAM BREAK

SIMPLIFIED BREACH EVALUATION

FERC GUIDELINES : TH CER C5H

HEIGHT OF POND 6, H= 24 FT

USE BR = 4H = 4(24) = 96 FT

REDWAY YERWOAL SIDE SLOPES.

ESTIMATE PEAK DISCHARGE ASSUMITES BROAD
CRESTED WEIR

 $\varphi = (24)^{32} = 2.6(96)(24)^{3/2}$ 

= 29,300 ofs (VERY CONSERVATIVE)

IF INSTANTANEOUS FAILURE, DEPTH BELOW DAM
IS ESTIMATED AS

y = 49(H)

= 10.7 FT

THE CROSS SECTION LETTING DON PG 294 CONFIRMS
THIS POTENTIAL FLOW DEPTH FOR THE PEAK DISCHARGE

CONCLUSION: THE WORST CASE INSTANTAMENCES

DAM BREAK WOULD GENERATE A MAXIMUM

FLOW DEFTH OF ALMOST I, FEET NEAR THE DAM.

WITHOUT ACCOUNTING FOR THE FLOOD WAVE

ATTENTUATION, A 10 OF RISE IN THE FLOODPEHIN

BELOW WILL ONLY MUNDATE PASTURE LANDS.

## ENGINEERING DEPT, AMERICAN ELECTRIC POWER SERVICE CORP. 1 RIVERSIDE PLAZA COLUMBUS, OHIO

SHEET 2 OF 4

DATE 6/7/11 BY 669 CK.

COMPANY G.O.

PLANT OKLA 40/100

	SUBJECT	POND	6-	DAM	BREAK
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LE RE	1020				•	0.004
11.7.5	1410					
1150	1560					
1112	2020	45				

EVALUATION BY: GART F. ZYCH, P.E. Aary F. Zych

Page 1 of 2

## Trapezoidal Channel Abalysis & Design Open Channel Uniform flow

Workshoel Name: OF Pond 6

Description: Determine flow depth from dam break

Solve For Depth

Civen Constant Data;

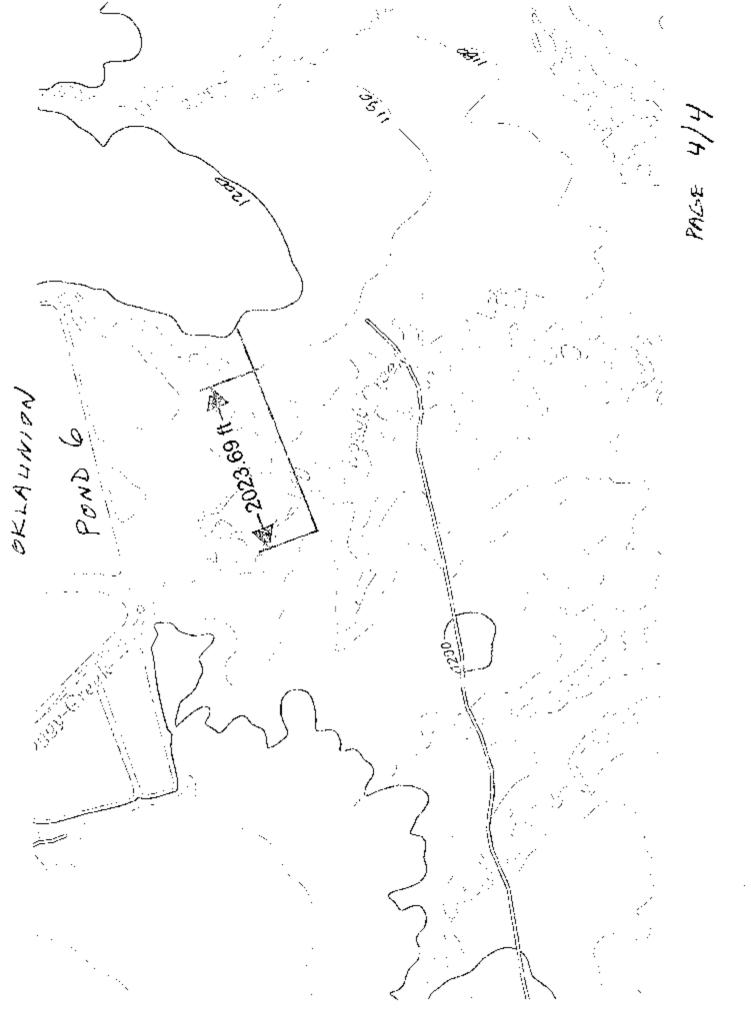
Bottom Width..... 400.00 Mannings 'n'..... 0.050 Channel Discharge.. 20300.00

Variable Input Data	Má ná mam	Maximum	Increment By
v.::::::::::::::::::::::::::::::::::::		==:====	=======================================
Z− <b>%</b> ⊝5t	40.00	50.00	10,00
Z-Right	40.00	50.00	10.00
Channel Slope	0.0005	0.0050	0.0005

Open Channel Flow Module, Version 3.43 (c) Haestad Methods, Inc. \* 37 Brockside Rd : Naterbury, Ct 06/08

Page 2 of 2

	VARIABLE	VARIABLE		VARIABLE	COMPUTES	)	COMPUTED
Hotiom Width	M=Left (B:V)	Z-Right (M:V)	Mannings "n"	Channel Slope ft/ft	Depth it	ಆರೆಟ	fps f
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400.00	50.00	40.00	0.050	0.0005	12.05	29300.00	2.58
400.00	40.00	50.00	0.050	0.0005	12.05	20300.00	2.58
400.00	50.00	50.00		0.0005	51,77	29300.00	2,52
400.00	40.00	40.00		0.0010		09300.00	3.40
400.00	60.00	40.00		0.0010	10.23	29300.00	3.33
400.00	40.00	50.00		0.0010	10.23	29300.00	3.33
400.00	50.00	50.00	0.050	0.0010	10.00	00.00860	31.35
100.00	40.00	40.00	0.060	0.0015	9.49	200.00	3.06
400.00	50.00	40.00		0.0015	9.28	29305.00	3.86
400.00	40.00	50.00	0.000	0.0015	9.28	09300.00	3.86
400.00	50.00	50.00		0.0015		29300.00	3.77
400.00	40.00	40.00	0.050	0.0025		29300.00	4.40
466.50	50.00	40.00	0.050	0.0020	8.66	29300.00	4.29
400.00	40.00	50.00	0.050	0.0020		20300.00	4.29
100.00	50.00	80.00	0.050	0.0020	કે.4ઇ	22300.00	4.19
400.00	40.00	40.00	0.050	0.0025	9.37	29300.00	4.77
400.00	10.00	40.90	0.050	0.0000	9.19	29300.00	4.65
400.00	40.00	50.00		0.0025	3.19	29300.00	4.65
400.00	50.00	50.00	0.050	0.0025	3.04	29300.00	4.55
400.00	40.00	40.00		0.0036	7,99	29300.00	5.09
400.00	50.00	49.00		0.0030		39300.00	4.97
400.00	49.00	50.00	0.050	0.9930	7.83	29309.00	4.97
400.00	00.00	50.00	0.050	0.0030	7,69	29300.00	4.86
400.50	40.00	40.00	0.080	0.0035		29306.00	5.38
400.00	10.00	45.00	0.050	0.0030	7.54	29300.00	5.26
400.00	40,00	50.00	0.050	0.9035		29300.00	5.26
400.00	50.00	50.00	0.680	0.0035	7.40	29300.00	5.14
400.00	40.00	40.00	0.050	0.0040		29390.00	5.65
400.00	50.00	40.00	0.050	0.0040		29300.06	5.82
400.00	40.00	50.00	0.050	0.0045	7.29	29300.00	5.52
400.00	00.00	90.00	0.050	0.0040	7.16	29350.00	5.40
400,00	40.00	40.00	0.050	0.0045	7.22	29300.00	4.190
400.00	50.00	40.00	0.050	0.0045	7.0%	39300.00	5.76
400.00	40.00	50.00	0.050	0.0045	7.08	29300.00	5.76
400.00	50,00	50.00	0.050	0.0045	6.06	29300.00	5.63
4000.06	40.09	40.00	0.050	0.0050	7.03	29300.00	n.10
400.00	50.60	40.00	0.050	0.0050	5.40	29300.00	5.93
400.00	40.00	55.00	0.050	0.0056	6.90	29300.00	0.98
100.00	50.00	50.00	0.050	0.5050	6.70	29300.00	5.85



## APPENDIX B

## Document 11

Coal Combustion Dam Inspection Checklist Forms



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Site Name:	OKLAUNION POWER STATION	Date:	February 23, 2011
Unit Name:	WASTERWATER EVAPORATION POND 6	Operator's Name:	AMERICAN ELECTRIC POWER
Unit I.D.:	WMU 001	Hazard Potential Classification:	High Significant Low
	Inspector's Name:	Kyle Shepard & Andy Cueto	

Check the appropriate box below. Provide comments when appropriate. If not applicable or not available, record "N/A". Any unusual conditions or construction practices that should be noted in the comments section. For large diked embankments, separate checklists may be used for different embankment areas. If separate forms are used, identify approximate area that the form applies to in comments.

	Yes	No		Yes	No
1. Frequency of Company's Dam Inspections?	Χ		18. Sloughing or bulging on slopes?		Χ
2. Pool elevation (operator records)?	Х		19. Major erosion or slope deterioration?		Χ
3. Decant inlet elevation (operator records)?	Х		20. Decant Pipes:		
4. Open channel spillway elevation (operator records)?	N/A	N/A	Is water entering inlet, but not exiting outlet?	N/A	N/A
5. Lowest dam crest elevation (operator records)?	Χ		Is water exiting outlet, but not entering inlet?	N/A	N/A
If instrumentation is present, are readings recorded (operator records)?		Х	Is water exiting outlet flowing clear?	N/A	N/A
7. Is the embankment currently under construction?		Х	21. Seepage (specify location, if seepage carries fines, and approximate seepage rate below):		
8. Foundation preparation (remove vegetation, stumps, topsoil in area where embankment fill will be placed)?	N/A	N/A	From underdrain?		Х
Trees growing on embankment? (If so, indicate largest diameter below)		Х	At isolated points on embankment slopes?		X
10. Cracks or scarps on crest?		Χ	At natural hillside in the embankment area?		Χ
11. Is there significant settlement along the crest?		Χ	Over widespread areas?		Χ
12. Are decant trashracks clear and in place?	N/A	N/A	From downstream foundation area?		Χ
13. Depressions or sinkholes in tailings surface or whirlpool in the pool area?		Х	"Boils" beneath stream or ponded water?		Х
14. Clogged spillways, groin or diversion ditches?	N/A	N/A	Around the outside of the decant pipe?		Χ
15. Are spillway or ditch linings deteriorated?	N/A	N/A	22. Surface movements in valley bottom or on hillside?		Х
16. Are outlets of decant or underdrains blocked?	N/A	N/A	23. Water against downstream toe?	Х	
17. Cracks or scarps on slopes?		Х	24. Were Photos taken during the dam inspection?	Х	

Major adverse changes in these items could cause instability and should be reported for further evaluation. Adverse conditions noted in these items should normally be described (extent, location, volume, etc.) in the space below and on the back of this sheet.

Issue #	Comments
	All active ponds on this site were incised. One pond that has not been active for 3 years was not incised but was in the process of being closed.



## **Coal Combustion Waste (CCW)**

## **Impoundment Inspection**

Impoundment NPDES Per	mit 1X0087815		INSPECTOR			
D Impoundment Na	Pate 11.16.2007 Ime WASTEWATI	ER EVAPOR	ATION POND NO	D. 6		
Impoundment Comp EPA Reg	•	ELECTRIC PO	OWER			
State Age (Field Office) Addı Name of Impoundm	ress 19//INDUS		LEVARD, ALBILEN		502-7833	
(Report each impou	ndment on a separ	ate form ui	nder the same Im	npoundment .	NPDES Permit	number)
New	Update 🗵					
Is impo	oundment currently being pumped in	-		Yes		No
IMPOUNDMENT	FUNCTION: WA	STEWATER	R AND RESIDUAL	STORAGE / E	VAPORATION	POND
Nearest Downstream	Town Name: NO	TOWN WI	THIN A 18 MILE F	RADIUS		
Distance from the im	poundment: ±18	MILES				
Location:						
Latitude 34	Degrees	04	Minutes	47.99	Seconds	ľ
Longitude 99	Degrees	10	Minutes	45.00	Seconds	V
State			County			
Does a st	ate agency regulat	te this impo	oundment?	Yes		No
	If So	Which Sta	ite Agency?			

HAZARD POTEN	NTIAL (In the event the impoundment should fail, the following would occur):
	<b>LESS THAN LOW HAZARD POTENTIAL:</b> Failure or misoperation of the dam results in no probable loss of human life or economic or environmental losses.
	LOW HAZARD POTENTIAL: Dams assigned the low hazard potential classification are those where failure or misoperation results in no probable loss of human life and low economic and/or environmental losses. Losses are principally limited to the owner's property.
	<b>SIGNIFICANT HAZARD POTENTIAL:</b> Dams assigned the significant hazard potential classification are those dams where failure or misoperation results in no probable loss of human life but can cause economic loss, environmental damage, disruption of lifeline facilities, or can impact other concerns. Significant hazard potential classification dams are often located in predominantly rural or agricultural areas but could be located in areas with population and significant infrastructure.
	<b>HIGH HAZARD POTENTIAL:</b> Dams assigned the high hazard potential classification are those where failure or misoperation will probably cause loss of human life.

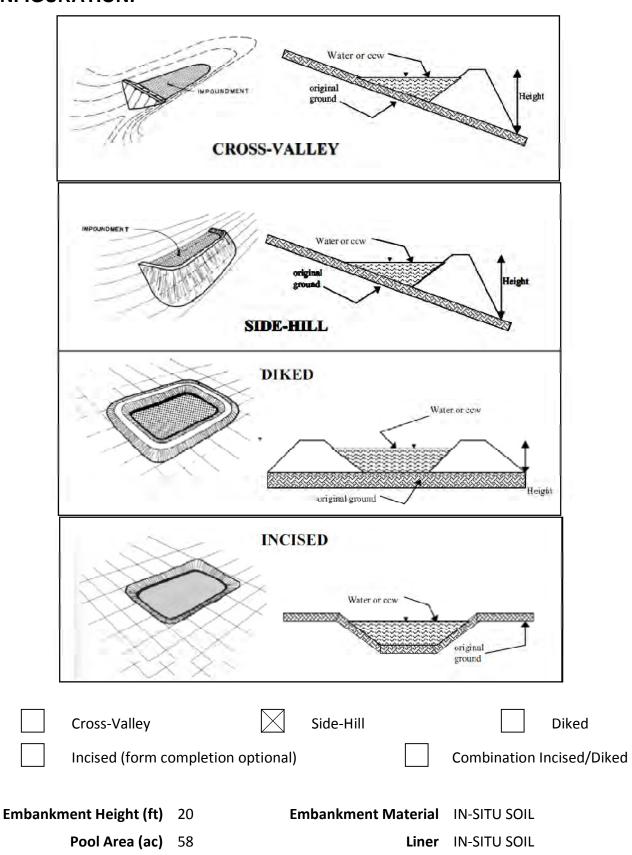
## **DESCRIBE REASONING FOR HAZARD RATING CHOSEN:**

UPON VISUAL INSPECTION, THERE WAS NO SIGHT OF ANY POSSIBLE BREACHING OR OVERTOPPING OF THIS IMPOUNDMENT.

**Current Freeboard (ft)** 3

# **US EPA ARCHIVE DOCUMENT**

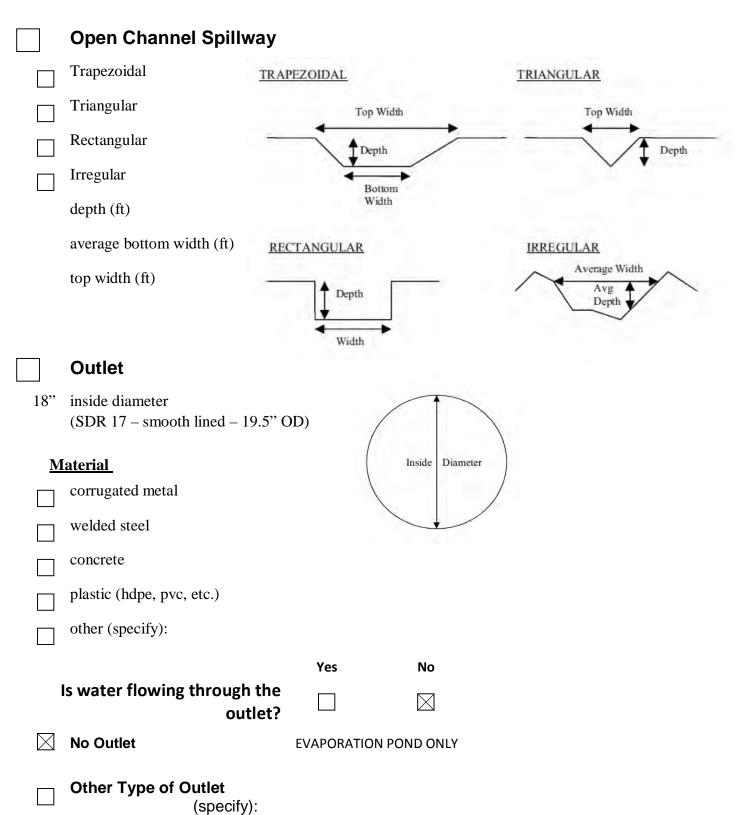
## **CONFIGURATION:**



Liner Permeability N/A



#### **TYPE OF OUTLET** (Mark all that apply)



The Impoundment was Designed By TIPPETT & GEE:

**US EPA ARCHIVE DOCUMENT** 

	Yes	No
Has there ever been a failure at this site?		
If So When?		
If So Please Describe :		

	Yes	No
Has there ever been significant seepages at this site?		
If So When?		

If So Please Describe:

**US EPA ARCHIVE DOCUMENT** 

	Yes	No
Has there ever been any measures undertaken to		
monitor/lower Phreatic water table levels based		
on past seepages or breaches		
at this site?		
If so, which method (e.g., piezometers, gw		
pumping,)?		

If So Please Describe:

# ADDITIONAL INSPECTION QUESTIONS

Concerning the embankment foundation, was the embankment construction built over wet ash, slag, or other unsuitable materials? If there is no information just note that.

NO

Did the dam assessor meet with, or have documentation from, the design Engineer-of-Record concerning the foundation preparation?

YES

From the site visit or from photographic documentation, was there evidence of prior releases, failures, or patchwork on the dikes?

NO

# **Available Information Checklist**

Coal Combustion Residuals Impoundment (CCRI) Dam

ITEM DECORPTION	PROVI	PROVIDED BY UTILITY		
ITEM DESCRIPTION	YES	NO	N/A	
1. Descriptive Information:				
a) Impoundment Capacity (Normal & Max)	Х			
b) Impoundment Surface Area	х			
c) Hazard Classification	х			
d) Freeboard (Normal & Min)	х			
e) Maximum Dam Height	х			
f) Dam Crest Elevation	х			
g) Crest Width	Х			
h) Upstream Slope Inclination	х			
i) Downstream Slope Inclination	х			
j) Spillway Type, Size, & Crest Elevation			х	
k) Outlet Condit Type, Size, & Max Flow Capacity			х	
l) Historical Maximum Pond Elevation	х			
m) Year Built	Х			
n) Design Life	Х			
o) Specific Wastes Permitted in Impoundment	х			
p) Other (describe)				
2. Regional Map showing CCWI & schools, hospitals, etc. w/i 5 mi downgradient		х		
3. Management Unit Dwgs:				
a) Plans	х			
b) Sections	х			
c) Elevations	х			
d) Other (describe) (maybe closed - may include a LOI for closing)	Х			
4. Design Information:				
a) Name of Designer of Record	х			
b) Design Assumptions		х		
c) Design Analyses (Including Hydrologic/Hydraulic & Slope Stability Analyses		х		





## **Available Information Checklist (Continued)**

Coal Combustion Residuals Impoundment (CCRI) Dam

ITEM DESCRIPTION		PROVIDED BY UTILITY			
		YES	NO	N/A	
d) Spillway Design Flood or Design Basis					х
e) Slope Stability Factors of Safety				Х	
f) Design Soil Properties and Parameters	5		х		
g) Other (describe)					
5. Permits:					
a) NPDES?	Number?	TX0087815	х		
b) Dam Safety - Operating Permit?	Number?	n/a			Х
c) Other (describe)	WQ00025740	00 - unknown permit no	•		
6. Subsurface Information:					
a) Geology				Х	
b) Geotechnical Report				х	
c) Test Boring Logs			х		
d) Subsurface Profiles				Х	
f) Other (describe)					
7. Monitoring Information:					
a) Observation Wells/Piezometer Readin	ngs				Х
b) Seepage Readings	<u> </u>				Х
c) Settlement Readings					х
d) Alignment Readings					х
e) Inclinometer Readings					х
f) Time vs Reading Graphs					х
g) Other (describe)					
8. Instrumentation Dwgs:					
a) Location Plan					х
b) Section Views					х
c) Other (describe)					





## **Available Information Checklist (Continued)**

Coal Combustion Residuals Impoundment (CCRI) Dam

ITEM DESCRIPTION	PROVI	PROVIDED BY UTILITY		
HEWI DESCRIPTION		NO	N/A	
9. Operation, Maintenance, & Surveillance:				
a) Operating Procedures	х			
b) Maintenance Procedures	х			
c) Inspection Procedures	X			
d) Third Party Inspection Reports	х			
e) Other (describe)				
10. Miscellaneous:				
a) Construction Documentation/Foundation Prep	х			
b) Spills or Releases		х		
c) Repairs			x	
d) Inundation Map		х		
e) Other (describe)				
f) Emergency Action Plan	х			

#### NOTE:

All data is to be furnished on CD to Dewberry by end of March 2011.



#### **Available Information Checklist - Addendum**

Coal Combustion Residuals Impoundment (CCRI) Dam

,	<u> </u>		
ITEM DESCRIPTION	PROVI	DED BY	UTILITY
TIEW DESCRIPTION		NO	N/A
11. Coal Combustion Residuals Handling Equipment Train:			
a) Fly Ash (dry train - described below)			
Generation & Collection Methods; Equipment	х		
Transport to Storage Methods; Equipment; Containment Methods	Х		
Storage Methods; Equipment; Containment Methods	х		
• Transport to Disposition Methods; Equipment; Containment Methods	Х		
b) Bottom Ash (wet train)			
Generation & Collection Methods; Equipment	х		
<ul> <li>Transport to Storage Methods; Equipment; Containment Methods</li> </ul>	х		
Storage Methods; Equipment; Containment Methods			
Transport to Disposition Methods; Equipment; Containment Methods			
c) Boiler Slag (same as Bottom Ash)			
Generation & Collection Methods; Equipment	Х		
<ul> <li>Transport to Storage Methods; Equipment; Containment Methods</li> </ul>	Х		
Storage Methods; Equipment; Containment Methods			
<ul> <li>Transport to Disposition Methods; Equipment; Containment Methods</li> </ul>	Х		
d) Flue Gas Desulfurization Sludge (inspected)			
Generation & Collection Methods; Equipment	Х		
<ul> <li>Transport to Storage Methods; Equipment; Containment Methods</li> </ul>	Х		
Storage Methods; Equipment; Containment Methods	Х		
Transport to Disposition Methods; Equipment; Containment Methods	х		
Note: AEP representatives preferred not to tour and inspect the Fly Ash $\mathfrak a$		train.	
However they did describe the process below.			

Fly Ash Disposal Process (dry train):

- 1. Fly ash is electrostatically precipitated and conveyed by gravity to a hopper
- 2. The ash is then pneumatically conveyed to a holding silo
- 3. The ash is then loaded via gravity feed into trucks
- 4. The ash is stock piled there to be either sold to a 3rd party for beneficial reuse or to be permanently disposed of in the landfill



# APPENDIX C

**Document 12** 

Additional Site Photographs

#### Appendix C - Additional Photographs



Figure C-1. Additional incised CCR pond #21



Figure C-2. Additional incised CCR pond #22



Figure C-3. Additional incised CCR pond #23



Figure C-4. Additional incised CCR pond #7